

Strategies for Managing Cool Thermal Energy Storage with
Day-ahead PV and Building Load Forecasting at a District Level

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Abstract

In hot climate areas, the electrical load in a building spikes, but not by the same amount daily due to various conditions. In order to cover the hottest day of the year, large cooling systems are installed, but are not fully utilized during all hot summer days. As a result, the investments in these cooling systems cannot be fully justified.

A solution for more optimal use of the building cooling system is presented in this dissertation using Cool Thermal Energy Storage (CTES) deployed at a district level. Such CTES systems are charged overnight and the cool charge is dispatched as cool air during the day. The integration of the CTES helps to downsize the otherwise large cooling systems designed for the hottest day of the year. This reduces the capital costs of installing large cooling systems. However, one important question remains - how much of the CTES should be charged during the night, such that the cooling load for the next day is fully met and at the same time the CTES charge is fully utilized during the day.

The solution presented in this dissertation integrated the CTES with Photovoltaics (PV) power forecasting and building load forecasting at a district level for a more optimal charge/discharge management. A district comprises several buildings of different load profiles, all connected to the same cooling system with central CTES. The use of forecasting for both the PV and the building cooling load allows the building operator to more accurately determine how much of the CTES should be charged during the night, such that the cooling system and CTES can meet the cooling demand for the next day. Using this approach, the CTES would be optimally sized, and utilized more efficiently during the day. At the

same time, peak load savings are achieved, thus benefiting an electric utility company.

The district presented in this dissertation comprises PV panels and three types of buildings – a mosque, a clinic and an office building. In order to have a good estimation for the required CTES charge for the next day, reliable forecasts for the PV panel outputs and the electrical load of the three buildings are required. In the model developed for the current work, dust was introduced as a new input feature in all of the forecasting models to improve the models' accuracy. Dust levels play an important role in PV output forecasts in areas with high and variable dust values.

The overall solution used both the PV panel forecasts and the building load forecasts to estimate the CTES charge for the next day. The presented method was tested against the baseline method with no forecasting system. Multiple scenarios were conducted with different cooling system sizes and different CTES capacities. Research findings indicated that the presented method utilized the CTES charge more efficiently than the baseline method. This led to more savings in the energy consumption at the district level.

Strategies for Managing Cool Thermal Energy Storage with Day-ahead PV and Building Load Forecasting at a District Level

Abdullah Alfadda General Audience Abstract

In hot weather areas around the world, the electrical load in a building spikes because of the cooling load, but not by the same amount daily due to various conditions. In order to meet the demand of the hottest day of the year, large cooling systems are installed. However, these large systems are not fully utilized during all hot summer days. As a result, the investments in these cooling systems cannot be fully justified.

A solution for more optimal use of the building cooling system is presented in this dissertation using Cool Thermal Energy Storage (CTES) deployed at a district level. Such CTES systems are charged overnight and the cool charge is dispatched as cool air during the day. The integration of the CTES helps to downsize the otherwise large cooling systems designed for the hottest day of the year. This reduces the capital costs of installing large cooling systems. However, one important question remains - how much of the CTES should be charged during the night, such that the cooling load for the next day is fully met and at the same time the CTES charge is fully utilized during the day.

The solution presented in this dissertation integrated the CTES with Photovoltaics (PV) power forecasting and building load forecasting at a district level for a more optimal charge/discharge management. A district comprises several buildings all connected to the same cooling system with central CTES. The use of the forecasting for both the PV and the building cooling load allows the building operator to more accurately determine how much of the CTES should be charged during the night, such that the cooling system and CTES can meet the cooling demand for the next day. Using this approach, the CTES would be optimally sized and utilized more efficiently. At the same time, peak load is lowered, thus benefiting an electric utility company.

To my parents

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Chapter 1 Introduction

1.1 Background

Electrical demand is increasing rapidly every year worldwide since 1974. The average growth in electrical energy production increased by 3.3 % annually worldwide between 1974 and 2016 [1]. Countries in the Organization for Economic Co-Operation and Development (OECD) have an average growth rate of 3.0% from 1974 to 2000, while non-OECD countries have an average rate of 4.3% for the same period of time. The electrical energy production growth rate could reach higher rates in certain countries, especially when there is no load management program coupled with the absence of energy storage systems.

For example, in hot countries this growth of electrical production is mainly driven by the rapid installation of HVAC systems and chillers in both homes and in commercial buildings, without a good load management coupled with the absence of storage systems. The peak production is only utilized for a few hours during the summer peak to meet the cooling load at the middle of the day.

Renewable energy resources represent 24% of the total electrical energy generated worldwide as of 2016 [2], and the solar share is only 1.2%. Many countries around the world have plans to invest in large-scale renewable energy projects. However, the main issue with these resources is the uncertainty in their output power, which can result in an overall power grid instability. With respect to solar power, this can be caused by the fluctuation in many meteorological variables, such as cloud cover, dust level, temperature and wind speed. Thus, solar PV output forecasting is of great importance for building operators, allowing them to optimally set demand response schedules.

Thus, a good way to fully exploit renewable energy resources is to combine it with storage systems. A commonly used storage medium is batteries; however, batteries are still expensive and thus would be hard to deploy them on a large scale. Other storage techniques include hydroelectric storage which are good for large scale projects, but would need a special geography to store water in the reservoir in order to discharge it when energy is needed.

Thermal Energy Storage (TES) is one way to store energy in the form of heat and discharge it when needed. Cool Thermal Energy Storage (CTES) is the another version of TES, it simply charges a tank during the off-peak period with cold water or ice (other materials have also been deployed), then this cold water or ice is discharged as a cold air during on-peak hours to cool down a building. CTES is very beneficial, especially in some applications, such as when the electricity prices are more expensive during the on-peak hours compared to the off-peak hours. In that case, CTES is charged during the off-peak hours (usually at night) and discharged during the on-peak hours, the goal here is to save in the overall building's electricity bill, by using low price electricity at the off-peak hours to offset high price electricity at the peak hours. CTES is also beneficial when the peak cooling demand is much higher than the average cooling load (common in hot countries). In this case, a chiller (installed in a building to meet partial building's peak cooling load) is used in combination of the CTES. By applying this setup, savings in the installation cost can be achieved by installing a smaller chiller system. Other useful CTES applications are discussed in more detail in the literature review chapter.

1.2 Objective

In most applications in the literature, CTES is fully charged during the off-peak hours (usually at night) regardless of the expected load for the next day. So, in the case that the cooling load is low for the next day, CTES is already fully charged, even though it might not be fully utilized. Thus, some energy is wasted, because the expected load for the following day and storage needed to serve the peak load are not matched.

The objective of this work is to develop PV output and building-level load forecasting methods that can be integrated for determining optimal charge and discharge strategies of CTES at a district level. The work is demonstrated using a case study of a district that contains different types of buildings, each one with its unique load profile, connected to the same central chiller system. This central chiller system has a CTES, which could serve as a partial storage system. Different types of buildings are considered in this study to demonstrate the usefulness of the proposed load forecasting methods, the characteristics of different load profiles are discussed in the subsequent chapters. To demonstrate the usefulness of the proposed PV forecasting methods, it is assumed that each one of these buildings has a PV panel system integrated with it. These load and PV forecasting methods are then incorporated into determining optimal charge/discharge strategies of the central CTES, which works together with a central chiller system during peak cooling demands. **Figure 1.1** shows the overall configuration of the district-level system.

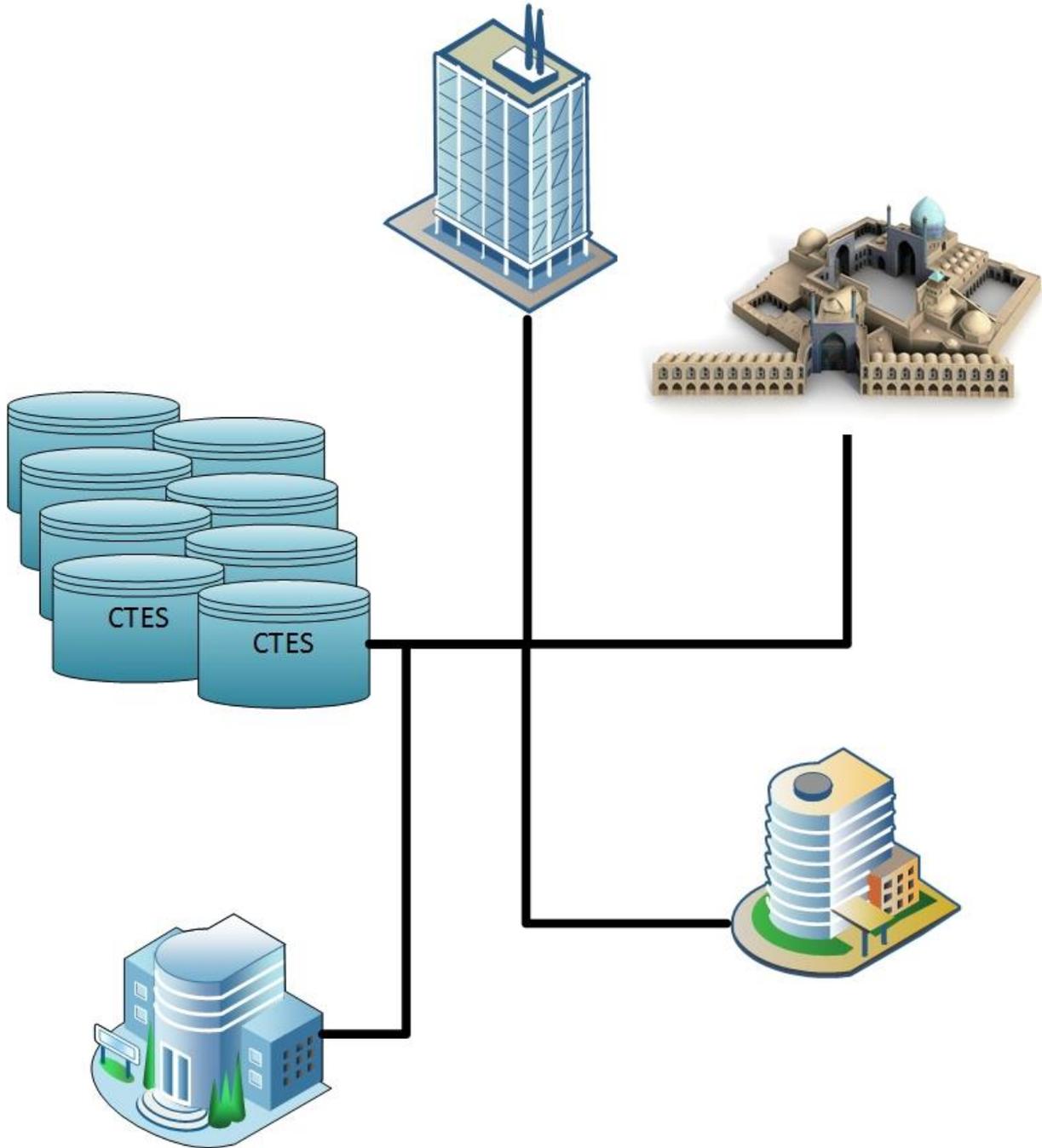


Figure 1.1 Overall configuration of the district-level system.

The demonstration case study starts by generating forecasts for all three building loads for the next day, as well as for the PV panels associated with each building. Once the forecasts are calculated, an estimate for the CTES charge for the next day is generated. This estimate takes into consideration the chiller maximum capacity and the

peak cooling demand for all buildings for the next day. For example, if the next day cooling load is high, the CTES is fully charged to meet the cooling load of all three buildings. Similarly, if the peak load for the next day is not high, such that it could be met by the chiller capacity, then CTES is charged or just partially charged, and thus an overall saving in the energy bill is achieved.

The proposed work involves the following tasks:

1. Solar PV forecasting – Day-ahead:

- a. Weather data collection for the proposed location, which includes all weather variables (i.e. Ambient temperature, cloud cover, wind speed, wind direction) and the dust at the target location, as the target location has high dust values all over the year.
- b. Develop the Neural Networks/Support Vector Regression/ Decision Tree and k-Nearest Neighbor models for the hour-ahead PV output forecasting.
- c. Data collection for the PV panels at the target location.
- d. Extend the Neural Networks/Support Vector Regression/ Decision Tree and k-Nearest Neighbor models for the day-ahead PV output forecasting.
- e. Evaluate and tune all the models.

2. Building Load forecasting – Day-ahead:

- a. Weather data collection for the target location, including all weather variables and the dust for the target location, as the target location has frequent dust storms. Dust has an impact on the available solar radiation intensity on the ground, hence the building load.
- b. Data cleaning for all of the data collected above. Cleaning the data for the buildings includes removing the days that has zero readings due to error in the meter reading. Also, interpolation for some of the missing readings during the day.
- c. Develop the building load forecasting models.
- d. Evaluate the building load forecasting models, and tune/optimize the model.

- e. Compare the performance of the different developed load forecasting models.
- 3. Control strategy for the CTES:**
- a. Develop a methodology for control of CTES.
- 4. Evaluate the proposed methods using a case study:**
- a. Data collection for the three target buildings from the electric utility company.
 - b. Integrate the CTES with the PV output and the building load forecasting models and estimate the effectiveness of the forecasting models and the savings due to the use of CTES.

1.3 Contributions

The main contributions of this work are listed below:

- a. Combining the CTES with the building load/PV output forecasting to estimate the required CTES charge for the next day.
- b. Applying CTES at the district level combined with building load forecasts and PV forecasts.
- c. Adding the dust as a feature for the PV and building load forecasts alongside the other weather features.
- d. Applying the developed forecasting techniques on different building types with different building-level load profiles (i.e., mosque, clinic and office building). Comparing different forecasting techniques.

Chapter 2 Literature Review

This chapter introduces the past research work that has been conducted in the relevant areas. First subsection discusses the building load forecasting work in the literature. Second subsection discusses the solar forecasting work conducted. The last three sections talk about the CTES applications and its control strategies.

2.1 Building Load Forecasting

Building load forecasting has been also studied recently in the literature. Similar to the solar irradiance the building load forecast is also dependent on the weather factors mentioned earlier. Moreover, the building load might be affected also by the solar irradiance components (i.e. GHI, DNI and DHI) that's mainly because by being under the irradiance the building envelope will absorb the heat generated by these irradiance components. Literature survey about residential building load forecasting could also be found here [3]. In [4] they have used deep learning to forecast the building load, they applied their model on residential building with four years data and 1-minute resolution. This high resolution data might not be always available, or might not be available at all times of the day, in [5] they used two reinforcement learning techniques incorporated with Deep Belief Network (DBN) to train the model without the need for labelled data. Neural network has also been used in the building load forecasting, in [6] they used a three layer feed forward neural network to estimate the building load, with a forecast horizon of 24-hour-ahead. In [7] they studied the grid level forecasting problem with the addition of consumer behavior by the addition of clustering algorithms to cluster groups of similar behavior together. In [8] they further analyzed the behavior to residential customers, based on the mixture model they used for clustering, and the data they have, they show that 10 different behavior profiles are available under the tested grid data. In [9] they studied the load forecasting problem on an event scale using 15 minutes data, the best performing machine learning model was the neural networks. In [10] they used occupancy data to model the building load, however, the occupancy sensors might not be available

always, so the occupancy data were estimated indirectly from car parking in the tested site. In [11] they studied the relationship between the load and the variables that affect the load, such as temperature and calendar days, whether these days are work days or weekends, they concluded that the a good temperature forecast is an important factor to the load forecast. In [12] they introduced a short term load forecast on the distribution level (i.e. the feeder level).

2.2 Solar Forecasting

Solar irradiance is directly dependent on multiple weather factors, mainly cloud cover, humidity and visibility, besides other parameters, such as ground albedo. Thus, better forecasts of these weather factors would result in an improved solar irradiance model. However, in some areas that have low cloud cover, the solar forecasts would be more affected by the remaining factors. Moreover, areas like Arabian Peninsula and North Africa are exposed to frequent dust storms and high aerosols index all over the year. Thus, developing a solar irradiance forecasting model that incorporates the dust phenomena is of a great importance for such areas.

