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Computer simulation of electron beams. I. Space-charge algorithm for asymmetric beams

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Longitudinal space-charge forces can be neglected in computer simulations of slowly curving quasilaminar electron beams. A particle-mesh-type algorithm for transverse space-charge forces is developed, and great simplification in numerical calculation of asymmetric electron beams is demonstrated. Some typical examples for kinescope beams are discussed.

I. INTRODUCTION

Accurate manipulation of electron beams is the key to design of many electron-optics devices such as CRT tubes, accelerators, etc. The advent of the digital computer has made it possible to calculate the trajectories of key electrons in the beam under the influence of the electromagnetic fields created inside the device by external sources. The inclusion, however, of the mutual Coulomb-repulsion forces of the electrons (space charge) makes the calculation nonlinear and therefore greatly increases the calculation time and expense. The numerical solution of the ensuing trajectory equations then requires a number of iterations; each iteration solves a trajectory equation with space-charge forces inferred from the solution of the previous iteration. Suppose N electron trajectories are to be calculated numerically, and each trajectory requires $L/\Delta z = l$ steps. In the absence of space-charge forces, Nl fields and potentials must be calculated in total (each field has three components, moreover). The inclusion of space-charge forces increases this number of fields and potentials to MN^2l (where M is the number of iterations). Aside from the extra factor MN , the calculation is also made more difficult by the need to avoid $1/r$ -type singularities in the Coulomb forces.

We show that it is possible to ignore the longitudinal space-charge force component for thin electron beams. This removes the need for iteration; i.e., reduces the space-charge calculation by a factor M . Also, the relative smoothness of transverse space-charge forces (with respect to interparticle distances) makes it possible to formulate a "particle-mesh force" algorithm of the type defined by Hockney and Eastwood.¹ The factor N^2 is then reduced to nN , where n is a mesh number much less than N . The algorithm is particularly useful for intricate "pencil" beams, e.g., as in kinescopes where lensing action mixes an initial thermal distribution of electrons into a long, quasilaminar² beam of electron trajectories. The beam may curve slowly with respect to its diameter; however, its perveance should not become too large (see Appendix A). Most important, no symmetry properties are assumed.

II. NEGLECT OF LONGITUDINAL SPACE-CHARGE FORCES

Let the beam be characterized by a smooth charge density $\rho(r)$ which is not a function of time. The nonrelativistic

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equations of motion are, for $\mathbf{r} = (r_T, z)$,

$$\ddot{\mathbf{r}} = - (e/m) [\mathbf{E}(r_T, z) + \dot{\mathbf{r}} \times \mathbf{B}_0(r_T, z)], \quad (1)$$

$$DH_1(z)/Dz = 0,$$

where $H_1(z) = m(\dot{z}^2 + \dot{r}_T^2)/2 - e\Phi(r_T, z)$ is the single-particle Hamiltonian, e is the electron charge, Φ is the electrostatic potential, $\mathbf{E} = -\nabla\Phi$ is the electrostatic field, and \mathbf{B}_0 is an externally applied magnetic field (the small induced field at r due to other particle motion is neglected). The second equation expresses conservation of $H_1(z)$ along a trajectory. The time dependence can be replaced by dependence on z (denoted by primes) through

$$\dot{r}_T = z'r'_T, \quad (2)$$

$$\ddot{r}_T = z^2 r''_T + \frac{1}{2} (dz^2/dz) r'_T,$$

and z^2 can be replaced by potentials, using $H_1(z) = H_1(0)$. The problem lies in the fact that the field $\mathbf{E}(r_T, z)$ is a solution of the Poisson equation,

$$\nabla \cdot \mathbf{E}(r) = \epsilon_0^{-1} \rho(r), \quad (3)$$

where ϵ_0 is the vacuum dielectric permittivity. However, $\rho(r)$ is determined by the trajectories of the electrons so that Eqs. (1) and (3) are coupled when space-charge forces are not negligible. The usual method of solution is iterative; the n th trajectory calculations use the charge density inferred from the $(n-1)$ st trajectories.

