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Investigation of Dynamic Loading for 13.2 MW Downwind Pre-Aligned Rotor

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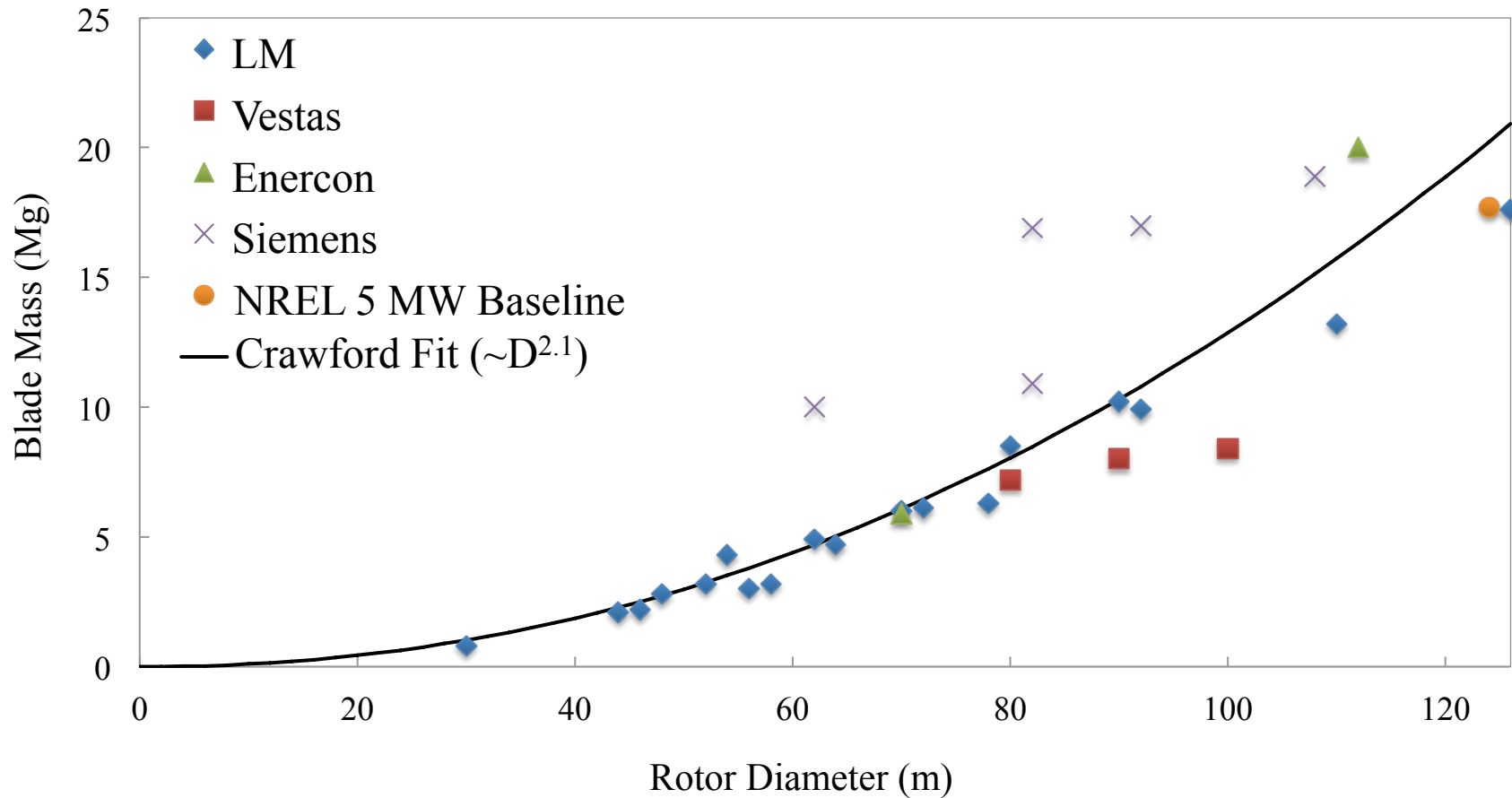
Patrick Moriarty (Senior Engineer)