Some work has been carried out to investigate the relationship between the PV module efficiency and dust accumulation over PV panels [13, 14]. In [15], authors studied the optimum cleaning frequency for the PV module to improve module efficiency. In [16] authors have compared the cost and performance of different PV cleaning techniques.

The other main concern due to the presence of dust in the air is the increased uncertainty in solar radiation forecast. Moreover, the forecasted Aerosol Optical Depth (AOD) values are not fully correlated with the ground-based AOD measurement. In [17] authors compared AErosol RObotic NETwork (AERONET) data with European Center for Medium-Range Weather Forecasts (ECMWF) readings across multiple sites around the world, the average correlation coefficient found to be 0.77 for dust areas. Thus, uncertainty in forecasted AOD values would lead to a lower solar forecasting accuracy,

especially in desert areas, where cloud-free environments are dominant and dust particles have frequent presence in the air.

Machine learning techniques have been widely used in solar irradiance forecasting. Artificial Neural Networks (ANNs) are the most widely used techniques for solar forecasting [18], which have been applied to both short-term [19, 20] and long-term forecasting [21]. ANN with more than one hidden layer is usually referred to as Multilayer Perceptron (MLP). k-Nearest Neighbors (kNN) has also been widely used in the literature, it has been applied to predict intra hour irradiances [22] , and to generate probabilistic forecasts [23]. Other machine learning methods have also been applied to solar forecasting, such as Support Vector Regression (SVR) [24] , random forests [25] and Lasso [26] . Machine learning techniques have also been used in solar forecasting with AOD as input, in [27] they used six thermal channels from SEVERI satellite images to predict the aerosols at 550 nm, then fed this prediction to ANN model to improve the Global Horizontal Irradiance (GHI), Direct Normal Irradiance (DNI) and Diffuse Horizontal Irradiance (DHI) forecasts.

Newer techniques such as deep learning has also been implemented in a number of time series forecasting models [28-30] , it has shown a superior accuracy compared to other machine learning methods. It was implemented to estimate the building energy consumption[4], predict the wind speed [31] and forecast the solar irradiance [32]. Convolutional version of deep learning has been implemented to predict the Photovoltaic output power [33] using both deterministic and probabilistic approaches. In [34] they implemented Long Short Term Memory (LSTM) version of deep learning to forecast the PV output power for the next day. Convolutional LSTM version was used to predict the short-term precipitation based on spatiotemporal data sequence [35]. Spatiotemporal data were also studied using other methods such as Kriging [36] and applied to solar irradiance forecasting.

Solar forecasting time horizon can be categorized into short-term, medium-term and long-term forecasting. In the short-term forecasting the predicted solar irradiance value

falls within the next few hours, multiple short-term models have been developed in the literature [37-39]. The medium-term forecasts generate predictions that cover the span of the next few days [40, 41]. Lastly, long-term forecasts predict the solar irradiance for the next few months to years [42].

2.3 District Level Cool Thermal Energy Storage

In [43] they studied the application of CTES on large scale, they simulated distributed CTES over semiarid, AZ, and estimated how much CTES capacity is required. In [44] they provide a comprehensive literature review for heat/cool thermal energy storage.

2.4 Cool Thermal Energy Storage Combined with Forecasts

In [45] they proposed a day-ahead scheduling algorithm of HVACs combined with CTES while considering errors of wind energy forecasts. In [46] they proposed optimal control strategy for based on Sequential Quadratic Programming (SQP) for CTES applied for commercial buildings. In [47] they proposed a Hybrid Model Predictive Control (HMPC) for HVACs in residential buildings combined with CTES. In [48] they studied the application of CTES and off-grid solar PV in the industry sector to reduce the peak demand.

2.5 Cool Thermal Energy Storage

Energy can be saved in many forms. It can be stored chemical form such as batteries, or mechanical form as in Hydroelectric storage. Or it can be stored in thermal form as in Cool Thermal Energy storage. In general, the main goal of energy storage is to lower the gap between energy consumption and energy generation, mainly by shifting the temporal difference between them. In this subsection an overview about the Cool Thermal Energy Storage (CTES) is given, the associated control strategies and the benefit of installing CTES in buildings. CTES is a storage system that is usually used

when the peak cooling loads in a building are high and can not be met by the current cooling system. It is also often used in places where the cooling demand is highly variable during the day, and the installation of high capacity cooling system is not economically feasible, since the peak capacity of the cooling system is only used part of the day. Moreover, CTES is often used in places where the electricity pricing is variable over the day, the prices in this case are high during the on-peak time during the day, while the prices are lower at the off-peak times usually during the night, hence, using a CTES to charge during off-peak hours would result in overall energy saving for a particular place or building.

CTES is suitable mostly as in the following cases as discussed in [49]:

1. The maximum cooling load of the building cannot be met using the existing chiller capacity, so CTES is installed to charge during the low demand periods, then discharge during the maximum cooling demand period.
2. The electricity prices are variable over the day, and the charges are higher during the building peak hours, while the load is mostly cooling load, hence, charging the CTES during the off-peak hours (usually at night), then discharging the cool air during the on-peak hours, to avoid running the high load during the peak hours, which would result in money savings.
3. The electric power that could be used in the building cannot exceed a certain limit, hence, another energy resource other than electricity should substitute the shortage in the energy. The CTES is a good option in the case that the building load consists mainly of chillers.
4. A backup cooling system is desirable in the site, so in the case of the chiller failure, there is another source of cooling during the failure of the main chiller or cooling

system. This is mainly beneficial for critical systems such as data centers or any other critical applications.

2.5.1 CTES Control Strategies

The control strategies for the CTES could be subdivided into two main control schemes, the full-storage system and the partial storage system. Below would be an explanation for each one.

2.5.1.1 Full-Storage System

The Full-Storage system is usually easy to control, it operates by fully charging the CTES during the off-peak hours, and then fully discharge it during the on-peak hours, the full storage could meet the full cooling loads needed for a certain period of time. The full storage is useful in application where the prices of the energy are higher than the prices of the off-peak hours. Also, it is useful in applications where the cooling demand is highly variable during the day, where installing a high capacity chiller to operate for a short period of time is not economically feasible, hence, the excess in the high temporal cooling demand will be met by the CTES. The full-storage system control strategy is shown in **Figure 2.1** [50].

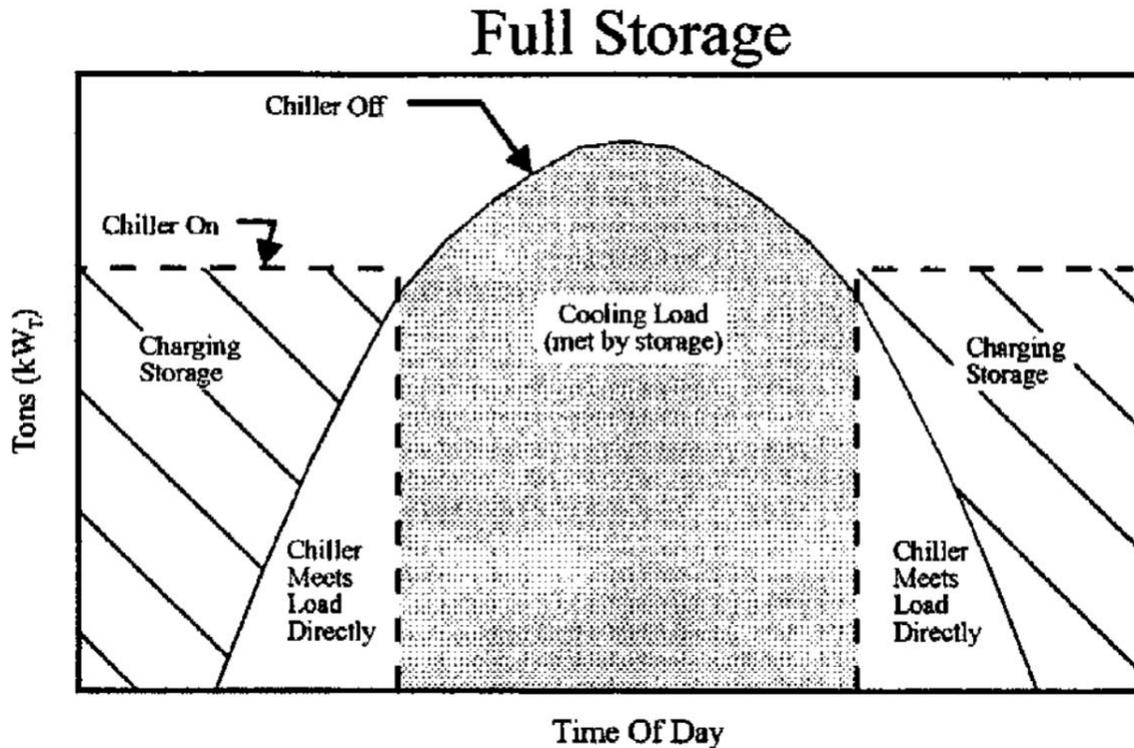


Figure 2.1 Full storage system for CTES [50]

2.5.1.2 Partial-Storage System

In partial-storage systems part of the cooling demand during the on-peak is met by the existing chiller and the other part is met by the CTES. It can mainly operate in two strategies. First one is the Chiller-Priority system, where in this case the chiller operates at its maximum capacity to meet the cooling loads during the on-peak periods, and the excess cooling load that cannot be met using the chiller maximum capacity will be compensated using the CTES. This approach is usually attractive in applications where the maximum chiller capacity cannot meet the maximum cooling load, and the peak load is much higher than the average load, the control scheme for the chiller-priority scheme is shown in **Figure 2.2**. The second partial storage control strategy is the storage-priority control scheme, in this case, the chiller operates at reduced capacity during the on-peak period, while the remaining cooling load is met by the CTES, the control strategy for the storage-priority is shown in **Figure 2.3** [50].

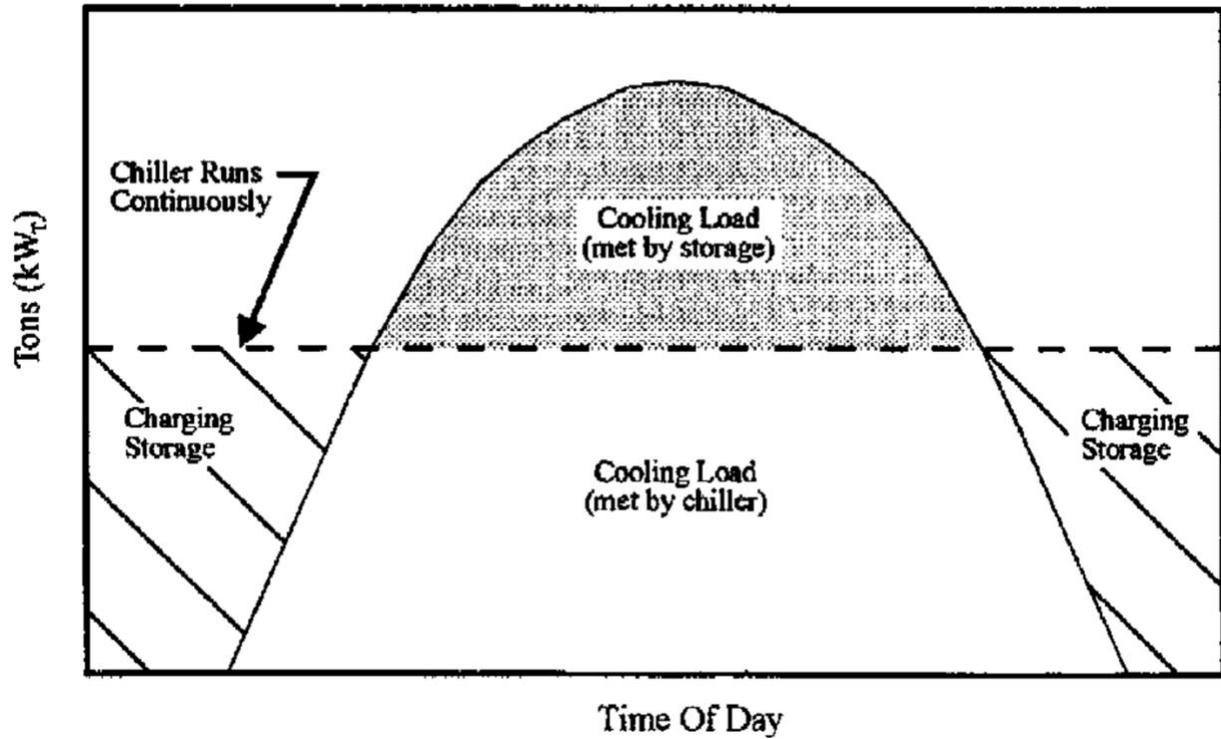


Figure 2.2 Chiller priority control scheme for the CTES [50].

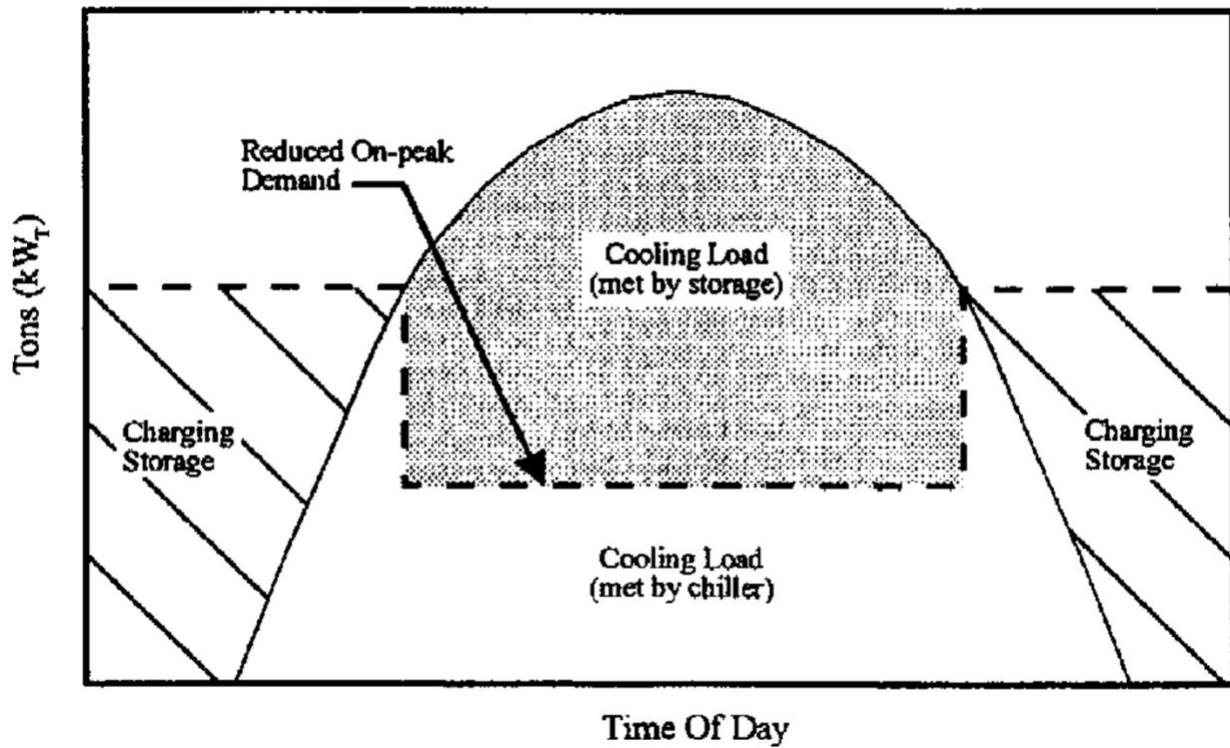


Figure 2.3 Storage priority control scheme for the CTES [50].

2.6 Knowledge Gap

The majority of the published work in the building-level load forecasting when combined with the CTES focused mainly on full storage systems. While most of the work conducted in the partial CTES focused mainly on the control strategies for the CTES, that's how to control the CTES flow during the day, while assuming the CTES is fully charged during the night regardless of the building load forecast. Moreover, the published building load forecasting work takes into consideration most of the weather variables, while ignoring the dust when building the forecasting model, in this work the dust is added to the building forecasting model. In addition, the proposed building load forecasting model is implemented at a district level, while most of work on the literature focused on a single building or on a distribution and feeder level. Finally, the PV panel system is added to the entire proposed model, combined with the building load forecasts and the CTES, which has never been conducted in the literature.