For the applications under consideration, an electron beam changes direction slowly, i.e., the local radius of curvature is large compared to the local diameter. The location \mathbf{r} in the beam can be decomposed into a set of locally orthogonal coordinates $\mathbf{r} = (\xi, \zeta)$, where $\hat{\zeta}$ is a unit vector in the main axial direction and $\hat{\xi}_x, \hat{\xi}_y$ are two others in a plane normal to $\hat{\zeta}$. The transverse space-charge approximation rests on the assumption that $\rho(\xi, \zeta)$ depends only weakly upon ζ . In general, however, the space-charge field $\mathbf{E}_{sp}(r)$ can be obtained from the integral form of Eq. (3),

$$\mathbf{E}_{sp}(r) = \frac{1}{4\pi\epsilon_0} \int d^3r_1 \rho(r_1) \frac{\mathbf{r} - \mathbf{r}_1}{|\mathbf{r} - \mathbf{r}_1|^3}, \quad (4)$$

but when $\partial\rho/\partial\zeta_1 = 0$, this simplified to the area integral over a cross section of the beam at $\zeta_1 = \zeta$:

$$E_{sp}(\xi, \zeta) = \frac{1}{2\pi\epsilon_0} \int d^2\xi \rho(\xi, \zeta) \frac{\xi - \xi_1}{|\xi - \xi_1|^2}. \quad (5)$$

This removes the iterative coupling because $\mathbf{E}_{sp}(r)$ then de-

depends only upon the *past* history of the trajectories so that the step from $r_T(z)$ to $r_T(z + \Delta z)$ does not require anything other than knowledge of local initial conditions. Equations (1), (2), and (5) can then be solved in a noniterative straightforward numerical procedure.

The approximation $\partial\rho/\partial\xi_1 = 0$ in Eq. (4) does require that trajectory directions do not differ drastically from ξ_1 , and also that acceleration not be very large along the beam. The magnitude of the space-charge forces also play a role because these cause the electrons to diverge from each other, which affects $\rho(\xi_1, \xi_2)$ for $\xi_2 > \xi_1$. A criterion is given in Appendix A for the restriction upon space-charge forces. These restrictions are not serious in kinescope drift regions, nor in lensing regions where the acceleration along the beam direction is slow over a length of several diameters, and where beam perveance is small.

III. DEVELOPMENT OF THE ALGORITHM

The elimination of time from Eqs. (1) and (2) transforms the trajectory equations into a set of ordinary second-order differential equations in z with initial conditions, if approximation (5) is valid. Whether linear multistep or single-step Runge-Kutta methods³ are used, we can illustrate what is involved by considering an equivalent set of difference equations:

$$\begin{aligned} r_i(z + \Delta z) &= r_i(z) + r_i'(z)\Delta z + \frac{1}{2} r_i''(z)\Delta z^2, \\ r_i'(z + \Delta z) &= r_i'(z) + r_i''(z)\Delta z, \\ r_i''(z) &= f\{\mathbb{E}[r_i(z)], \mathbb{B}_0, r_i'\}. \end{aligned} \quad (6)$$

The functional dependence of $r_i''(z)$ need not be specified in detail here; it follows from Eqs. (1), (2), and (5). In particle-particle⁴ methods, the beam is represented by N trajectories,

each with characteristic charge q_j ($1 < j < N$). The space-charge part of the field $\mathbb{E}[r_i(z)]$ acting upon particle i can then be written as

$$\begin{aligned} \mathbb{E}_{sp}^{(i)} &\equiv \mathbb{E}_{sp}[r_i(z)] \\ &= \frac{1}{2\pi\epsilon_0} \sum_{j=1}^N q_j \frac{\xi_i - \xi_j}{|\xi_i - \xi_j|^2} \equiv \sum_{j=1}^N \mathbb{E}_{ij} \end{aligned} \quad (7)$$

in terms of the locally orthogonal locations ξ_j of the j th trajectory from trajectory i . The $j = i$ term must be excluded, and q_j is conserved along a representative trajectory. The solution of Eq. (6) for one step Δz requires $\frac{1}{2}N(N-1)$ calculations of \mathbb{E}_{ij} , hence roughly $N^2L/2\Delta z$ calculations (where L is the total path length) are needed. This poses two problems: not only is N^2 a large number, but also N would have to be chosen extremely large in order to ensure that near singularities for ξ_j close to ξ_i are balanced out by other near trajectories.