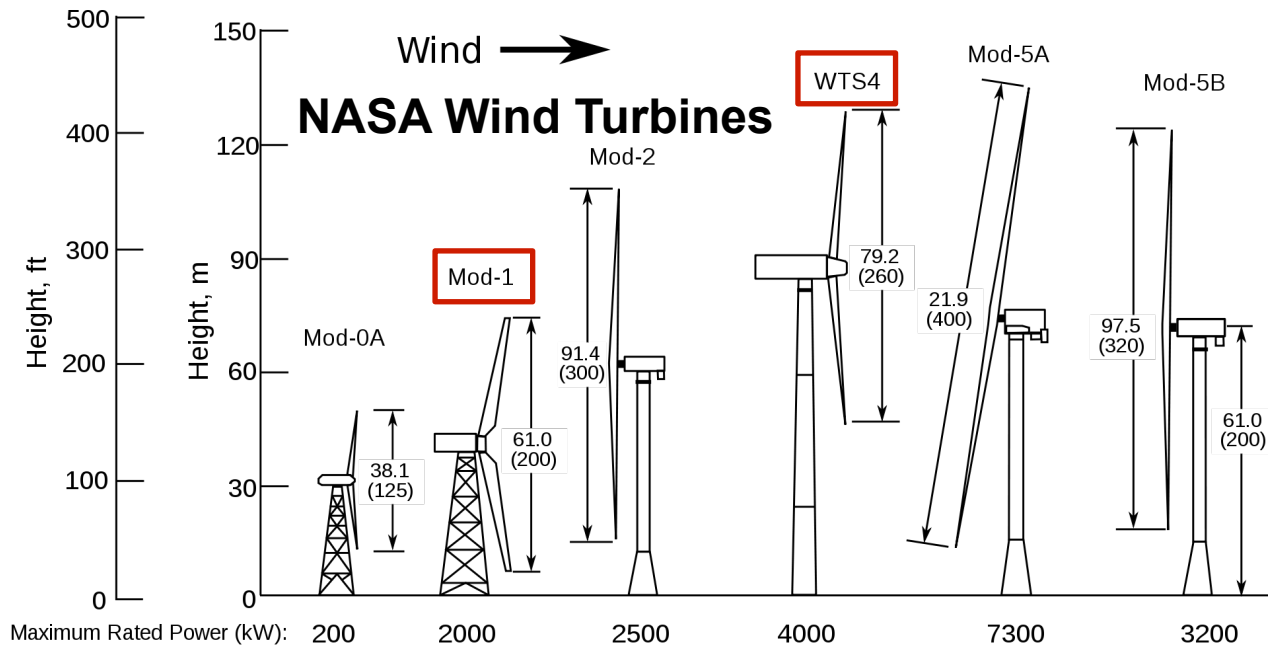


Outline

- **Extreme-scale issues & Force alignment**
- **Pre-Alignment & Impact of this design**
- **FAST simulations & main results**
- **Discussion & Conclusion**

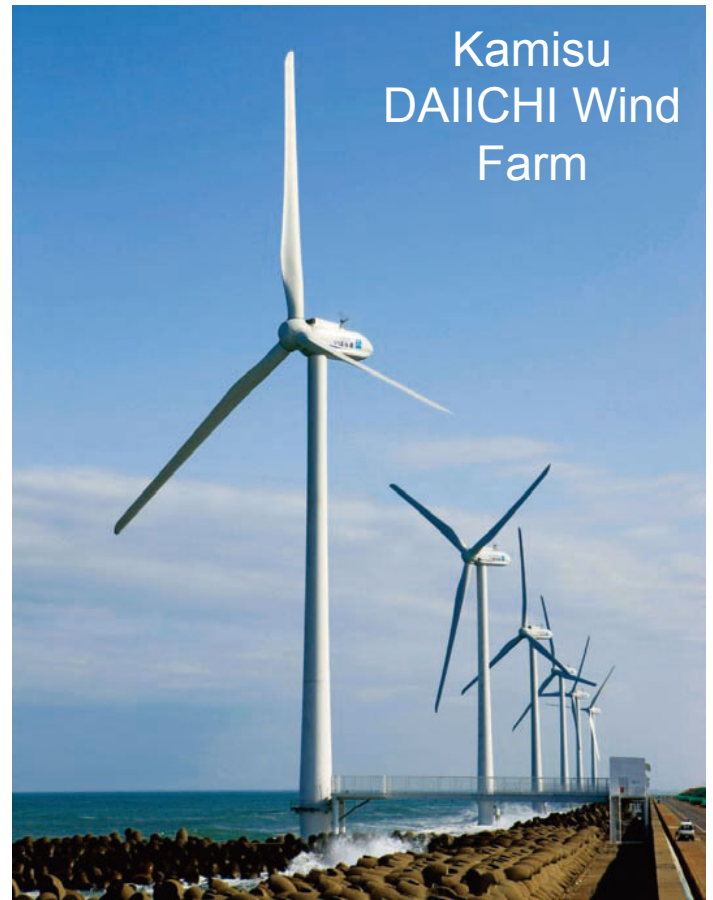
Increasing sizes lead to increasing mass & increasing exponents (2.5+)
once gravity loads start to dominate