Chapter 3 Methodology

In this section the methodology for the proposed work is discussed. At first an overview of the proposed work is shown. Then different machine learning techniques used in the forecasting work are summarized. The methods used in this work are multilayer perceptron, kNN, SVR and decision trees. Each of these methods is discussed in the following subsections.

3.1 Overall Framework

In this section, the framework of the proposed system is presented. In **Figure 3.1** the system flow diagram is shown. The system starts by forecasting the building load forecasts for the next day, these building are of different load profiles as shown earlier in **Figure 1.1**. At the same time, the PV power forecasts are estimated for the next day as well. Now based on these obtained forecasts for both the different buildings and for the PV panel system, an estimate for the CTES charge is calculated, such that, all the buildings cooling demand is met for the next day, during the peak demand period. In the design of the chiller that serves all the buildings (shown in **Figure 1.1**), the peak capacity of the chiller is less than the peak cooling demands, and the goal is to save in the capital costs when initially installing the chiller, since the maximum chiller capacity is only used in peak hours during only summer months, so, installing CTES will be more economically visible, taking into consideration that the energy prices during peak hours is more than the energy prices during off-peak hours. Now, if the buildings cooling load for the next day does not exceed the chiller capacity, then the CTES is not charged.

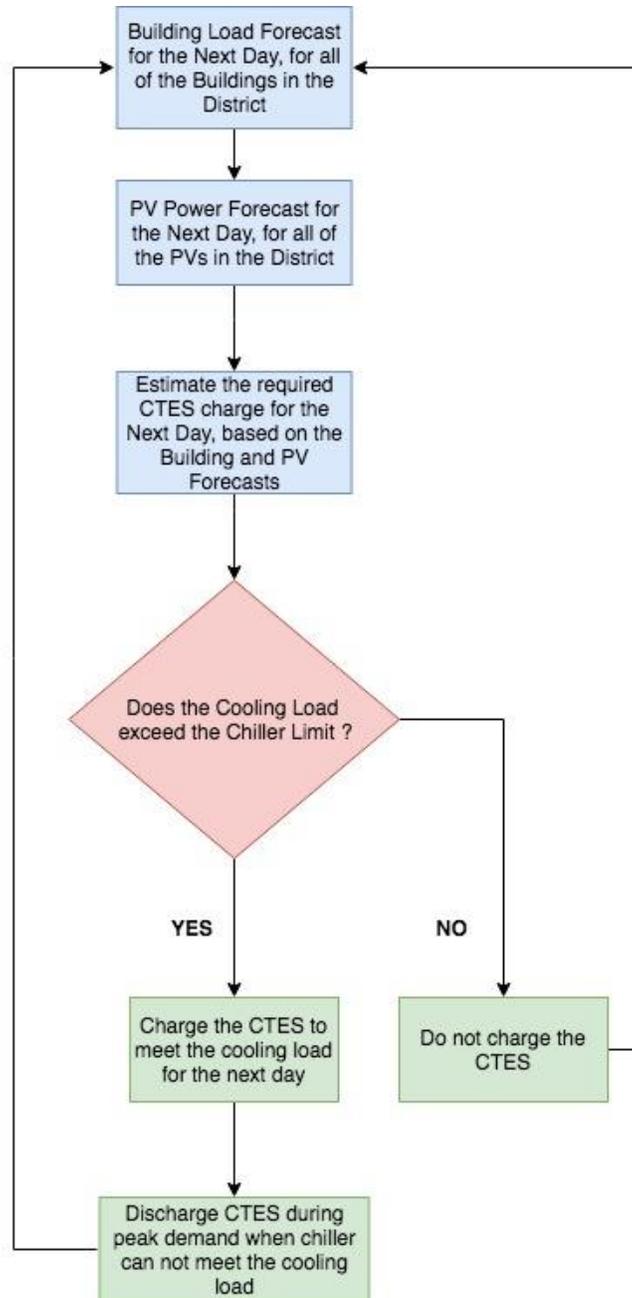


Figure 3.1 System Overview.

3.2 Forecasting techniques

3.2.1 Multilayer Perceptron

The basic component of any MLP network is a neuron. A single neuron output is calculated based on the summation of the incoming neurons values, originating from the previous layers, then multiplied by the weights on these connections and added to a bias term, finally applied to an activation function, as shown in Eq. (1). The structure of a single neuron is shown **Figure 3.2**.

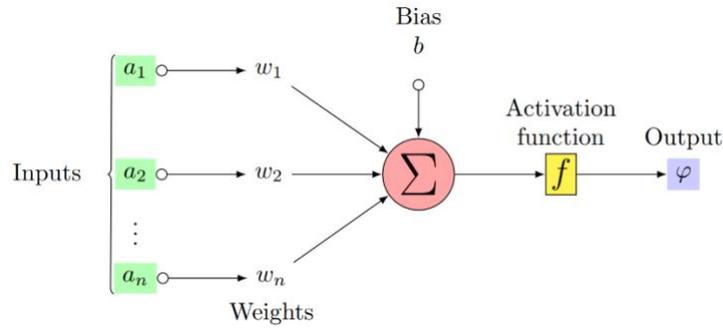


Figure 3.2 Neuron Structure

$$\varphi = f\left(b + \sum_{i=1}^n w_i a_i\right), \quad (1)$$

where b is the bias term; w_i is the weight on each connection; a_i is the value of each incoming connection; n is the total number of incoming connections for the neuron; f is the activation function; and φ is the output value. The choice of the activation function depends on the problem on hand. For time series predictions, Rectified Linear Unit (ReLU) has proved to have the best accuracy performance compared to all other activation functions. Eq. (2) shows the updated neuron output φ after applying the ReLU activation function.

$$\varphi = \max\left(0, b + \sum_{i=1}^n w_i a_i\right). \quad (2)$$

Neurons are only the building blocks of the MLP model. The basic structure of the proposed model is illustrated in **Figure 3.3**.

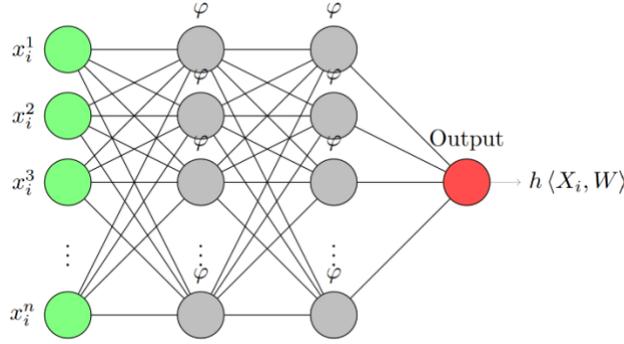


Figure 3.3 MLP Network Structure.

The first layer is the input layer (in green), which is the input data (i.e., training data) entry points to the network that will construct model parameters. Subsequent layers (in grey) are the hidden layers. The MLP network could have as many hidden layers as needed, the number of hidden layers and the structure of the network is highly dependent on the application. This work involved two hidden layers as any additional hidden layers do not contribute to the model's overall accuracy.

The input data points of the proposed model are defined as $X_i = [x_i^1, x_i^2, \dots, x_i^l]$, and their labels are y_i , where $i \in \{1, 2, \dots, n\}$, n is the total number of training data points and l is the total number features for the input data point. The output of each data point X_i is denoted as $h(X_i, W)$, where W is the set of weights on the connections between the neurons across all of the network.

After the construction of the network, the goal now is to find the optimum set of weights W , such that the error between the actual and the predicted labels values is minimized. In order to achieve this, the squared error loss function (Eq. (3)) is added at the output neuron (denoted in red as shown in Fig. 5), at which the performance of the proposed MLP model is being optimized, by comparing the ground truth labels with the predicted values, during the training phase.

$$L = \frac{1}{2} (h(X_i, W) - y_i)^2, \quad (3)$$

where $h(X, W)$ is the predicted value; y_i is the actual value; and L is the total loss. Now, in order to find the optimum W values, the gradient of the loss function L is computed with

respect to each weight on the network $w_{j \rightarrow k}$, where, j and k denote the neuron index; and $w_{j \rightarrow k}$ denotes the connection between neuron j to neuron k . So, the gradient can be expressed as shown in Eq. (4):

$$\begin{aligned} \frac{\partial}{\partial w_{i \rightarrow k}} L(w) &= \frac{\partial}{\partial w_{i \rightarrow k}} \sum_i \frac{1}{2} (h\langle X_i, W \rangle - y_i)^2, \\ &= \sum_i (h\langle X_i, W \rangle - y_i) \frac{\partial}{\partial w_{i \rightarrow k}} h\langle X_i, W \rangle. \end{aligned} \quad (4)$$

Finally, the gradient for each weight in the network is to be determined, until the optimum value for each weight is reached, i.e., the overall loss is minimized. This would be computationally expensive if classical optimization techniques, e.g., gradient decent, are used. Thus, the Adam solver [51] was selected for solving this problem, which proved to perform well on large datasets.

The structure of the implemented MLP network has seven neurons at the first hidden layer and five neurons at the second hidden layer. The number of these neurons at these different layers was selected by adding more neurons and keep tracking the Root Mean Square Error (RMSE) performance, until the error is minimized over the training data. Adding more neurons to the first or second hidden layers does not improve the model's overall accuracy.

3.2.2 Support Vector Regression

Support Vector Regression (SVR) is a supervised machine learning algorithm. It is extension of Support Vector Machines (SVM) to regression problems. It solves the following optimization problem:

$$\begin{aligned} \min_{q, \beta, \zeta, \zeta^*} & \frac{1}{2} q^t q + C \sum_{i=1}^n (\zeta_i + \zeta_i^*), \\ \text{s.t.} & \\ & y_i - q^t \phi(X_i) - \beta \leq \varepsilon + \zeta_i, \\ & q^t \phi(X_i) - y_i + \beta \leq \varepsilon + \zeta_i^*, \\ & \zeta_i, \zeta_i^* \geq 0, i = 1, \dots, n, \end{aligned} \quad (5)$$

where q is the weight vector; β is the bias term; ξ_i, ξ_i^* are the slack variables; C is a tradeoff variable for the flatness of the curve; and ε is the tolerance variable; $\phi(X_i)$ is the higher dimensional training vector resulted from X_i . After solving the problem for q and β , the test point label \hat{y}_i can be predicted as follows:

$$\hat{y}_i = \langle q, \phi(X_i) \rangle + \beta, \quad (6)$$

where $\langle ., . \rangle$ is the dot product of q and $\phi(X_i)$. Now, solving for the dual problem of Eq. (5) and the introduction of the Lagrange multipliers, the final solution will be as follows:

$$\hat{y}_j = \sum_{i=1}^n (\delta_i - \delta_i^*) K(X_i, X_j) + \beta, \quad (7)$$

where δ_i, δ_i^* are the Lagrange multipliers and $K(X_i, X_j)$ is the kernel function used to find the dot product between two ϕ without transforming them into the higher dimensional space. Thus, the computational complexity would be lowered significantly, this is commonly known as the kernel trick. SVR error performance could be improved by the use of kernels as well. There are four known kernels used in the literature, linear, Radial Basis Function (RBF), polynomial and sigmoid kernels. The RBF kernel has proved to work well on regression problems in the literature, due to its computational efficiency [52]. In this work, RBF was used as kernel, the mathematical formulation for the kernel is as follows:

$$K(X_i, X_j) = e^{-\frac{\|X_i - X_j\|^2}{2\sigma^2}}. \quad (8)$$

For SVR, similar steps were followed as the MLP. The C value that minimizes the RMSE over the training data was chosen, the optimum C value in this work was found to be 1000.

3.2.3 kNN Regression

kNN is a widely used clustering algorithm. However, it could also be implemented to solve regression problems. For each test point \hat{x} the distance to all training datapoint x_i is to be determined in the dataset as follows:

$$D_i = \sqrt{\sum_j (x_i^j - \hat{x}^j)^2}. \quad (9)$$

For each test point \hat{x} the distance to all training points x_i is computed, then the k nearest neighbors labels values y_i are averaged to predict the \hat{x} label value \hat{y} . In this work, kNN was optimized by changing the number of neighbors and tracking the RMSE values over the training data. The RMSE value was at its minimum when the number of neighbors k is five. So, for all of the kNN models, the number of neighbors was chosen to be 5.

3.2.4 Decision Tree Regression

Decision trees is a widely used machine learning algorithm, it can be used for both classification and regression. It is constructed by nodes and leafs, each node has different number of branches which would lead to another nodes or leafs. Each test point will start from the root node, then will follow the branches that are tested to be true for that test point, this procedure will be followed until a leaf is reached, then the predicted value \hat{y}_i of a test point is assigned a value as the value of the leaf that is has reached. The construction of the tree could be done using different algorithms, one of most widely used algorithm is Iterative Dichotomiser 3 (ID3), however, in this work we have implemented the classification and regression trees (CART) algorithm, since it would also solve the regression problem, and not restricted to the classification problem.

3.3 Models Input Variables

In order to see the best forecasting model for each variable (i.e. PV panel system, mosque, clinic and office building), the model has been tested under different feature selection schemes. At the beginning, the models were tested with only a single feature to see the sensitivity of the model to this feature and how important is it. After the single feature selection, different combinations of these features are fed to the forecasting models.

Table 3-1 shows all the features used to forecast the four variables, namely, the PV panel output power, the mosque demand, the clinic demand and the office building demand.

Table 3-1 Input variables to the forecasting models.

Variable name	Feature
x_i^1	Clear sky GHI
x_i^2	Clear sky DNI
x_i^3	Forecasted GHI
x_i^4	Forecasted DNI
x_i^5	Total cloud cover
x_i^6	Wind speed
x_i^7	Wind Direction
x_i^8	Temperature
x_i^9	Low cloud cover
x_i^{10}	Medium cloud cover
x_i^{11}	High cloud cover
x_i^{12}	Total Aerosol Optical Depth at 550nm
x_i^{13}	Dust Aerosol Optical Depth at 550nm
x_i^{14}	Hour
x_i^{15}	Month
x_i^{16}	Day of week
x_i^{17}	Day of year
x_i^{18}	PV generation at same hour and pervious day
x_i^{19}	mosque demand at same hour and previous week
x_i^{20}	clinic demand at same hour and previous week
x_i^{21}	office building demand at same hour and previous week

Each forecasting model (i.e. for PV panel system, mosque, clinic and office building) has been tested under four different machine learning models and each one of these machine learning models was tested under different feature selection schemes. The different combinations of these feature selection schemes are listed in **Table 3-2**. The variables x_i^{18} , x_i^{19} , x_i^{20} and x_i^{21} are defined as $x_i^{historical}$ depending on each forecasted variable. So, when we are doing forecasting for the PV panels generation $x_i^{historical}$ refers to x_i^{18} and when we are doing forecasting for the mosque the variable $x_i^{historical}$ refers to x_i^{19} . Similar thing applies also to the remaining two variables (i.e. clinic and office building). This definition is followed for simplicity. The variable x_i^{16} which refers to the day of the week is only important when doing the forecasting for the different types of buildings, as the behavior of these buildings is affected by the weekend/weekday behavior. However, this is not true for the PV panel system forecasting, as the generation of the PV panels is totally independent of the weekday/weekend schedule. Because of that, the variable x_i^{16} is not included in the PV panel forecasting model, and the variable x_i^{16} in **Table 3-1** is only applicable to the three buildings types (i.e. clinic, mosque and office building). And it is not included in all of the forecasting models for the PV generation.

Table 3-2 Feature combinations.