Particle-mesh methods⁵ offer an attractive alternative. Consider for illustrative purposes only that the beam travels in the z direction and let $\mathbf{r} = (x, y, 0)$ be the transverse coordinate. Define a square mesh in a plane normal to z , and let M mesh squares cover the cross section of the beam. Define a mesh density

$$\rho_j = \frac{1}{h^2} \sum_{i=1}^N q_i \theta[r_i(z) - \mathbf{R}_j(z)], \quad (8)$$

where $\mathbf{R}_j(z)$ is the center of the j th mesh square with area h^2 , and $\theta(\mathbf{r}_1 - \mathbf{r}_2)$ is zero when $|x_1 - x_2| > h/2$ or $|y_1 - y_2| > h/2$, and unity otherwise. The new densities should be smoothly varying, and each mesh square should contain many trajectories. Using Eq. (5), one finds for the space-charge fields at \mathbf{r} due to a square of area h^2 centered at \mathbf{r}_j with uniform charge density ρ_j

$$\begin{aligned} E_x(\mathbf{r}) &= K \left[\frac{1}{2} t_f \ln \left(\frac{t_f^2 + s_f^2}{t_i^2 + s_i^2} \right) - \frac{1}{2} t_i \ln \left(\frac{t_f^2 + s_f^2}{t_i^2 + s_i^2} \right) \right. \\ &\quad \left. + 2s_f [\arctan(t_f/s_f) - \arctan(t_i/s_f)] - 2s_i [\arctan(t_f/s_i) - \arctan(t_i/s_i)] \right], \\ s_f &= x - x_j + \frac{1}{2}h, \quad t_f = y - y_j + \frac{1}{2}h, \quad s_i = x - x_j - \frac{1}{2}h, \quad t_i = y - y_j - \frac{1}{2}h, \quad K = h^2\rho_j/2\pi\epsilon_0. \end{aligned} \quad (9)$$

A similar expression holds for $E_y(\mathbf{r})$. Equation (9) suggests the following interpolation formulas for $\mathbb{E}_{sp}(\mathbf{r}, z)$:

$$\mathbb{E}_{sp}[\mathbf{r}(z)] = K \sum_{j=1}^M \frac{\mathbf{r} - \mathbf{r}_j(z)}{|\mathbf{r} - \mathbf{r}_j(z)|^2 + h^2/\pi}. \quad (10)$$

Each term of Eq. (10) has the same limiting value as $\mathbf{r} \rightarrow \mathbf{r}_j(z)$ or as $\mathbf{r} \rightarrow \infty$ as the corresponding form of Eq. (9); the computational advantage of Eq. (10) over Eq. (9) consists of not needing to evaluate a number of logarithms and arctangents for each term. The major discrepancies between Eqs. (10) and (9) occur at distances $|\mathbf{r} - \mathbf{r}_j(z)| \sim \frac{1}{2}h$, as illustrated in Fig. 1 which plots the ratio of the x component of Eq. (9) to that of one term of Eq. (10) for $K = 1$, $h = 1$. Therefore, Eq. (10) will converge towards the correct answer as $h \rightarrow 0$ providing h does not become so small that the graininess of chosen elec-

tron trajectories becomes a factor (see Appendix B).

IV. SOME NUMERICAL RESULTS

The simplest space-charge problem is the expansion of an axially symmetric uniform laminar beam containing current I and with initial waist radius R_0 .⁶ The radius at distance z , $R(z)$, is given analytically by Eq. (A2), and the expansion factor $r(z)/r(0)$ of any core of initial width $r(0)$ is a constant at fixed z . A test case was chosen in a 3.5 mA beam of initial radius $R_0 = 50$ (in arbitrary units). The electron velocity was chosen to be equivalent to 30 keV. At $z = 13\,500$ units, Eqs. (A2) yield an expansion factor 1.3522 (to a four-decimal-place accuracy). The numerical results for $r(z)$ are given in Fig. 2 as a function of $r(z) = 1.3522 r(0)$. The beam was discretized into 16 circle sectors, each of which