SCD 3.0



Kamisu
DAIICHI Wind
Farm



SCD 6.0



Hitachi
2.0/80

Rotor size trends

Larger turbines mean more energy captured

Increased MW reduces “plant” & “utility-integration” costs

Next great frontier: “extreme-scale” off-shore wind turbine systems

Reduce the rotor mass and satisfy tower clearance requirement

Early evaluations of new wind turbine concept

Pre-Aligned Concept

Bio-Inspiration



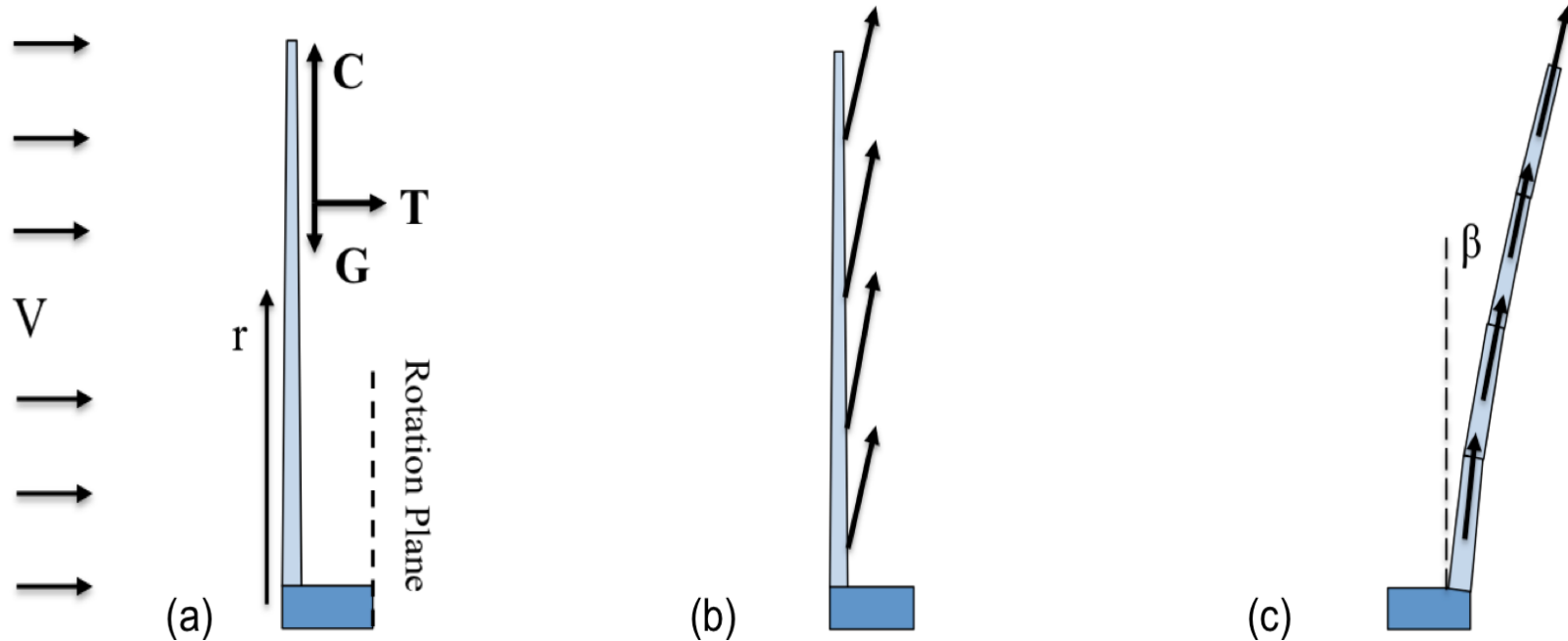
Fix load alignment to reduce cantilever moments

Wind Turbine Forces

Conventional

vs.