Feature Combination	Variables
1	x_i^1
2	x_i^2
3	x_i^3
4	x_i^4
5	x_i^5
6	x_i^6, x_i^7
7	x_i^8
8	x_i^9
9	x_i^{10}
10	x_i^{11}
11	x_i^{12}
12	x_i^{13}
13	x_i^{14}
14	x_i^{15}
15	x_i^{16}
16	x_i^{17}
17	x_i^{14}, x_i^{15}
18	$x_i^{14}, x_i^{15}, x_i^{16}$
19	$x_i^{historical}$
20	$x_i^{historical}, x_i^8$
21	$x_i^{historical}, x_i^8, x_i^{14}$
22	$x_i^{historical}, x_i^8, x_i^{14}, x_i^{15}$
23	$x_i^{historical}, x_i^8, x_i^{14}, x_i^{15}, x_i^{16}, x_i^{17}$
24	$x_i^{historical}, x_i^5, x_i^8, x_i^{14}, x_i^{15}, x_i^{16}, x_i^{17}$
25	$x_i^{historical}, x_i^8, x_i^{11}, x_i^{14}, x_i^{15}, x_i^{16}, x_i^{17}$
26	$x_i^{historical}, x_i^3, x_i^8, x_i^{11}, x_i^{14}, x_i^{15}, x_i^{16}, x_i^{17}$
27	$x_i^{historical}, x_i^3, x_i^6, x_i^7, x_i^8, x_i^{11}, x_i^{14}, x_i^{15}, x_i^{16}, x_i^{17}$
28	$x_i^{historical}, x_i^8, x_i^{11}, x_i^{12}, x_i^{14}, x_i^{15}, x_i^{16}, x_i^{17}$
29	$x_i^{historical}, x_i^8, x_i^{11}, x_i^{13}, x_i^{14}, x_i^{15}, x_i^{16}, x_i^{17}$
30	$x_i^{historical}, x_i^3, x_i^6, x_i^7, x_i^8, x_i^{11}, x_i^{13}, x_i^{14}, x_i^{15}, x_i^{16}, x_i^{17}$
31	$x_i^{historical}, x_i^3, x_i^4, x_i^6, x_i^7, x_i^8, x_i^{11}, x_i^{13}, x_i^{14}, x_i^{15}, x_i^{16}, x_i^{17}$

3.4 Model Evaluation and Error Measure

3.4.1 Error Measure

All of the forecasting models under the different feature selection schemes and under different machine learning methods were tested also under multiple error metrics, to better assess their performance. Each error metric has its own advantages and drawbacks. In this section these error metrics are defined with an explanation for each method.

Root Mean Squared Error (RMSE) is the first error metric used, it is widely used in the literature and is defined as follows:

$$RMSE = \sqrt{\frac{\sum_{i=1}^n (\hat{y}_i - y_i)^2}{n}}, \quad (10)$$

\hat{y}_i is the forecasted value at the time i ; y_i is the ground truth or actual reading at time i and n represents the total number of test points in the test dataset. The main advantage of RMSE is that the results of the error are in the same unit as the forecasted value, in this work the unit for the PV panel system and the buildings is *Watts*, which is the instantaneous power generation or consumption. RMSE is sensitive to the outliers compared to the other error metrics.

The second error metric used in this work is the normalized RMSE (nRMSE), it is basically calculated similar as the RMSE but the final result is divided by the maximum value in the test dataset, it is defined as follows:

$$nRMSE(\%) = \frac{\sqrt{\frac{\sum_{i=1}^n (\hat{y}_i - y_i)^2}{n}}}{y_{max}} \times 100, \quad (11)$$

where y_{max} is the maximum value in the test dataset. The nRMSE is a percentage error, hence, it has no unit. Normalized error such as the nRMSE are a good option when comparing the error across different datasets, as each dataset would have a different maximum value, hence, a normalization approach is required to compare the performance of these different datasets.

Third error metric used in this work is the Mean Absolute Percentage Error (MAPE), it is defined as follows:

$$MAPE(\%) = \frac{100}{n} \sum_{i=1}^n \left| \frac{\hat{y}_i - y_i}{y_i} \right|. \quad (12)$$

MAPE is also a percentage error and it is a good option when comparing the performance of different dataset. It has the issue of dividing by zero and also it could reach values more that 100% depending on the forecasting accuracy.

Fourth error metric used is the Mean Absolute Error (MAE), is can be found using the average absolute different between the predicted and the actual values across the testing dataset, is it given as follows:

$$MAE = \frac{1}{n} \sum_{i=1}^n |\hat{y}_i - y_i|, \quad (13)$$

MAE has the same units as the tested variable and is less sensitive to outliers when compared to RMSE, that's mainly because of the absence of the square term in the equation.

Last error metric used is the normalized MAE (nMAE). It is also calculated in a similar manner as the MAE, but by dividing over the maximum test value in the test dataset, the nMAE is defined as follows:

$$nMAE(\%) = \frac{1}{n} \sum_{i=1}^n \frac{|\hat{y}_i - y_i|}{y_{max}} \times 100, \quad (14)$$

The five error metrics defined earlier were all used to assess the performance of the forecasting models.

3.4.2 Smart Persistence

Smart persistence is the benchmark model implemented in this work only in the initial case study, when doing the irradiation forecasting, it is based on the deterministic irradiance variation from time t and time $t + T$, calculated from the clear sky model. The smart persistence mathematical formulation is as follows:

$$\hat{I}_{sp}(t + T) = \frac{I_{cs}(t + T)}{I_{cs}(t)} I(t), \quad (15)$$

where $\hat{I}_{sp}(t + T)$ is the smart persistence irradiance prediction at time $t + T$, $I_{cs}(t + T)$ is the clear sky model at time $t + T$, $I_{cs}(t)$ is the clear sky model at time t , $I(t)$ is the irradiance observed value at time t . The Ineichen and Perez clear sky model [53, 54] was used in this work.

3.4.3 Forecast Skill

The performance of the forecasting models need to be normalized by a benchmark. The forecast skill proposed in [55], is a way to normalize and compare the accuracy of the model against the benchmark model. The mathematical formulation of the forecast skill is as follows:

$$FS = 1 - \frac{RMSE_{model}}{RMSE_{sp}}, \quad (16)$$

where FS is the forecast skill value, $RMSE_{model}$ is the RMSE value resulted from the forecasting model, $RMSE_{sp}$ is the RMSE resulted from the smart persistence model. A forecast skill of 0 indicates that the model performance is similar to the smart persistence model. A higher positive FS value indicates that the model has a better performance compared to the smart persistence model, with a maximum FS value of 1. A negative FS value indicates that the forecasting model performs worse than the smart persistence model.

3.5 Control Strategy for the CTES

The control strategies for the CTES has been already discussed in the literature review section. Basically, there are two main types of the CTES in terms of the cooling capacity. The first one is the full storage system, where the cooling demand is met totally by the CTES during the peak hours. The second type is the partial CTES, where the cooling load is met partially by the CTES during the peak hours, while the remaining cooling demand is met by the existing chiller capacity. In this work, the partial storage system is proposed.

Chapter 4 Data

The data in this work were collected from four different resources, the following subsections discuss in detail the data resources, their resolution and cleaning methods.

4.1 PV panel data

The PV panel data were collected starting from 03-Jun-2016 until 31-08-2018. The PV panel system is placed on a rooftop of a mosque in Riyadh, Saudi Arabia. The PV site has a peak capacity of 120 kW and it has a total of 5 inverters. The inverters were installed over time, and all of them were fully operational by 15-Jul-2016. The site has a power reading every 1-minute and it is managed by King Abdulaziz City for Science and Technology (KACST) and Saudi Electricity Company (SEC) in a joint project. The data were provided as a 1-hour resolution data, using backward average. For example, the data collected from 10:01 a.m. to 11:00 a.m. are averaged across the period and then given as the value for 11:00 a.m. We then subtracted 1-hour from these readings, such that the 11:00 a.m. reading is 10:00 a.m., that's basically to make the data forward averaged as in the remaining datasets. The maximum reading in the dataset is 105,928.5 Watts on 25-Mar-2018 at 11:00 a.m. This is mainly because the sun is almost perpendicular to the solar PV panels during the month of March for the tested location. The tilt angle is kept fixed at 24° during the whole year. Any reading in the dataset with value less than 100 Watts is considered zero. The data have a few missing dates, where the readings are None, and these days were omitted from the dataset. The seasonality of the PV panel system is on a daily basis, meaning that, the pattern of the PV power curve repeats itself on a daily basis. Because of that, we have added the PV power generation for the past day as a feature to forecast the PV output for the next day.

4.2 Buildings Load Data

The building data were provided by SEC, which has three building types: mosque, health clinic and an office building. The demand reading for the buildings has a reading every 30 minutes, the reading is for the instantaneous power, given in the form HH:MM, where the HH represents the local time in hours and MM represents the local time in minutes. All the data for the three buildings have two readings each hour, one at HH:00 and the other at HH:30. In order to do the forward average reading for each hour, the data were interpolated to minutely resolution, such that the readings for each hour has 60 readings, then the average for each hour is found by averaging these 60 readings over the hour, using forward average. Performing the interpolation then taking the average again lead to a better average than just taking the two values recorded at HH:00 and HH:30, because the latter way ignores the load in the next half-hour and will not be considered in the average, while the interpolation then averaging approach takes into account the power reading in the next half-hour. Each load profile in the proposed work is different from the others in terms of the load profile characteristics. The details of each load profile are discussed in the following subsections.

4.2.1 Mosque

The daily load profile of the mosque is shown in **Figure 4.1**. The mosque load varies greatly over the day and night. The mosque load profile has multiple spikes over the day, which occur during the prayer times (5 prayers a day). Each prayer has a known time, which is correlated with solar time, hence, can be converted to local time. As seen from **Figure 4.1** the maximum load occurs during the midday, when the temperatures is at its peak causing the cooling demand to reach its peak as well. The lowest demands are during the first prayer, which is before sunrise, and at the end of the night, when the mosque is at its coolest point, causing the cooling demand to drop to its lowest. This is seen from **Figure 4.1**. The peak demand of the mosque occurs during the second and the third prayer, that is around the midday for the second prayer, hence the cooling demand is high during that time. The seasonality of the mosque load profile is weekly, that's because the Friday prayer occurs once a week during the midday, and this prayer

is crowded more than the other prayers during the other days of the week. Moreover, the mosque is more crowded during the weekends, as for the second and third prayer during the workdays, people are at their work, and they pray at their work place. Because of that, we chose the seasonality of the mosque to be weekly, and we fed the forecasting model for the mosque the demand for the previous week at the same day and hour. The maximum reading for the power meter during the whole period for the mosque is 160,80 kW. While the minimum is 700 W and the standard deviation is 29,65 kW.

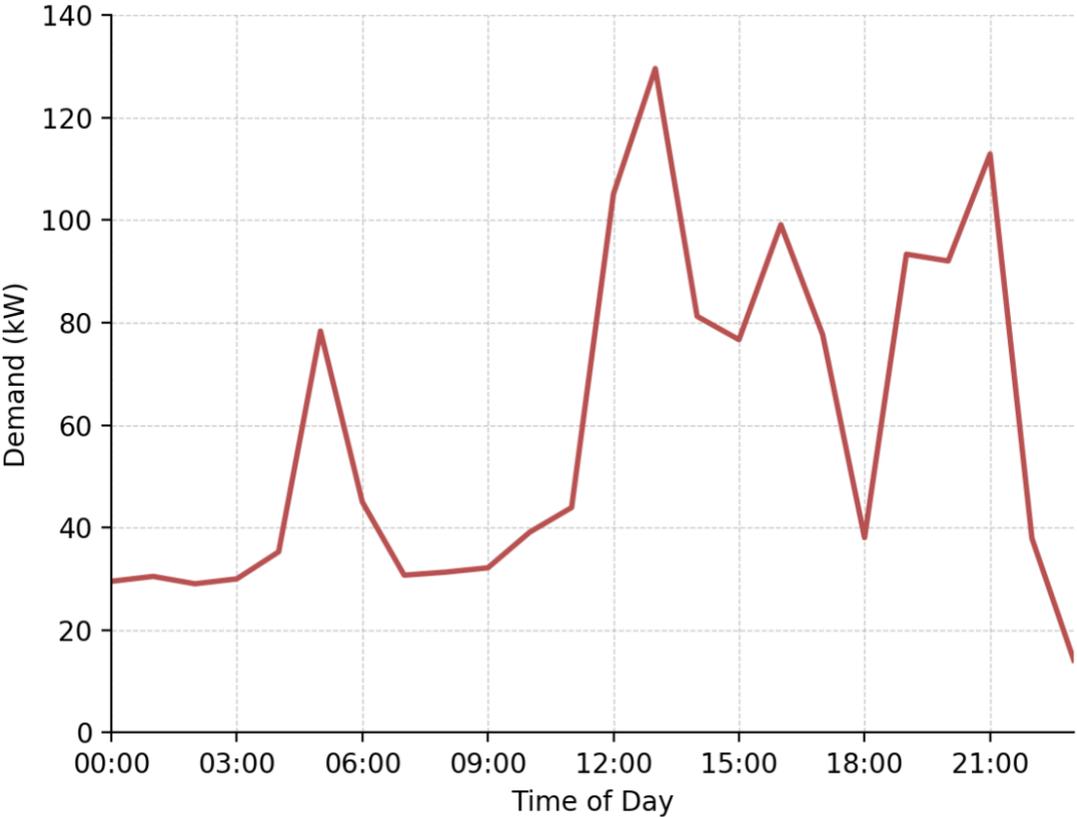


Figure 4.1 Mosque load profile for 21-Jul-2017.

4.2.2 Clinic

The clinic load profile is shown in Figure 4.2, the load has much less variability when compared with the mosque. The load is smooth and peaks around 4:00 p.m. (local time). The minimum load is around 40 kW, while the maximum is around 50 kW, that’s 25%

above the minimum. The maximum reading for the power meter during the whole period for the clinic is 102,45 kW. While the minimum is 9,45 kW and the standard deviation is 16 kW. The load behavior of the clinic has weekly seasonality, meaning that the load shape repeats itself every week with small variations depending on the weather conditions and the vacations. Because of this weekly seasonality we choose the load feature to be the previous week load at same day of the week and same hour. The clinic load is the smoothest among all the studied loads. Meaning that, the deviation between the maximum and the minimum is the lowest when compared with the other loads in this work.

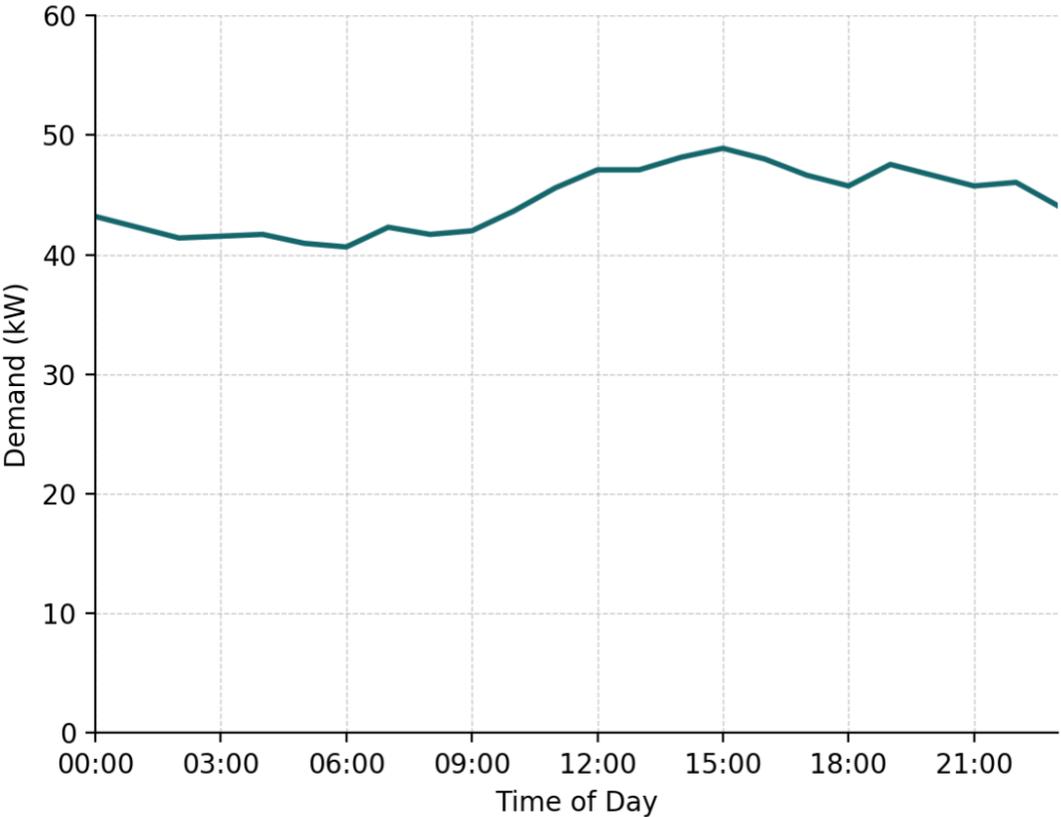


Figure 4.2 Clinic load profile for 21-Jul-2017.