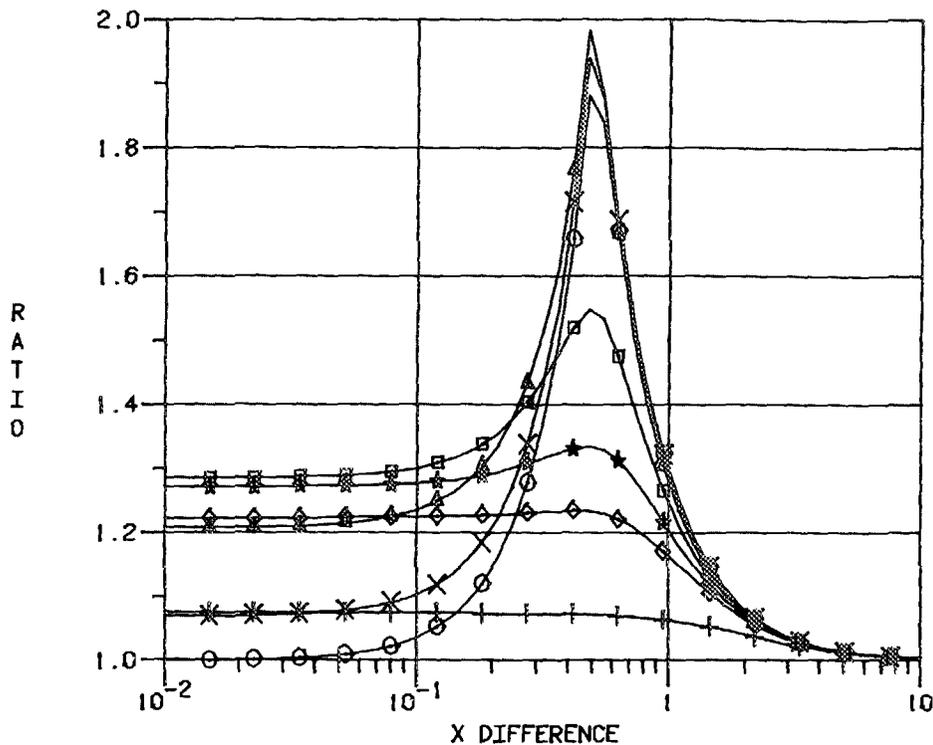


FIG. 1. Ratio of exact to approximated E_x space-charge field (in a plane) from a uniform unit square vs x distance from its center for y distance 0(\circ), 0.2(\times), 0.4(\triangle), 0.6(\square), 0.8($*$), 1.0(\diamond), and 2.0(∇).

was divided into 18 annular pieces of equal radial width. The space-charge mesh consisted of 169 squares. While that choice means only a few electrons per mesh square, the regularity of the discretization avoids the pitfalls of granularity, and Fig. 2 shows a good representation of the laminar beam in only five steps in the z direction. Figure 3 shows predictions of several electron landing positions in a typical kinescope drift-region beam discretized into 1500–1600 representative trajectories. These data are for a 3.5 mA beam with velocity of the electrons very close to 25 keV, and the drift distance is 13.5 in. along the axis. Radial symmetry has been

chosen for simplicity, although no use has been made of it. An initial phase space⁷ (consisting of values of x, x', y, y' , and charge density q for each beamlet) is prepared at the entrance to the drift region. This phase space is quite distorted from a typical input cathode phase space because the electrons have passed through a number of electrostatic lenses and have also undergone aberrations. Moreover, the input phase space at the cathode is complicated by a thermal distribution of emitted electrons. The details are discussed elsewhere.⁸ Figure 3 compares the unapproximated numerical calculation based upon Eq. (4) with an axisymmetric space-charge