Load-Aligned



Load combination of centrifugal (C), gravity (G), and thrust (T) aligned along the blade path via downwind coning

Method & Test Conditions

Methodology

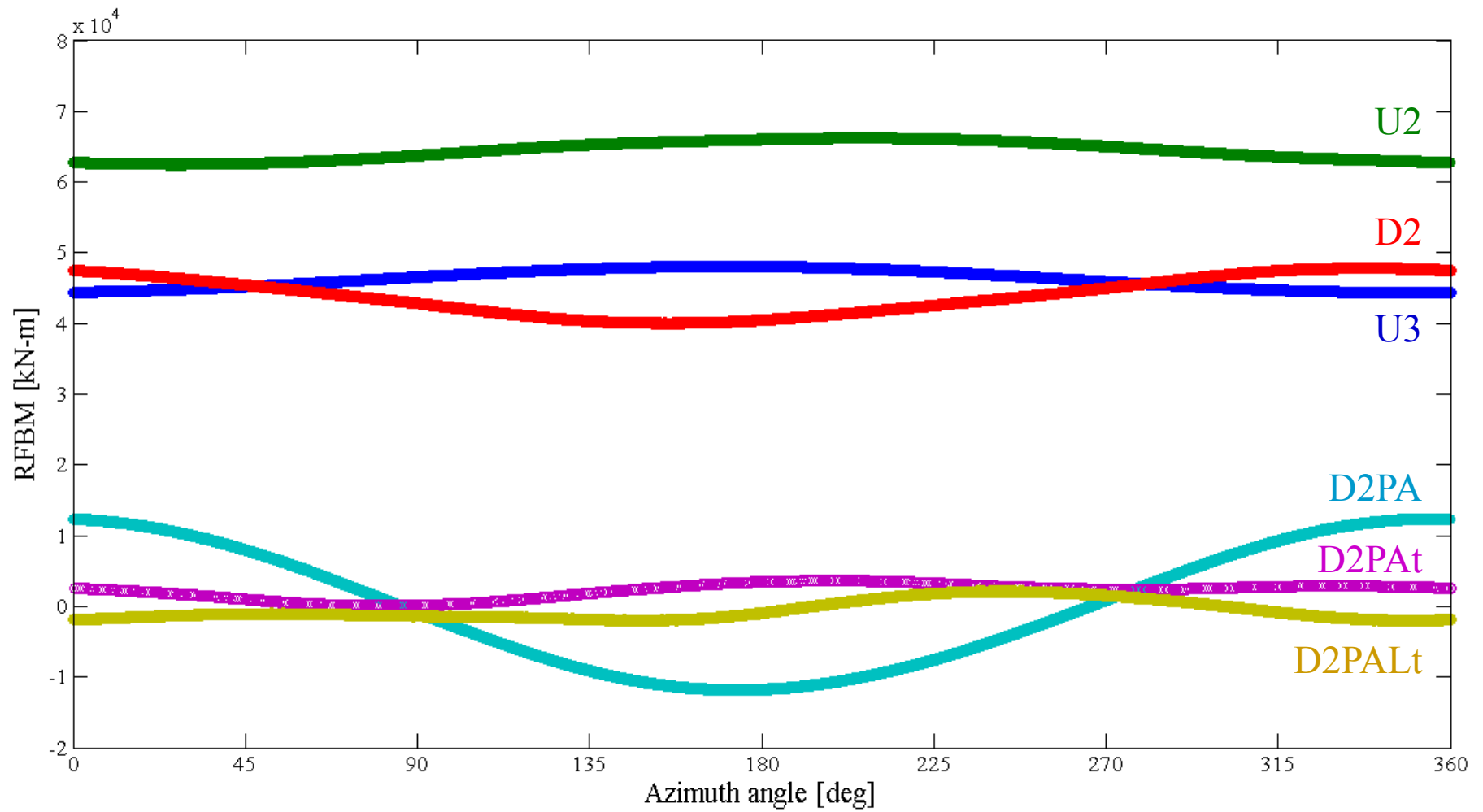
- Aeroelastic simulator FAST, an open source code developed at NREL, is employed to predict loads acting on HAWT blades
- Reference turbine is Sandia 13.2 MW upwind turbine with 100 m blades
- Damage equivalent loads (DEL) of the blades, calculated by MLife code, are used to address impacts of different designs on fatigue