4.2.3 Office building

The office building load profile is shown in **Figure 4.3**, the peak demand occurs around 1 p.m. (local time). While the minimum occurs at around 7-8 a.m., that's just before the employees come to work. The maximum demand is around 100 kW, while the minimum is around 75 kW. The maximum reading for the power meter during the whole period for the office building is 147,68 kW. While the minimum is 30,4 kW and the standard deviation is 18,8 kW. As the previous two loads, the load behavior of the office building has weekly seasonality. Because of this weekly seasonality we choose the load feature to be the previous week load at same day of the week and same hour. The office building load is in the middle when it comes to the variations in the load when compared with the other two loads, the mosque and the clinic.

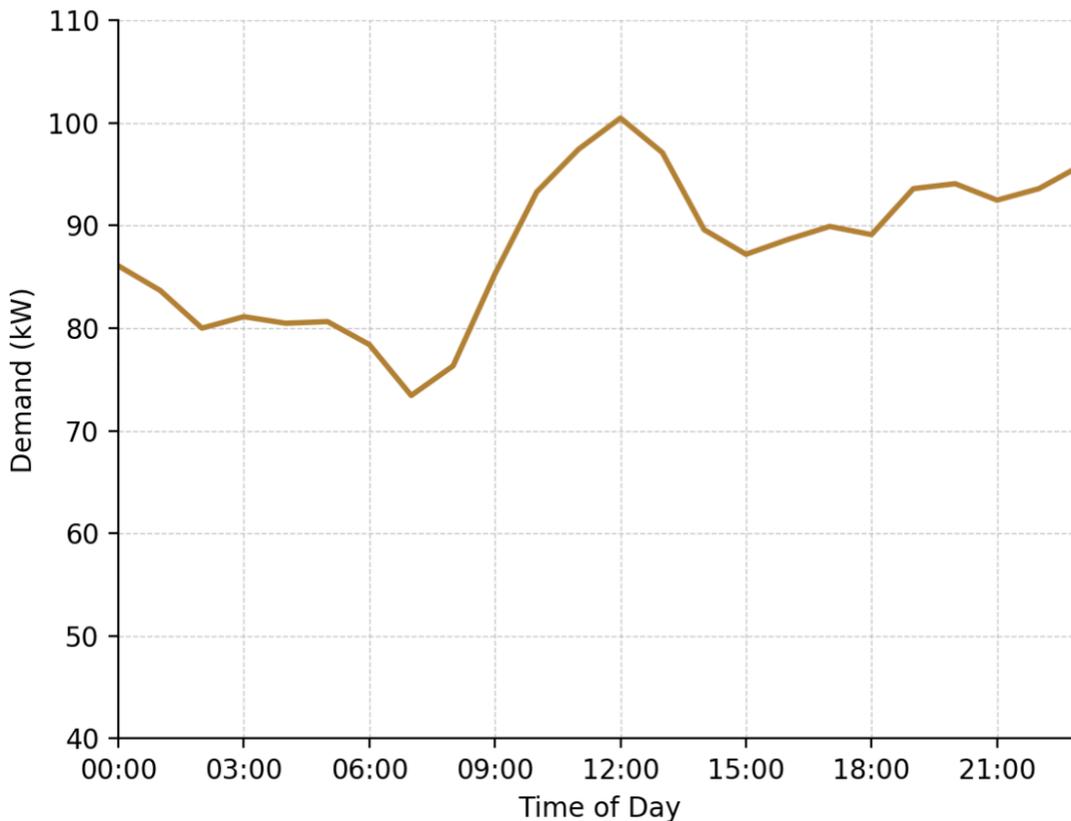


Figure 4.3 Office building load profile for 21-Jul-2017.

4.3 CAMS near-real time global atmospheric composition service data

The CAMS near-real time global atmospheric composition service data is a satellite dataset that has been processed to estimate the atmospheric composition at a global scale. The CAMS data is available every 3-hours and it is averaged forward. In order to have a 1-hour resolution data, we performed a linear interpolation for the hours in between, such that we have an atmospheric reading every hour. The CAMS data have lots of features to choose from, the list of available features can be found here¹. The data have AOD readings at multiple wavelengths (i.e., 469, 550, 670, 865 and 1240 nm). The data have also the estimates for the particulate matter pm at different scales from 1 to 10 μm , temperature estimated at two meters above the ground and wind direction at 2 meters above the ground. Multiple grid sizes are available through CAMS, in this work we have used the smallest available grid size, which is $0.125^\circ \times 0.125^\circ$ that contains the site under test. The service is implemented by European Center for Medium-Range Weather Forecasts (ECMWF).

4.4 CAMS radiation service

The CAMS radiation service is a service that provides the radiation forecasts for the GHI, DNI and DHI on horizontal surface. The forecasts are estimated for both the clear sky conditions and for the actual weather conditions taken from the CAMS near-real-time. The provided forecasts are available on a monthly, daily, hourly and up-to 1-minute resolution. The hourly data is used in this work. The data can be downloaded from here². The data from this dataset is forward averaged as the remaining datasets in this work.

4.5 Data Splitting

¹ <https://apps.ecmwf.int/datasets/data/cams-nrealtime/>

² <http://www.soda-pro.com/web-services/radiation/cams-radiation-service>

After all the data has been cleaned and as described in earlier sections, all the data from the four different resources has been integrated together using the timestamp information. The total number of features of this integrated dataset is shown in **Table 3-1**, which includes all the tested features. Now, after integrating the datasets and before training the forecasting models, the data has been split into training and testing. The training dataset is used to train the forecasting models (i.e. Decision Trees, kNN, etc.). While the testing data is used to test the model performance after the model has been trained. We split the data into 80% as training data and the rest 20% is used as testing data. The data splitting is random across the dataset, this way we can insure that the test data has contains different days, hours and weather conditions. The training data and test data are the same across all the models. Meaning that, the training data used to train the kNN and the remaining forecasting methods are the same. Similar this also applies to the testing data.

4.6 Data Normalization

Each of the features shown in **Table 3-1** in the dataset has different maximum and minimum values. So, features with higher values would impact the model more when performing the forecasting. In order to make all the features have the similar impact initially on the forecasting model, a data normalization technique has been used before training the data. The data normalization used in the work is shown in Eq. (17):

$$x_{norm} = \frac{x_i - \bar{x}_i}{\sigma}, \quad (17)$$

where x_{norm} is the normalized feature, x_i is the original feature value, \bar{x}_i is the mean value across that feature and σ is the standard deviation for that specific feature.

Chapter 5 Dust Analysis

In this chapter only the preliminary results on the forecasting models discussed earlier are shown, to investigate the effectiveness of adding the dust as feature to the forecasting model. The preliminary results were tested on an hour-ahead time horizon, with dust included as an input parameter. Dust information was fed to the forecasting model, including both the ground measured dust at the last hour and the forecasted dust based on the satellite data for the next hour. The forecasting is for three solar irradiance components, namely the Global Horizontal Irradiance (GHI), Direct Normal Irradiance (DNI) and the Diffuse Horizontal Irradiance (DHI). The overall forecasting model is shown in **Figure 5.1**.

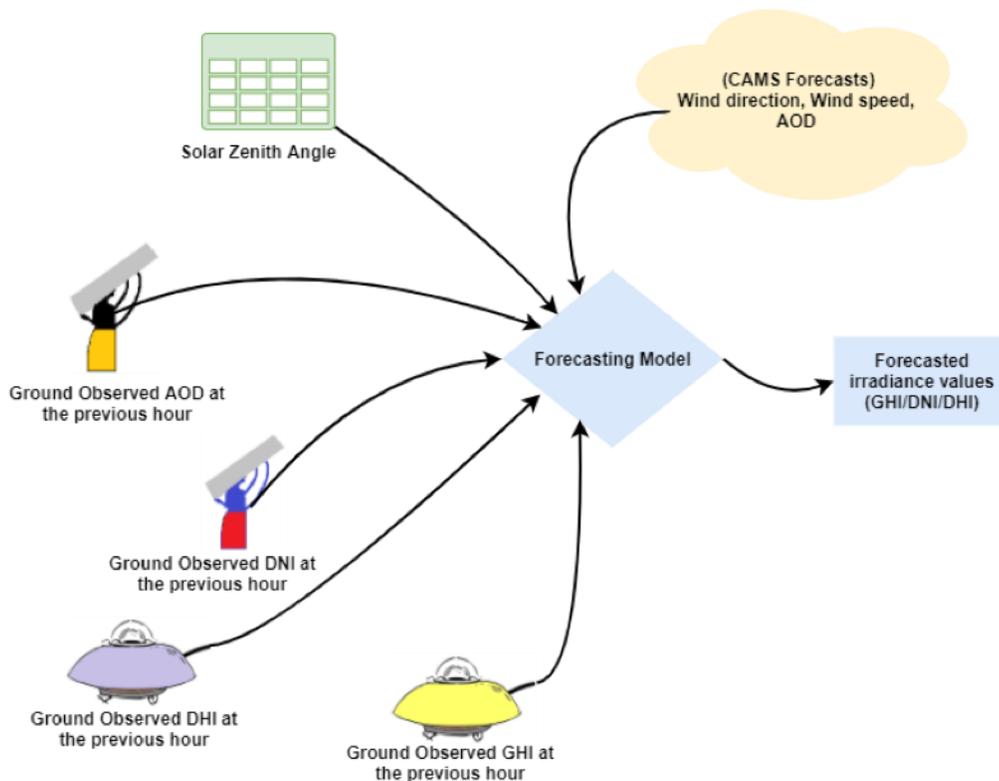


Figure 5.1 Basic structure of the forecasting model.

Annual average AOD at 550 nm over the world for the year 2015 is shown in **Figure 5.2**, as can be seen from **Figure 5.2** the test location reside in area where the average AOD is high. In **Figure 5.3** the annual average GHI over Saudi Arabia is shown.

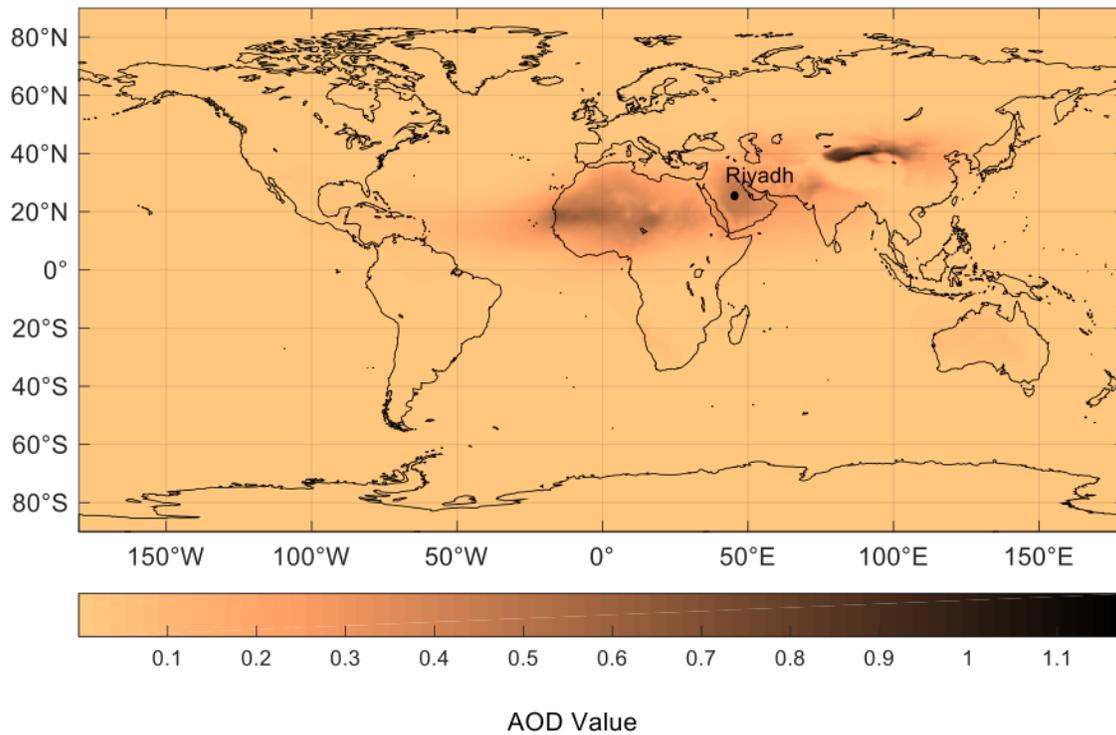


Figure 5.2 Annual average AOD at 550 nm over the world for the year 2015 using CAMS dataset [56].

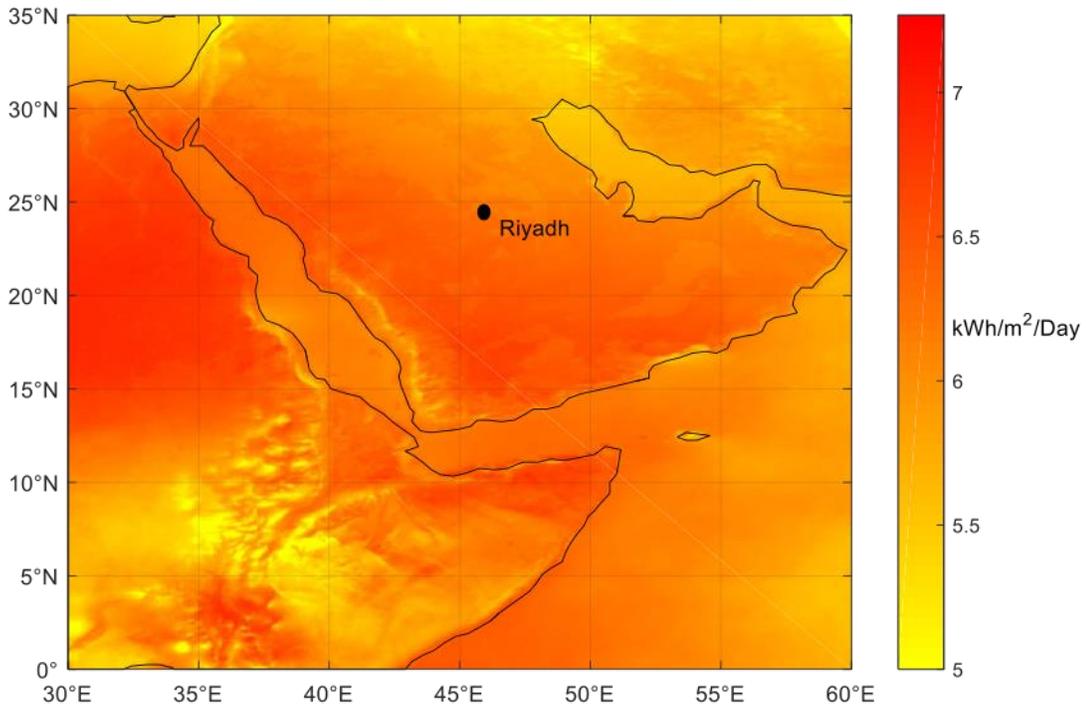


Figure 5.3 Annual GHI over Saudi Arabia for the year 2013 based on Meteosat data.

In order to design the proposed solar forecasting system, machine learning/data driven approaches were used as discussed earlier in Methodology section. Different machine learning methods, namely Multilayer Perceptron (MLP), SVR, kNN and decision tree were implemented. The inputs for these models are listed in **Table 5-1****Error! Reference source not found..** For each solar irradiance variable (i.e., GHI, DNI and DHI), a forecasting model was generated using these four methods. Each forecasting method was tested under different feature selection schemes as shown in **Table 5-2**.

Table 5-1 Input variables to the forecasting models.