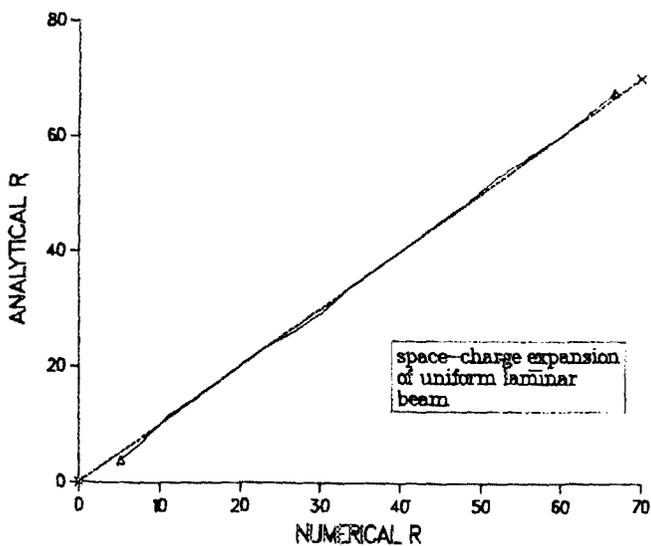


FIG. 2. Comparison of space-charge expansion of a uniform laminar beam under the transverse-force algorithm to the analytical result (ordinate) for expansion constant ≈ 1.3522 . The full line would coincide with the 45° line if there were perfect agreement.

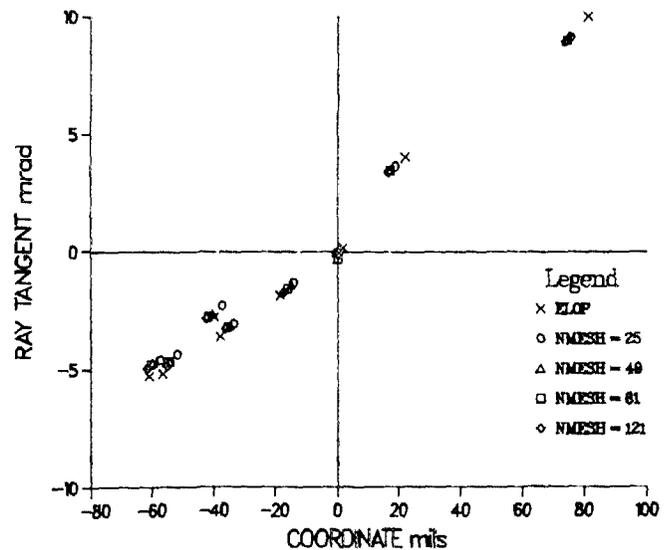


FIG. 3. Comparison $r' = dr/dz$ vs r of selected kinescope electrons after a drift of 13.5" at 25 keV for various values of the number of mesh squares NMESH (1 mil = 0.001 in). The ELOP values are calculated from an unapproximated Poisson equation.

program ELOP⁹ to diverse calculations based upon Eq. (5) with the algorithm of this paper. Various choices of the number of mesh squares are shown. The smoothness of the space-charge forces is apparent in this type of beam because the results for NMESH = 121 (121 squares) hardly differ from those for NMESH = 25 (25 squares). Moreover, there is good agreement everywhere with the ELOP calculation, except for a very weak edge beamlet that is highly aberrated. Further comparisons entail calculations of beam current densities, but these are discussed in a companion paper¹⁰ as the problem of beam representation is a topic in its own right.

A typical simulation of 1519 trajectories over 11 z steps with a space-charge grid of 49 squares required 18 CPU seconds on an IBM 3081 computer. We estimate that a full-scale three-dimensional space-charge calculation in a similar particle-particle simulation would require of the order of 3000 cpu seconds on the same computer,¹⁰ unless simplified analytical calculations are considered.¹¹⁻¹³ Hence it appears that reasonably accurate simulations of electron beams at low cost are quite feasible with the algorithm.¹⁴

APPENDIX A: NEGLECT OF LONGITUDINAL SPACE-CHARGE FIELD

In order to study restrictions upon the approximation of Eq. (4) by Eq. (5), consider an axisymmetric laminar beam of transversely uniform density $\rho(z)$ with a waist of radius R_0 at $z = 0$. Then the x component of the space-charge field, according to Eq. (4), is

$$E_x(\mathbf{r}) = \frac{1}{4\pi\epsilon_0} \int d^2r_1 \int_{-\infty}^{\infty} dz_1 \rho(z_1) \times \frac{x - x_1}{[(\mathbf{r} - \mathbf{r}_1)^2 + (z - z_1)^2]^{3/2}}. \quad (\text{A1})$$