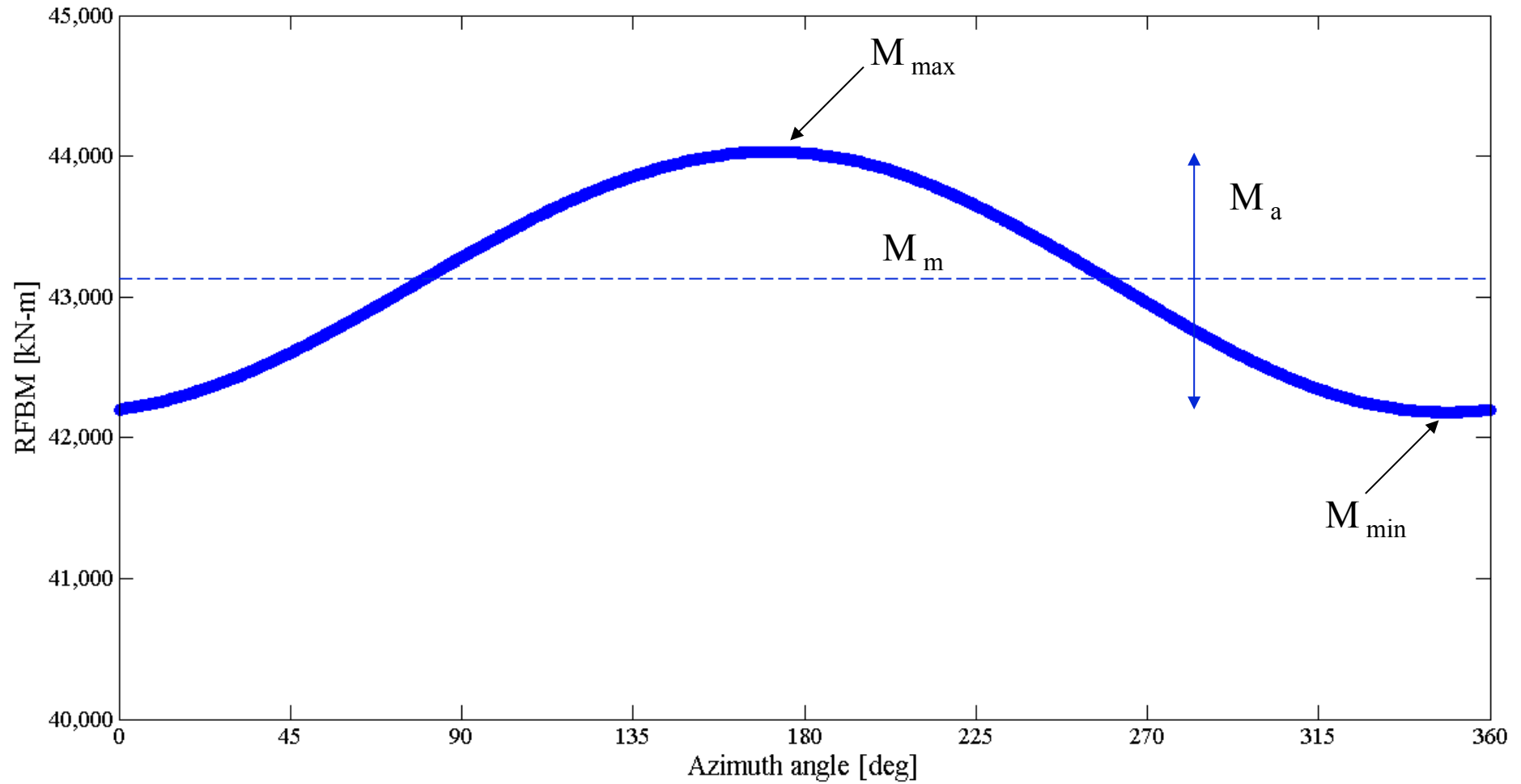
Sandia 13.2 MW Reference

- Rated wind speed $V_{\text{rated}} = 11.3 \text{ m/s}$
- Blade: SNL100-00 (117 Mg)
- Conventional design: U3, U2, D2
- Pre-aligned design: D2PA, D2PAL
- Modify Drivetrain and control system
- Turn on pitch and variable-speed controllers
- Turn off tower shadow and potential flow
- Calculate damage equivalent loads (DELs)