Input Variable	Input Variable Explanation
x_i^1	Ground measured GHI at last hour
x_i^2	Ground measured DNI at last hour
x_i^3	Ground measured DHI at last hour
x_i^4	Hour of the Day
x_i^5	Month of the Year

x_i^6	Solar Zenith Angle
x_i^7	Wind Speed
x_i^8	Wind Direction
x_i^9	CAMS AOD at 550 nm
x_i^{10}	AERONET AOD at 550 nm observed at last hour
x_i^{11}	Angstrom Exponent α

Table 5-2 GHI/DNI/DHI forecasting model feature selection schemes.

Variable	Feature Selection Scheme	Input Variables
GHI	1	$x_i^1, x_i^4, \dots, x_i^7$
	2	$x_i^1, x_i^4, \dots, x_i^9$
	3	$x_i^1, x_i^4, \dots, x_i^8, x_i^{10}, x_i^{11}$
DNI	1	$x_i^2, x_i^4, \dots, x_i^7$
	2	$x_i^2, x_i^4, \dots, x_i^9$
	3	$x_i^2, x_i^4, \dots, x_i^8, x_i^{10}, x_i^{11}$
DHI	1	$x_i^3, x_i^4, \dots, x_i^7$
	2	$x_i^3, x_i^4, \dots, x_i^9$
	3	$x_i^3, x_i^4, \dots, x_i^8, x_i^{10}, x_i^{11}$

In the next sections the datasets are discussed and analyzed, the final section shows the results for this preliminary case study.

5.1 Datasets

The datasets used in this preliminary case study were collected from KACARE, AERONET, and CAMS, covering the period of three years from January 14th, 2013 to December 31st, 2015 with a temporal resolution of one-hour. The data collection, cleaning and quality assurance techniques for each dataset are discussed below.

5.1.1 KACARE dataset

KACARE is a government agency responsible for the renewable energy legislation, analysis, measurements and research in Saudi Arabia. In 2013, KACARE started Renewable Recourse Monitoring and Mapping (RRMM) Solar Measurement Network.

The goal of this RRMM Solar Measurement Network is to provide accurate ground-based measurements of solar radiation alongside the relevant weather parameters across the country. The total number of stations in the network is 53 [57].

The KACARE dataset used in this work was collected in Riyadh, Saudi Arabia, with exact site information as shown in the **Table 5-3**.

Table 5-3 KACARE site information.

Latitude	24.90693° North
Longitude	46.39729° East
Elevation	764.0 Meters

The used measurement instruments are shown in **Table 5-4**.

Table 5-4 List of measurement Instruments.

Parameter	Equipment	Units	Uncertainty	Details
Relative Humidity	Relative Humidity Probe	% RH	+/- 3% to +/- 7%	Primary
GHI	Pyranometer	W/m ²	+/- 2.0%	Primary
GHI	Rotating Shadowband Radiometer	W/m ²	+/- 5.0%	Secondary
DNI	Pyrheliometer	W/m ²	+/- 2.0%	Primary
DNI	Rotating Shadowband Radiometer	W/m ²	+/- 5.0%	Secondary
DHI	Pyranometer	W/m ²	+/- 2.0%	Primary
DHI	Rotating Shadowband Radiometer	W/m ²	+/- 5.0%	Secondary
AOD	CIMEL C-318 Sunphotometer	No unit	+/- 0.01 OD	Primary

KACARE data are collected every minute during daytime, containing GHI, DNI, DHI and relative humidity readings. In this work, we have computed the one-hour average of these 1-min readings. So, for each hour HH:MM, we average all the minutes MM in

that hour from MM=00 to MM=59, then use this averaged (GHI/DNI/DHI) value in the tested models as x_i^1 , x_i^2 and x_i^3 . In order to have more robust measurements, a secondary Pyranometer similar in make and model was installed at the same site to measure GHI, plus the rotating shadowband radiometer listed in **Table 5-4**. Data is collected from the secondary equipment in case of the failure of the primary equipment. The last column in the **Table 5-4** shows whether the equipment was used as a primary or a secondary for the measurements. For post processing data quality assurance NREL's Solar Energy Research Institute Quality Control (SERI-QC) procedures were followed [58]. Data can be requested through KACARE Atlas website (KACARE; <https://rratlas.kacare.gov.sa/>)

5.1.2 AERONET dataset (AERONET; <https://aeronet.gsfc.nasa.gov/>)

The AERONET program is a remote sensing ground-based measurement network supported by NASA and many international institutions around the world. Their goal is to measure the AOD across different locations in the world and provide these measurements, alongside with microphysical properties, as an open access data.

AOD is a measure of the attenuation of radiation due to aerosols. AOD has no unit of measurements, i.e., unitless. The minimum AOD value is zero, which indicates that the atmosphere is clear. AOD value of 1 or more indicates a severe dust storm present in the scene. Depending on the type of aerosols to be estimated, AOD is measured at multiple wavelengths. In this work, the focus is to investigate the effect of dust, which is measured at 550 nm, using both ground-based and satellite-based measurements.

AOD equipment for the tested site is located at the same coordinates shown in **Table 5-3**. This site has AOD readings at seven different wavelengths (i.e., 340, 380, 440, 500, 670, 870 and 1020 nm), as well as water vapor, solar zenith angle and the angstrom values. This study focuses on the wavelengths at 440 and 670, since they are used to extrapolate the AOD value at 550 nm, at which the dust concentration in the air is being measured. The extrapolation of AOD at 550 nm can be calculated as follows:

$$\tau_2 = \exp(\ln(\tau_1) - \alpha \ln(\frac{\lambda_2}{\lambda_1})), \quad (18)$$

where τ_1 is the AOD at 440 nm; α is the Angstrom Exponent and it is a good indicator for the aerosol particle size in the air, $\alpha \leq 1$ indicates that the AOD particle distribution is mainly dominated by coarse mode particles, while $\alpha \geq 2$ represents an AOD distribution that is mainly dominated by a fine mode particles [59], τ_2 is the desired AOD at 550 nm, at which the dust accumulation in the air is being measured. λ_1 and λ_2 are the wavelengths at 550 nm and 440 nm. Angstrom Exponent α can be found using the AOD readings at 440 nm and 670 as follows:

$$\alpha = \frac{\ln(\tau_3) - \ln(\tau_1)}{\ln(\lambda_3) - \ln(\lambda_1)}, \quad (19)$$

where τ_3 is the AOD value at 670 nm and λ_3 is the wavelength at 670 nm.

The dataset has multiple readings every hour without consistency in data reading intervals. However, in most of the days there is at least one reading every hour. If multiple readings are recorded for an hour HH:MM, all the readings through that hour (MM=00 to MM=59) are averaged, hence, we have one value per hour, this value is denoted as x_i^{10} as shown in **Table 5-1**. If one hour has a no readings, then the missing reading at this hour is substituted by implementing a linear interpolation. **Figure 5.4** shows histogram of how many distinct hours the AERONET AOD readings are measured each day for the tested site.

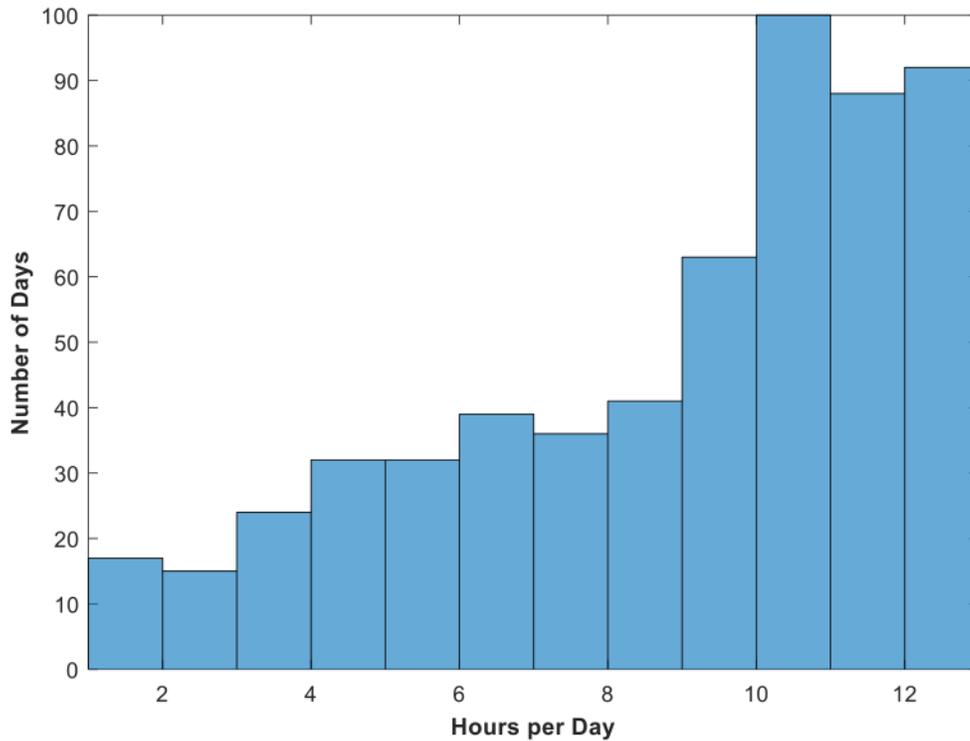


Figure 5.4 Histogram of the number of hours the AOD was measured each day, based on the data provided by AERONET for KACARE sites.

It can be seen that 92 days that have readings at 12 distinct hours. Clearly from the plot, some days have measurements only 1 hour or 2 hours. In this case linear interpolation will not provide realistic AOD values. Thus, in order to ensure the quality of input data, the dataset was selectively chosen to include only the days that have readings recorded for at least 6 distinct hours during that day. Data from AERONET are available at three quality levels: Level 1.0 is raw data collected from the measurement devices directly; Level 1.5 data are cloud screened; and Level 2.0 data are cloud screened and manually inspected [60]. Level 1.5 data were used in this work due to the unavailability of Level 2.0 for the requested period of time. AOD data are measured using CIMEL C-318 sunphotometer [61].

5.1.3 CAMS dataset

CAMS is one of the Copernicus programs aimed to provide data on atmospheric composition at regional and global scale. It is managed by the European Commission (EU), in partnership with European Space Agency (ESA), the European Organization for the Exploitation of Meteorological Satellites (EUMETSAT) and the ECMWF.

The data contains many air quality parameters. It has AOD readings at five different wavelengths (i.e., 469, 550, 670, 865 and 1240 nm), Particulate Matter at different diameters (i.e., 10, 2.5, 1 μm), plus other weather parameters, such as temperature, wind speed, dew point temperature, cloud cover and albedo.

The CAMS system utilizes AOD data retrieved from both Polar Multi-Sensor Aerosol Product (PMA_p) provided by EUMETSAT, alongside with the AOD data retrieved from Moderate Resolution Imaging Spectroradiometer (MODIS) provided by NASA.

A grid size of $0.5^\circ \times 0.5^\circ$ that contains the site indicated in **Table 5-3** was used in this work. The temporal resolution of the CAMS data is based on 3 hours forecasting step, starting from 00:00 UTC to 21:00 UTC for each day, so, for each day the available forecasts are for the hours 00:00, 03:00, 06:00, 09:00, 12:00, 15:00, 18:00 and 21:00, a total of 8 readings. In order to match the temporal resolution of the CAMS readings with other KACARE and AERONET datasets readings, a linear interpolation was performed on CAMS dataset, such that, a one reading was made available at each hour of the day. In this work, we implemented an hour-ahead forecasting model, hence, we used the forecasted CAMS AOD value for the next hour, which was already interpolated as discussed above. This CAMS AOD value is fed into the model as x_i^9 , as shown in **Table 5-1**. **Error! Reference source not found.** All of CAMS data used in this work are available through ECMWF website (ECMWF; <https://www.ecmwf.int/>).

5.2 Data analysis

This section provides some insights and analysis about the dataset implemented in this work. **Figure 5.5** shows a windrose plot alongside with dust AOD values for the site

under study in Riyadh, Saudi Arabia. The location is surrounded by two deserts, the Rub' Al-khali desert from the South and South East and Addahna desert from the North East. This makes the selected site a perfect choice for this work.

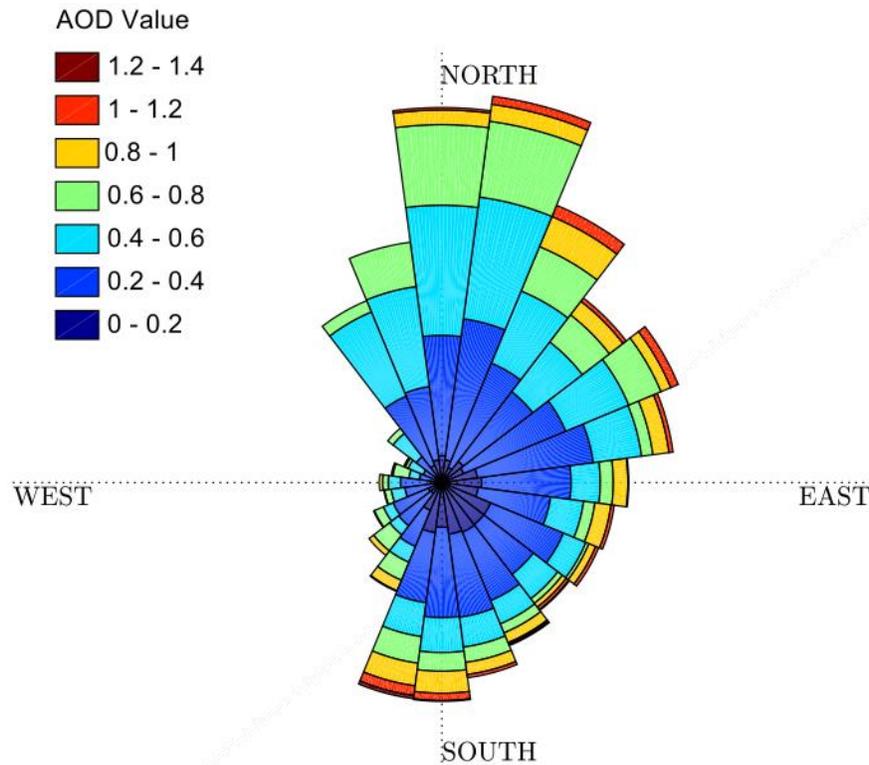


Figure 5.5 Windrose plot versus AOD values.

As can be clearly seen from the plot, the AOD values are highly dependent on the wind direction. The southern winds would have a higher chance of carrying dust particles, and in the second place the northern winds with a lower chance. This could be understood, knowing the fact that there is a large sand dessert laying at the southern side of the site, and another large desert laying at the northeastern side. Thus, any wind originating from these directions would have a higher probability of carrying sand particles, hence increasing the AOD value. Conversely, winds coming from the western side would have a lower probability of carrying dust particles. Therefore, dust intensity in the air is highly dependent on the wind direction. Accordingly, the solar irradiance is dependent on wind direction as well.

A scatter density plot to compare AERONET AOD at 550 nm (AOD_{550}) and CAMS AOD_{550} values is shown in **Figure 5.6**. As can be clearly seen, CAMS AOD_{550} seems to

overestimate the actual AERONET AOD_{550} readings. The correlation between the two datasets found to be 0.634. This moderate correlation coefficient means that CAMS AOD_{550} forecasts are uncertain. Accordingly, this would lead to a lower solar irradiance forecasts accuracy. Thus, a ground-based measurement for AOD_{550} would provide a correction factor for CAMS AOD_{550} forecasts for the next hour, hence, a more accurate solar irradiance forecasts.