By using $\rho(z_1) = j(z_1)/\dot{z}_1 = (m/2e)^{1/2} j(z_1)/\Phi^{1/2}$ under the assumption that Φ is the velocity in eV and $j(z_1)$ is the current density in the z_1 plane, we note that the insertion of Eq. (A1) into Eq. (1), for $B_0 = 0$, leads to the well-known¹⁵ expression for the beam radius $R_0(z)$ at z :

$$R_0(z) \equiv R_0 \exp W^2, \quad \int_0^W dt e^{t^2} = K_p^{1/2} z / R_0, \quad (\text{A2})$$

$$K_p \equiv \beta I / 4\Phi^{3/2}, \quad \beta \equiv (m/2e)^{1/2} / 2\pi\epsilon_0,$$

where $I = \pi R_0^2 j(0)$ is the total current, and K_p is the perveance (a well-known measure of space-charge force in a beam). An important feature of Eq. (A2), and of Gauss' law, is that a laterally uniform beam at $z = 0$ remains so at other values of z . Now apply Eq. (A1) at $z = 0$, $\mathbf{r} = \mathbf{R}_0$ (i.e., at the edge of the beam):

$$E_x \approx \frac{1}{2\pi\epsilon_0} \int d^2r_1 \frac{x - x_1}{|\mathbf{R}_0 - \mathbf{r}_1|^2} \times \left(\frac{1}{2} \int_{-L/2}^{L/2} dz_1 \rho(z_1) \frac{|\mathbf{R}_0 - \mathbf{r}_1|^2}{[|\mathbf{R}_0 - \mathbf{r}_1|^2 + z_1^2]^{3/2}} \right). \quad (\text{A3})$$

The truncation of the dz integral at $\pm L/2$ is not a serious error as long as $L \gg 2R_0$. However, for weak perveance K_p so

that $K_p z^2 / R_0^2 \ll 1$, Eq. (A2) is well approximated by $R_0(z) = R_0 + K_p z^2 / R_0$, and it is quite obvious that $z = L/2$ can be quite large in the above sense if K_p is sufficiently small. From this and from the homogeneity of the beam at all z it follows that to first order, for $|z| \ll L/2$,

$$\rho(z) \approx (1 + K_p z^2 / R_0^2)^{-2} \rho(0). \quad (\text{A4})$$

Let the new variable $t = z / |\mathbf{R}_0 - \mathbf{r}_1|$ in Eq. (A3) and insert Eq. (A4). We obtain

$$E_x = \frac{\rho(0)}{2\pi\epsilon_0} \int d^2r_1 \frac{x - x_1}{|\mathbf{R}_0 - \mathbf{r}_1|^2} G [K_p |\mathbf{R}_0 - \mathbf{r}_1|^2 / R_0^2], \quad (\text{A5})$$

$$G(Q) \approx \int_0^\infty dt (1 + Qt^2)^{-2} (1 + t^2)^{-3/2},$$

and Q is an abbreviation for the product $K_p |\mathbf{R}_0 - \mathbf{r}_1|^2 / R_0^2$. The extension of the upper bound of the integral to infinity is no problem due to the rapid falloff of the integrand with t . The $G(Q)$ integral can be given in closed form,

$$G(Q) = \frac{1 + Q/2}{(1 - Q)^2} + \frac{Q(1 - Q/4)}{(1 - Q)^{5/2}} \ln \left(\frac{1 - (1 - Q)^{1/2}}{1 + (1 - Q)^{1/2}} \right), \quad (\text{A6})$$

which can be expanded for small Q into the series,

$$G(Q) = 1 + Q \ln Q + (3/2 + \ln 4)Q + O(Q^2/nQ) + \dots \quad (\text{A7})$$

Hence $G(Q) = 1$ is a good approximation for $Q \ll 1$, and the error is of order $Q \ln Q$. Because $Q \lesssim K_p$ it follows that the error in setting $G(Q) = 1$ is of order $K_p \ln K_p$, and also that E_x is approximated well by Eq. (5). So even in the most favorable case of a laminar beam, there is a restriction on beam perveance that limits the validity of neglecting longitudinal space-charge forces.