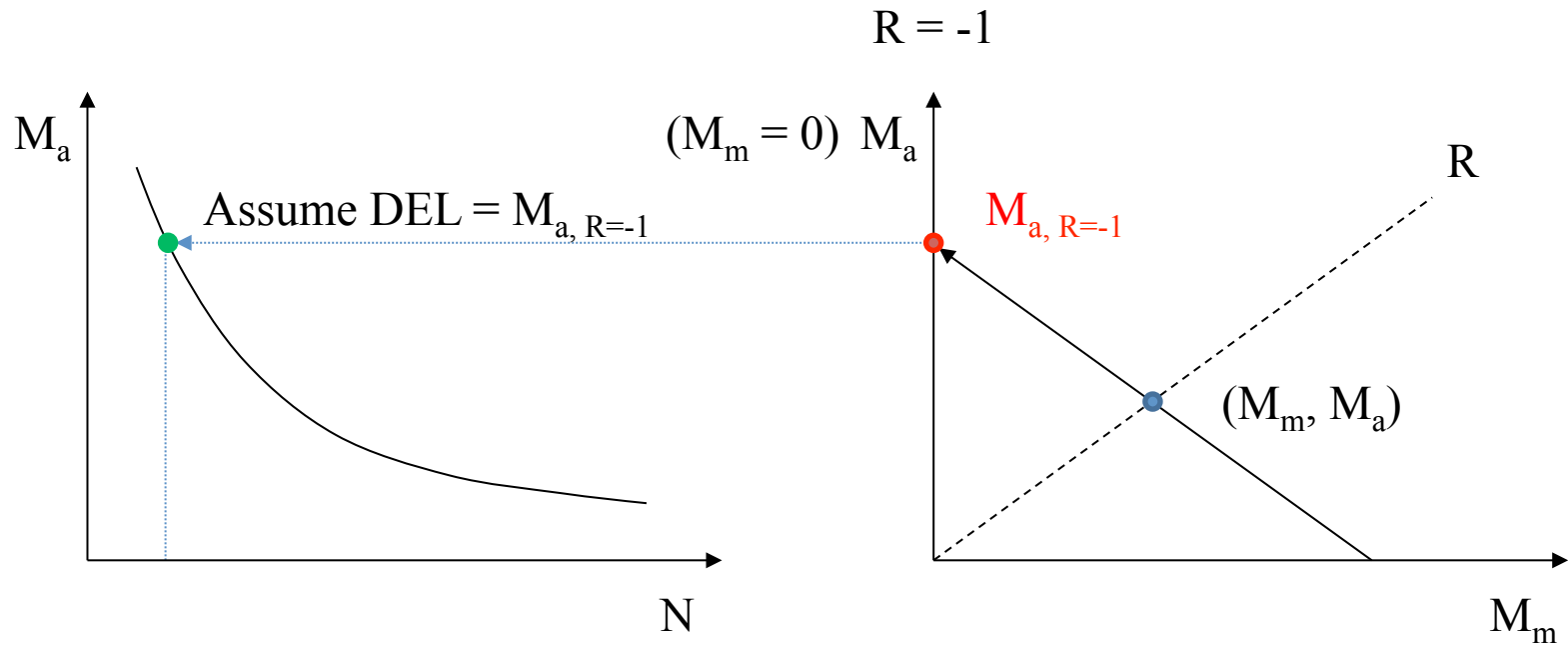
Case parameters and main outputs in FAST Simulation

Case	Blade Mass (Mg)	Rotor Mass (Mg)	Cone (deg)	α (deg)	Teeter	ω (rpm)	Cp (-)	λ (-)
U3	114.2	342.6	-2.5	0.0	No	7.44	0.459	7.06
U2	114.2	228.4	-2.5	-1.8	No	8.93	0.458	8.47
D2	114.2	228.4	2.5	-1.8	No	8.93	0.458	8.47
D2PA	114.2	228.4	17.5	-1.8	No	8.93	0.418	7.90
D2PA _t	114.2	228.4	17.5	-1.8	Yes	8.67	0.388	7.86
D2PAL _t	125.6	251.2	Stretch blade by 10%			8.93	0.395	8.93