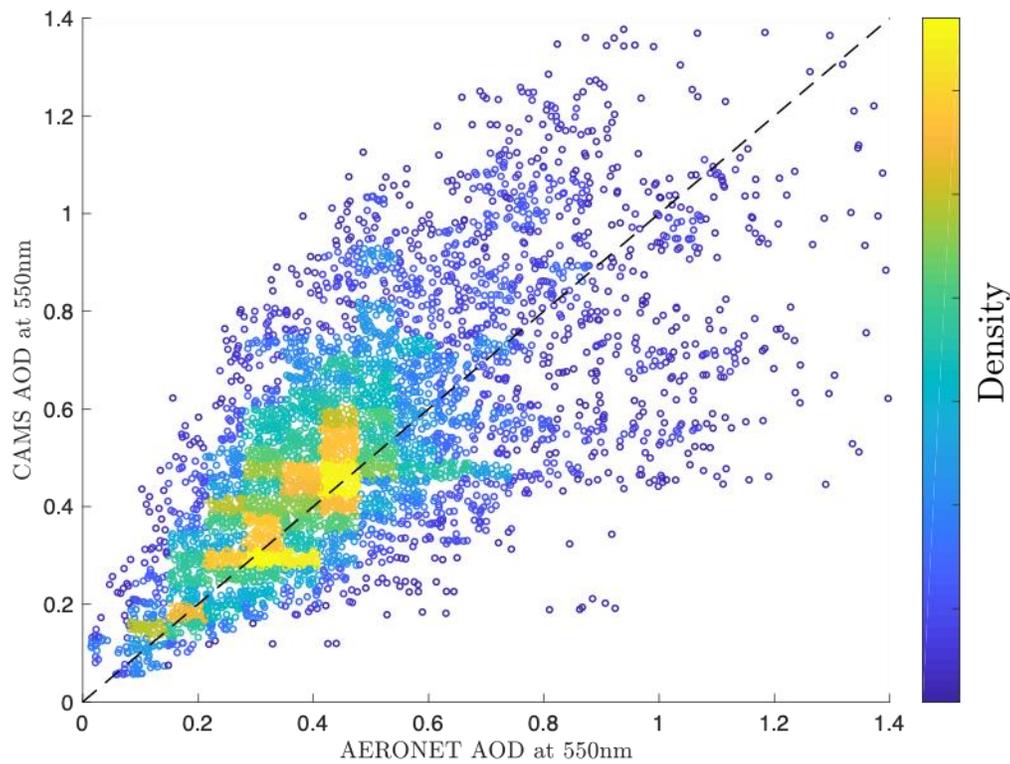


Figure 5.6 AERONET AOD values at 550 nm vs. CAMS AOD values at 550 nm. The dashed line represents the ideal estimation case.

Figure 5.7 shows the AERONET AOD_{550} hourly readings histogram. The standard deviation is 0.3070 with the mean of 0.4413. Statistics of the remaining variables are shown in **Table 5-5**. The AOD_{550} covers the spectrum of clear sky to heavily dusty weather.

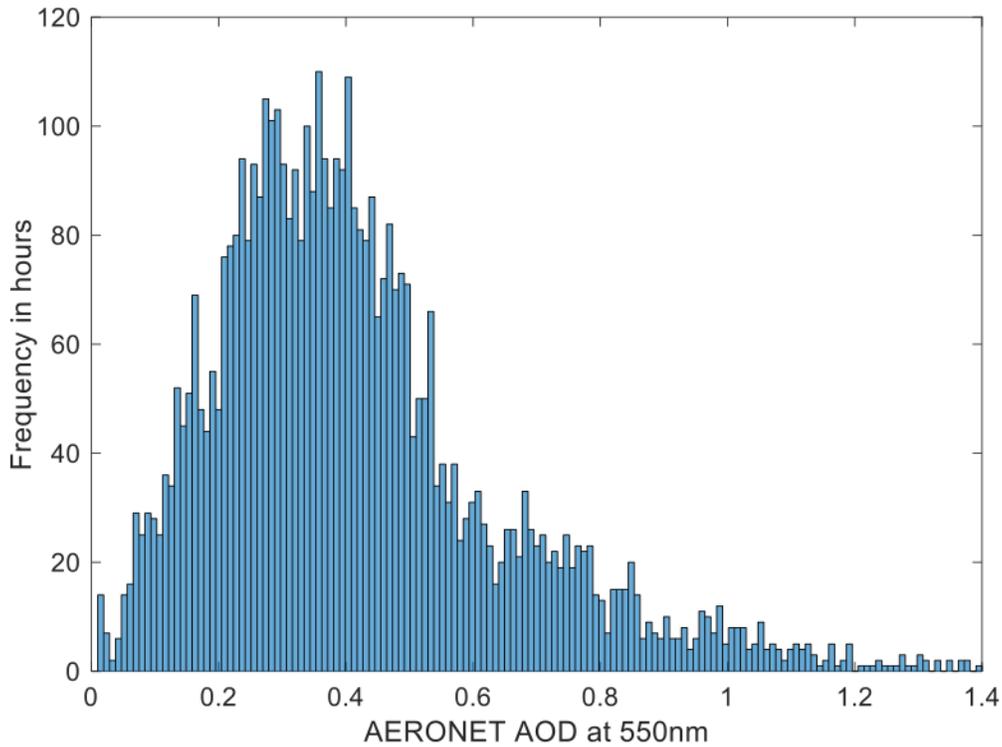


Figure 5.7 AERONET AOD at 550 nm histogram.

Table 5-5 Variables mean and standard deviation.

	Mean	Standard Deviation	Unit
GHI	620.34	272.96	W/m ²
DNI	567.11	242.26	W/m ²
DHI	221.63	112.82	W/m ²
Wind Speed	4.212	1.75	m/s
AERONET AOD_{550}	0.4413	0.3070	--
CAMS AOD_{550}	0.5375	0.2569	--

Figure 5.8 shows the average monthly AOD_{550} for the test site, starting from 2013 to 2015, for both the AERONET and CAMS datasets. April then May have the highest AOD_{550} among all the other months in both datasets. Moreover, CAMS dataset appears to overestimate the AOD_{550} values most of the year except for the months starting from

August to December. This over estimation in the AOD_{550} values obtained from CAMS dataset is expected as can be seen in **Figure 5.6**.

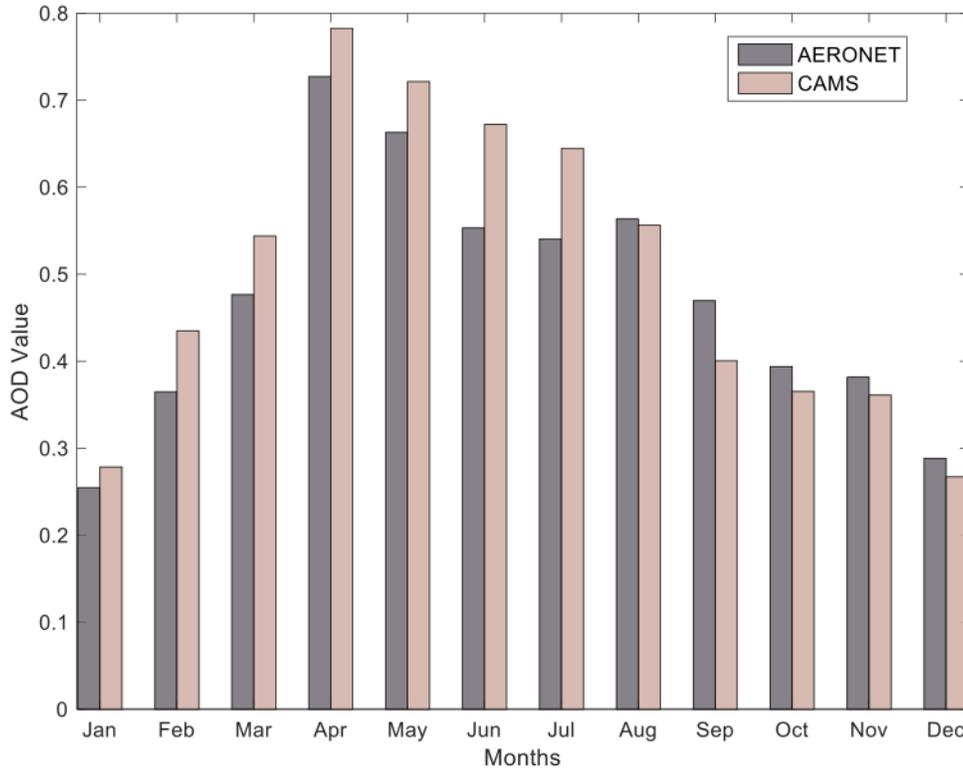


Figure 5.8 AERONET and CAMS average AOD at 550 nm for each month of the year, using data from 2013 to 2015.

In **Figure 5.9** the average behavior of (GHI/DNI/DHI) over the whole dataset is shown under different AOD values. As can be seen from the figure, DNI is the most sensitive radiation variable to AOD. DNI drops by roughly 60% when moving from clear atmosphere periods ($AOD=0$) to periods with large aerosol presence ($AOD=1$) caused by extreme dust events. On the other hand, DHI increases as AOD value increases. DHI increases by roughly 130% when moving from a clear sky condition to an extreme dust condition. Lastly, GHI is the least sensitive variable to AOD. That is mainly because GHI is composed of both DNI and DHI. Hence, any loss in the DNI component is partially compensated by the increase in DHI component. As a result, the effect of AOD on GHI is limited.

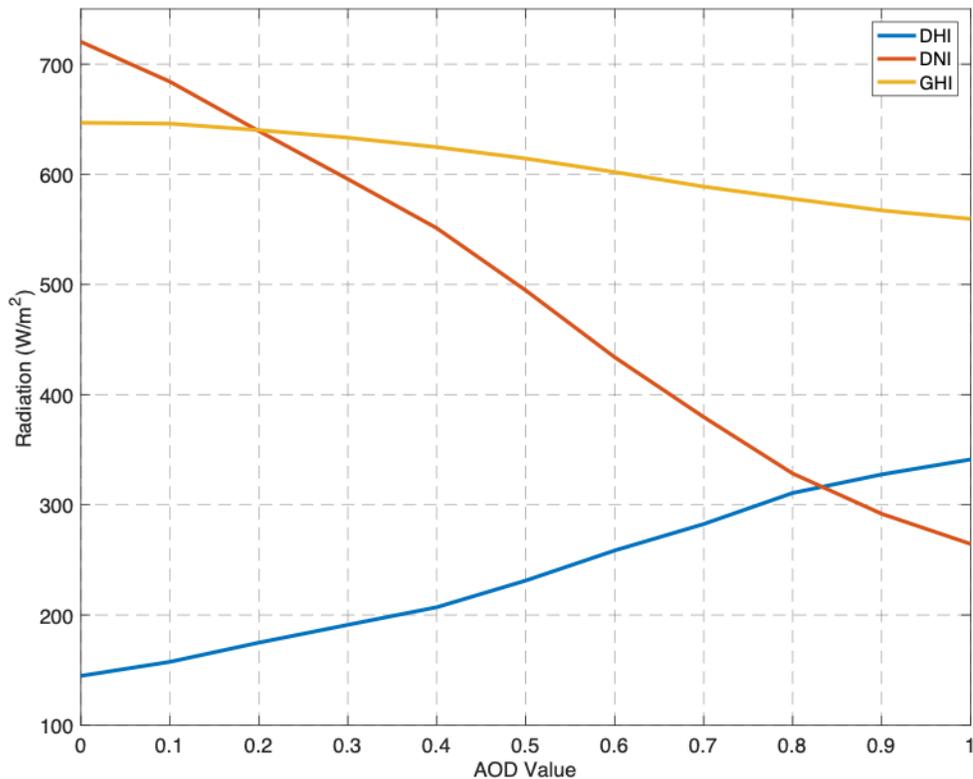


Figure 5.9 (GHI/DNI/DHI) biases under different AOD values.

5.3 Results and discussion

The forecasting model basic structure is shown in **Figure 5.1**. The input variables for GHI/DNI/DHI forecasting models are listed in **Table 5-1** **Error! Reference source not found.** & **Table 5-2**. The construction of each forecasting method and the different subsets of the selected parameters are discussed earlier.

Table 5-6 shows the GHI results using the testing data under these different methods and feature selection schemes. Each row in **Table 5-6** represents a set of selected features and each column represents the forecasting method used. For the first row in **Table 5-6**, features $x_i^1, x_i^4, \dots, x_i^8$ are considered, they represent a set of features as described in Table 1, these features are considered the basic feature selection scheme in this work. As we move to the next row, when the CAMS AOD_{550} x_i^9 is added to the model, an improvement can be seen in all the models except for the kNN. Now, as we

move to the last row, when we remove the CAMS $AOD_{550} x_i^9$ and add both the AERONET $AOD_{550} x_i^{10}$ and the angstrom exponent x_i^{11} , improvement was observed in all tested models. When comparing the FSs for the MLP, kNN and SVR in the last row with the CAMS AOD_{550} model, an improvement of around 9%, 2% and 0.45% was observed, respectively. As can be seen from Table 6, when the new features are added, the RMSE and FS results for the MLP model kept on improving, while those for the SVR and kNN have no noticeable improvement. The smart persistence model for the GHI achieved an RMSE of 56.54 (W/m^2), the values for this smart persistence model were computed as described in Eq. (12), and then the RMSE for this model was obtained as shown in Eq. (10). The GHI forecasting model implemented using the MLP has the best RMSE results on average, also it achieved the best RMSE result when the proposed features (i.e., x_i^{10} and x_i^{11}) were added. Moreover, MLP model has a FS improvement of around 16.6% when compared to the best performing model in the remaining models (i.e. kNN, SVR, decision tree).

On average the AOD_{550} effect on the GHI results across all tested methods is limited. To further analyze this effect, the MAPE for GHI forecasts was computed versus the AOD_{550} values under two solar zenith angles $\theta = 40^\circ$ and 60° . **Figure 5.10** shows the MAPE for the GHI model when tested under these two solar zenith angles, the MAPE for GHI has a slight increase as the AOD_{550} value increases, this is shown in **Figure 5.10** as the red and blue lines. Hence, the errors in the GHI forecasts increase as the AOD_{550} value increases. Moreover, the MAPE for GHI also increases as the solar zenith angle increases (i.e. the beginning and the end of the day). However, the MAPE tend to stay below 10% and around 5% on average. As can be seen from **Figure 5.10**, the maximum MAPE for the GHI occurs at high AOD_{550} values. When $\theta = 60^\circ$ the MAPE is around 10%, while for $\theta = 40^\circ$ it's around 4%. Hence, AOD_{550} has some effect on GHI, however, this effect is limited, this can be clearly seen in **Figure 5.6**, as the AOD_{550} values were added to the models, only a limited improvement was observed in the RMSE values on average. The yellow lines and the right y-axis in the **Figure 5.10** show the GHI values under different AOD_{550} values, as for the MAPE, the GHI readings were also analyzed under two solar zenith angles $\theta = 40^\circ$ and 60° . As can be seen from the yellow lines, the GHI values decrease as the AOD_{550} value increases. However, this decrease in the GHI

value is smooth and not steep as to be compared with DNI values later. The analysis using remaining solar zenith angles would lead to similar results. However, the results for $\theta = 40^\circ$ and 60° are shown since the remaining zenith angles have some missing readings in the test data set under specific AOD values.

Overall, GHI results indicate that the MLP model outperformed all other methods as the new features were added. Hence, the MLP model is able to understand the complexity and diversity of these features and keep minimizing the RMSE. On the other side, the kNN, SVR and decision tree methods seem to saturate around the same RMSE value as these new features were added. The RMSEs for training and testing datasets are shown in **Figure 5.11**, for both kNN and SVR when they are tested under different feature selection schemes. It is apparent that these two models were overfitted when some features were added as can be seen in **Figure 5.12**. The model parameters for kNN and SVR were optimally chosen based on the training set, the kNN model was tested under different number of neighbors k , the model's RMSE saturates around $k = 5$. Similarly, for the SVR, the model was tested under different C values, the optimum C value is found to be 1000. In [62], they were able to achieve a FS of 22% using their best subset of features including the GHI observed only at the last hour, in [63] they achieved 30.5% FS over the one-hour forecast horizon.

Table 5-6 RMSE results (W/m²) for GHI model and the forecast skill (FS).