APPENDIX B: ACCURACY OF THE SPACE-CHARGE FIELD ESTIMATE

The use of Eq. (10) instead of Eq. (5) involves several approximations. These are examined here in some more detail. Consider a mesh square of area $S = h^2$ in the cross section of the beam and assume z is the beam axis of importance for simplicity. The integral of importance is

$$E_x(\mathbf{r}) = \int_S d^2r_1 \rho(\mathbf{r}_1) G_x(\mathbf{r} - \mathbf{r}_1), \quad (\text{B1})$$

where $G_x(\mathbf{r} - \mathbf{r}_1) = (x - x_1) / |\mathbf{r} - \mathbf{r}_1|^2$, and \mathbf{r} is the point where space-charge due to the square is measured. Define

$$\langle \rho \rangle \equiv \frac{1}{h^2} \int_S d^2r_1 \rho(\mathbf{r}_1), \quad Q(\mathbf{r}) \equiv \frac{1}{h^2} \int_S d^2r_1 G_x(\mathbf{r} - \mathbf{r}_1), \quad (\text{B2})$$

and let $\bar{Q}(\mathbf{r}) \equiv (x - x_1) / [|\mathbf{r} - \mathbf{r}_1|^2 + h^2/\pi]$. It is easily seen that (B1) can be rewritten as

$$E_x(\mathbf{r}) = \langle \rho \rangle \bar{Q}(\mathbf{r}) + h^2 \langle \rho \rangle \{ Q(\mathbf{r}) - \bar{Q}(\mathbf{r}) \} + \int_S d^2r_1 \{ \rho(\mathbf{r}_1) - \langle \rho \rangle \} G_x(\mathbf{r} - \mathbf{r}_1). \quad (\text{B3})$$

The first term is the approximation Eq. (10), and the remaining terms are the error estimates. Figure 1 shows that the second term is negligible, except for an area around

$|\mathbf{r} - \mathbf{r}_1| \sim h/2$ that decreases in proportion to the rest as $h \rightarrow 0$. The third term also vanishes as $h \rightarrow 0$ provided the mesh square contains many trajectories so that $\langle \rho \rangle$ is smoothly varying from the one square to the next.

¹R. W. Hockney and J. W. Eastwood, *Computer Simulation Using Particles* (McGraw-Hill, New York, 1981).

²By "quasilaminar," we mean beams that do allow for crossing trajectories, but in which the effective beam envelope (containing, e.g., 90% of the current) does not change in diameter rapidly over many diameters length.

³E. g. J. D. Lambert, in *The State of the Art in Numerical Analysis*, edited by D. Jacobs (Academic, London, 1977), p. 451.

⁴R. W. Hockney and J. W. Eastwood, *Computer Simulation Using Particles* (McGraw-Hill, New York, 1981), p. 18. See also T. Groves, D. L. Hammond, and H. Kuo, *J. Vac. Sci. Technol.* **16**, 1680 (1979).

⁵R. W. Hockney and J. W. Eastwood, *Computer Simulation Using Particles* (McGraw-Hill, New York, 1981), p. 120.

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¹¹W. P. Lysenko, *IEEE Trans. Nucl. Sci.* **NS-26**, 3508 (1979).

¹²W. P. Lysenko and E. A. Wadlinger, *IEEE Trans. Nucl. Sci.* **NS-28**, 2509 (1981).

¹³W. J. Gallagher, *IEEE Trans. Nucl. Sci.* **NS-28**, 2552 (1981).

¹⁴The estimate is based largely upon the considerations of Sec. I, and partly upon the ELOP program which exploits axial symmetry and is therefore much more efficient than an equivalent asymmetric computer program.

¹⁵O. Klemperer (and M. E. Barnett, in collaboration), *Electron Optics*, 3rd edition (Cambridge University, London, 1971).