M-N Curve + Goodman Diagram



$$M_a = M_u \times N^{(-1/m)}$$

$$R = \frac{M_{\min, 1 \text{ cycle}}}{M_{\max, 1 \text{ cycle}}} = \frac{M_m - M_a}{M_m + M_a}$$

Where,

M_a Amplitude moment in one load cycle

M_u Ultimate moment of the blade

N Allowable cycles to failure

m Slope of the curve

$M_{\min, 1 \text{ cycle}}$

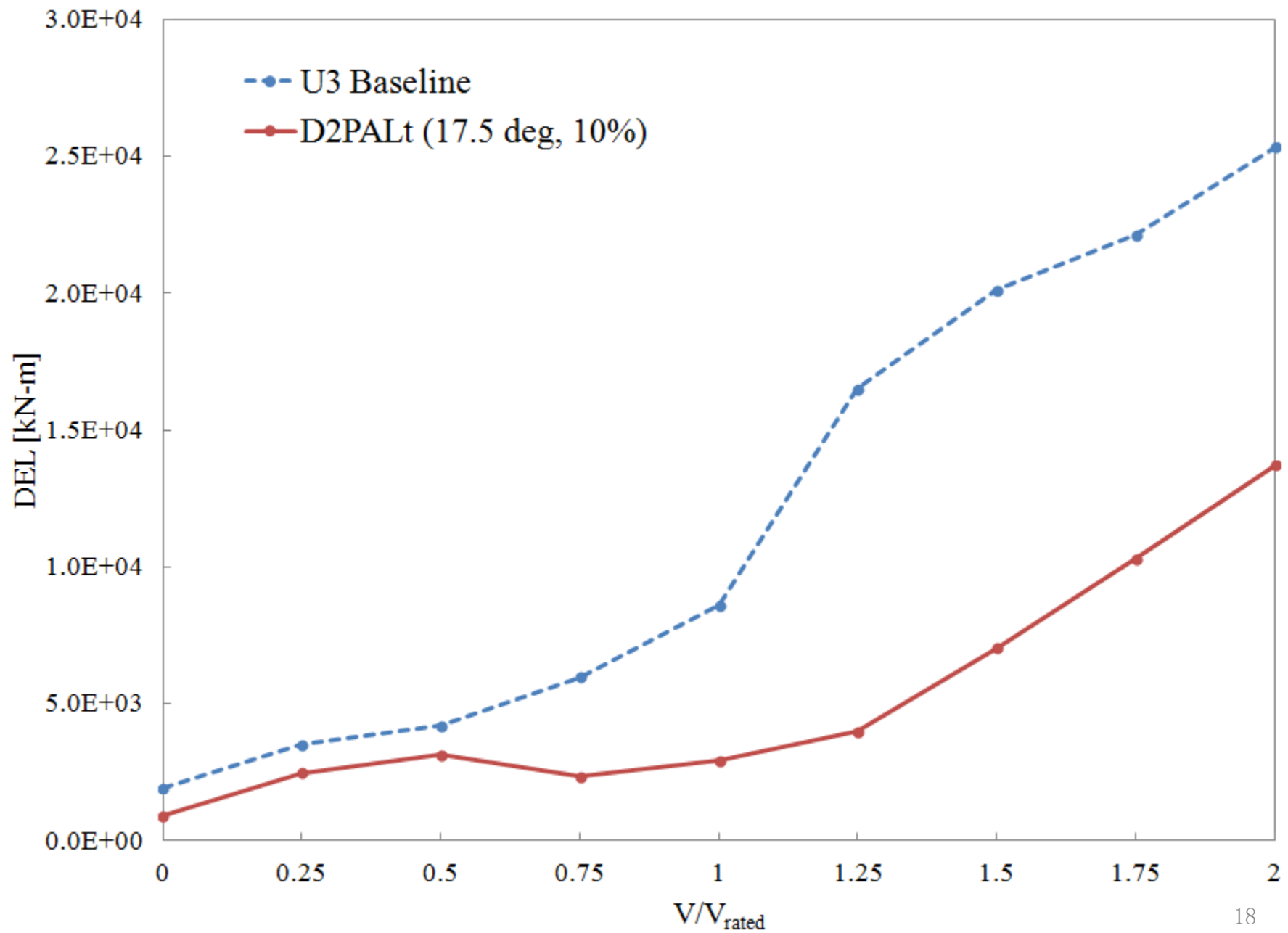
Minimum moment in one load cycle

$M_{\max, 1 \text{ cycle}}$

Maximum moment in one load cycle

Case parameters and main outputs in FAST Simulation

Case	Rotor Mass (Mg)	Cone (deg)	α (deg)	Teeter	ω (rpm)	Cp (-)	Pwr (MW)	RFBM (kNm)	DEL (kNm)
U3	342.6	-2.5	0.0	No	7.44	0.459	13.20	4.62E4	8.84E3
U2	228.4	-2.5	-1.8	No	8.93	0.458	13.20	6.44E4	3.79E4
D2	228.4	2.5	-1.8	No	8.93	0.458	13.20	4.39E4	1.73E4
D2PA	228.4	17.5	-1.8	No	8.93	0.418	11.09	155	2.01E4
D2PA _t	228.4	17.5	-1.8	Yes	8.67	0.388	10.29	606	2.85E3
D2PAL _t	251.2	Stretch blade by 10%			8.93	0.395	13.20	-581	3.41E3



CONCLUSIONS

Steady-state analysis of D2PA allows substantial reduction in flapwise bending moment for 13.2MW wind turbine blades at rated wind condition

Stretching blade length by 10% can make up the power losses

Pre-aligned design has lower DELs at different steady wind speeds than conventional three-bladed design, but it has two blades that requests rotor running at a higher rpm

Much more work needed to determine relative feasibility for force-aligned downwind systems

Tower shadow

Turbulent wind condition

Control system

IEC standard tests

SNL100-02 blades



Question and Comment

Manufacturer & Model		Year	Commercial Availability	Location	Rated Power (MW)	Blade Number	Rotor Diamter (m)	Comments
Smith-Putnam		1941	Prototype	Castleton, VT	1.25	2	53	First MW wind turbine. 1100 hrs. Blade failure.
GE MOD-1		1979	Prototype	Howard Knob, NC	2	2	61	World's second multi-MW wind turbine. Sponsored by DOE and administered by NASA. Operated at least 18 months but full operating history is unknown.
Hamilton-Standard WTS-3		1981	Prototype	Sweden	3	2	78	Sucessfully operated for 11 years.
Hamilton-Standard WTS-4		1982	Prototype	Wyoming	4	2	79.2	World record for power output for over 20 years.
GROWIAN I		1983-1988	Prototype / FAILURE	Germany	3	2	100	The most famous, most discussed and criticised German federal research project.
Wind Turbine Company WTC-1000		Around 2000	Unknown / 250, 500kW Prototype	Colorado / California	1	2	54.3	A modern update of Smith-Putnam. Compared to 3-blade upwind ones, head weight reduces by one-half and manufacturing costs reduce by one-third.
Aerodyn / Ming Yang	SCD 3.0	2011	Available	South China Sea	3	2	110	Off-shore. Designed by Aerodyn and manufactured by Chinese licensee Ming Yang.
	SCD 6.0	2013	Prototype	China	6.5	2	140	
	SCD 8.0		Prototype in Development		8	2	168	
Carter Wind Energy			Planned		10-50	2		Scale-up 300-500kW products.
Hitachi HTW 2.0/80		~2010	Available	Fukushima, Japan	2	3	80	Experimental off-shore floating wind farm project begins in 2012. In second term, 7-MW wind turbines will be added between 2013 and 2015.
Hitachi HTW 5.0/126		2013-2015	Prototype in Development	Kamisu City, Japan	5	3	126	A demonstration prototype is under construction.
Nautica Windpower AFT		2017	Concept / Prototype			2		Advanced Floating Turbine. Digital prototype. A 1/3-scale version with a 35- m rotor is expected by 2013.
Subaru 80/2.0			Available		2	3	80	Manufactured by Fuji Heavy Industries. Designed for strong wind. Special attention is being given to withstand the heavy typhoon in Japan.
SWAY			Prototype	Norway	2.5-12	3		NREL is collaborating with SWAY. The SWAY 1/5 scale prototype has a 13-m rotor on a 29-m tower, with a large portion of the tower beneath the ocean surface.

Planned Simulation Progress