Input Variables	MLP		kNN		SVR		Decision tree	
	RMSE	FS %	RMSE	FS %	RMSE	FS %	RMSE	FS %
$x_i^1, x_i^4, \dots, x_i^8$	38.24	32.35	38.15	32.52	57.97	-2.53	48.51	14.20
$x_i^1, x_i^4, \dots, x_i^9$	37.78	33.16	43.23	23.52	56.37	0.28	45.78	19.08
$x_i^1, x_i^4, \dots, x_i^8, x_i^{10}, x_i^{11}$	32.75	42.10	42.11	25.51	56.11	0.75	45.88	18.85

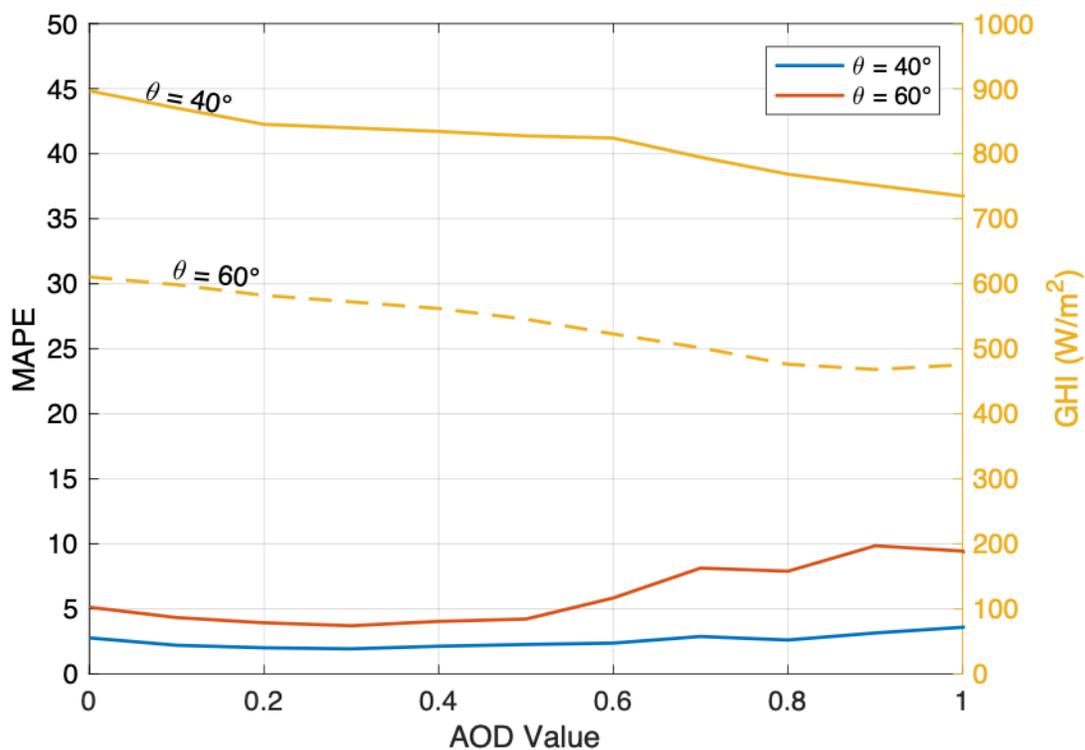


Figure 5.10 Left y-axis shows MAPE for GHI vs AOD, right y-axis shows GHI value vs. AOD. The results were computed for different solar zenith angles $\theta = 40^\circ$ and 60° .

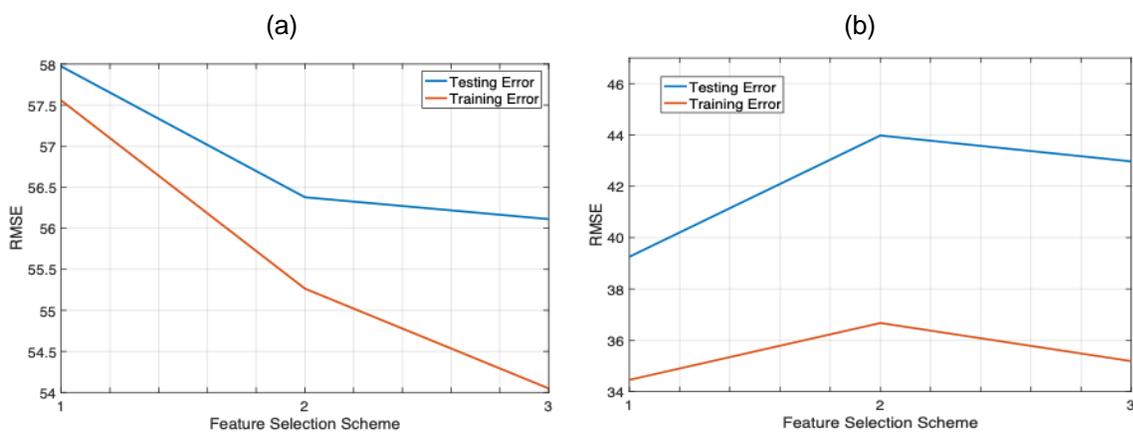


Figure 5.11 The training and testing error for tested under two methods. (a) shows the RMSE values for the SVR model. (b) shows the RMSE for the kNN model.

Table 5-7 shows DNI results under the same discussed models and feature selection schemes, the results presented were computed using the testing data discussed earlier.

The parameters of the kNN and SVR models were optimized again for the DNI model following similar steps discussed earlier for the GHI model. The smart persistence model for the DNI achieved an RMSE of 102.40 (W/m^2). As can be seen from **Table 5-7**, the accuracy of all the models kept on improving as more features were added.

In order to analyze this more, the MAPE for DNI is calculated under different AOD_{550} values. **Figure 5.12** shows the MAPE for DNI versus the AOD_{550} value for the model $x_i^2, x_i^4, \dots, x_i^9$, where the ground observed AOD_{550} and angstrom exponent (i.e., x_i^{10} and x_i^{11}) were not added to the model yet. As before, MAPE for the DNI was measured at two solar zenith angles $\theta = 40^\circ$ and 60° shown in red and blue in **Figure 5.12**. As can be seen from the plots, MAPE for the DNI increases noticeably as the AOD_{550} value increases. Hence, DNI value is very sensitive to AOD_{550} value under the clear sky conditions. The effect of AOD_{550} on DNI value is 3 to 4 times larger when compared to the GHI [64], this can be clearly seen when comparing the GHI and DNI errors in both Fig. 12 and **Figure 5.12** under the same θ . The maximum MAPE for the GHI when $\theta = 60^\circ$ is about 10% while that for the DNI is around 45%. Moreover, the MAPE for DNI also increases as the solar zenith angle increases (i.e. the beginning and the end of the day). In [42] they studied multiple AERONET locations around the world and classified the tested site (i.e. Riyadh, Saudi Arabia) as high turbidity site, moreover, they show that the AOD versus DNI relationship can be characterized by a linear estimation in low turbidity sites, however, for high turbidity sites the linear relationship is no longer applicable, hence, constructing a DNI forecasting model will be a harder problem in these sites. The yellow lines and the right y-axis in **Figure 5.12** show the DNI value under different AOD_{550} values, DNI values were computed under two solar zenith angles $\theta = 40^\circ$ and 60° . When the AOD_{550} value increases, a high drop in the DNI values is noticed for the same solar zenith angle θ .

Now, as the ground measured AERONET AOD_{550} x_i^{10} and the angstrom exponent x_i^{11} were added to the model, a good improvement in the RMSE and FS values was observed in all of the tested methods, with the MLP having the best RMSE and FS results among all of the other methods. As can be seen from Table 7, the ground measured AERONET AOD_{550} and the angstrom exponent (i.e., x_i^{10} and x_i^{11}) acted as a correction factor for the CAMS AOD_{550} (i.e., x_i^9) forecasts, hence, the FS for DNI model using MLP has improved

by around 8.5% compared to the model where x_i^{10} and x_i^{11} were not added. The MLP model had an improvement of around 7.5% compared to the best performing model in the remaining models (i.e. kNN, SVR and decision tree). The kNN, SVR and decision tree models had all improved by around 7.28%, 7.3% and 3.34%, respectively, when the new features (i.e., x_i^{10} and x_i^{11}) were added. Overall, a noticeable improvement had been achieved among all the tested models when the new features (i.e., x_i^{10} and x_i^{11}) were added. This is to be expected, since the DNI is very sensitive to AOD_{550} values as shown in **Figure 5.12**, hence, a more accurate AOD_{550} indicators would lead to better performing DNI forecasting model.

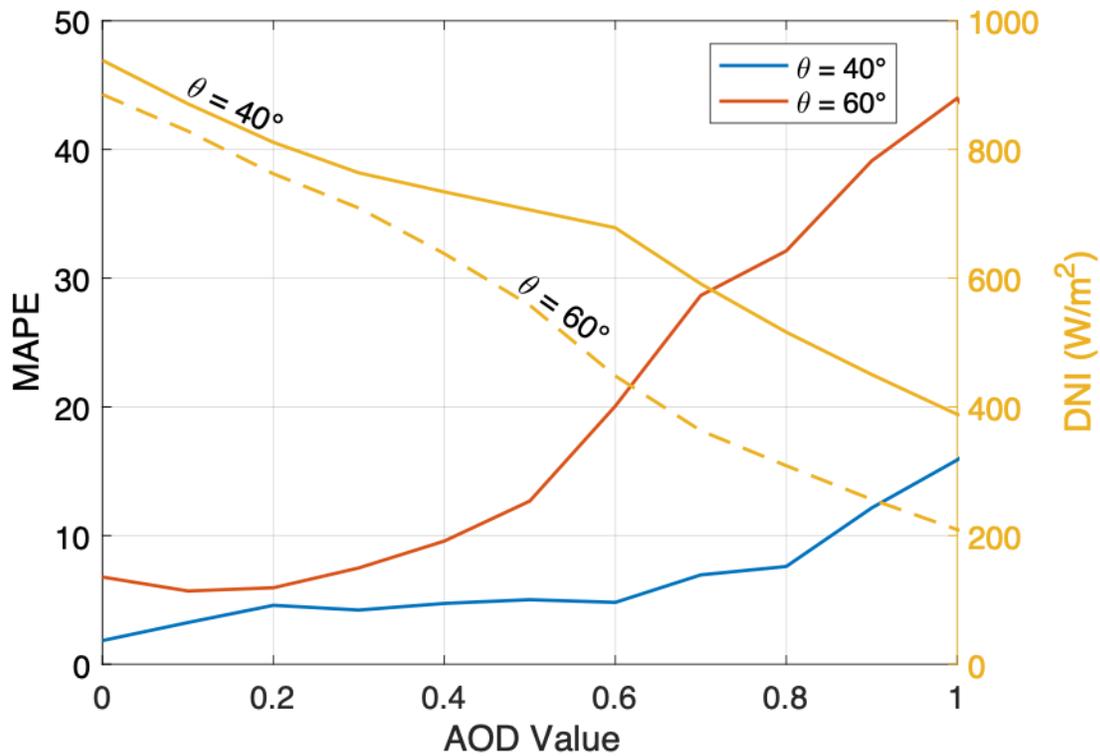


Figure 5.12 Left y-axis shows MAPE for DNI vs AOD, right y-axis shows DNI value vs. AOD. The results were computed at different solar zenith angles $\theta = 40^\circ$ and 60° .

Table 5-7 RMSE results (W/m^2) for DNI model and the forecast skill (FS).

Input Variables	MLP		kNN		SVR		Decision Tree	
	RMSE	FS(%)	RMSE	FS(%)	RMSE	FS(%)	RMSE	FS(%)
$x_i^2, x_i^4, \dots, x_i^8$	76.55	25.24	84.01	17.94	79.40	22.46	81.78	20.13
$x_i^2, x_i^4, \dots, x_i^9$	72.06	29.62	83.64	18.31	78.52	23.31	81.47	20.43
$x_i^2, x_i^4, \dots, x_i^8, x_i^{10}, x_i^{11}$	63.36	38.12	76.18	25.59	71.02	30.64	78.05	23.77

The performance of GHI and DNI using the MLP model was tested under extreme dust events that persisted for a number of days as these values are of special importance to grid operators. These parameters were analyzed for a period of three days starting from 6th to 8th of September 2013. This analysis was conducted using the best set of features as shown in the last row in **Table 5-6** & **Table 5-7**. The average AOD over these three days is 0.84. The AOD behavior during the daytime on these days is depicted in Fig. 15. The forecast skill for GHI when using MLP is 28.34%, whereas for the DNI it is 14.56%.

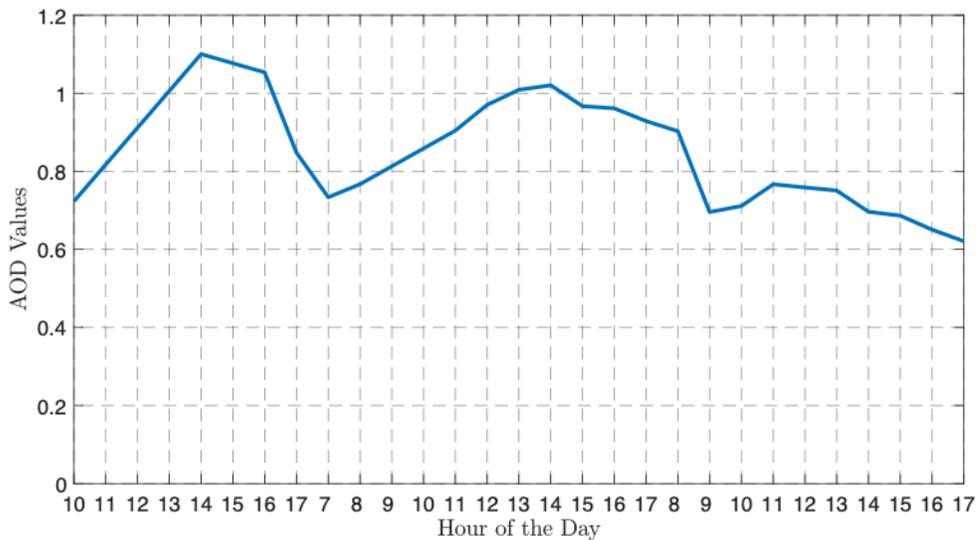


Figure 5.13 Hourly AOD values during sand storm that persisted for three days, starting September 6th to 8th in 2013.

Table 5-8 shows the RMSE and FS for DHI model, measured using the testing dataset, under different methods and features selection schemes. The kNN and SVR models' parameters were optimized again for the DHI model following similar steps discussed earlier for the GHI model. The smart persistence model for the DHI achieved an RMSE of 41.59 (W/m^2). On average, the MLP model outperformed all of the

remaining methods under all feature selection schemes, the decision tree regression had the second best performance. As more features were added to these models, their RMSE and FS had improved for all of the tested methods. At first, improvement was observed when adding the CAMS AOD_{550} x_i^9 in all tested models. As the proposed features (i.e., x_i^{10} and x_i^{11}) were added, the overall accuracy has improved significantly across all models, and slightly for the SVR. For the MLP model, the FS has improved by around 13.4% when compared to the model that utilizes the CAMS AOD_{550} . Similarly, FS has improved by around 7% for the kNN, 4.5% for SVR and 12.5% for decision tree. As for the GHI and DNI models implemented earlier, the MLP model has shown a superior accuracy when compared to the other methods, moreover, the proposed features (i.e., x_i^{10} and x_i^{11}) increased the accuracy noticeably across all the tested methods.

Table 5-8 RMSE results (W/m^2) for DHI model and the forecast skill (FS).

Input Variables	MLP		kNN		SVR		Decision Tree	
	RMSE	FS(%)	RMSE	FS(%)	RMSE	FS(%)	RMSE	FS(%)
$x_i^3, x_i^4, \dots, x_i^8$	31.00	25.45	35.66	14.25	37.89	8.9	36.36	12.56
$x_i^3, x_i^4, \dots, x_i^9$	29.47	29.13	33.81	18.68	36.88	11.31	35.98	13.48
$x_i^3, x_i^4, \dots, x_i^8, x_i^{10}, x_i^{11}$	23.90	42.52	30.88	25.73	35.02	15.78	30.79	25.96

Further analysis for the DHI performance versus the AOD_{550} value is shown in **Figure 5.14**. The MAPE for DHI decreases as the AOD_{550} value increases. The MAPE is relatively small when compared to the MAPE for DNI model under the same solar zenith angle. For example, when $\theta = 60^\circ$, the maximum MAPE for the DHI model is about 15%, while for the DNI model it's is about 45%. As with the previous models, the MAPE for DHI increases as the solar zenith angle increases (i.e. at the beginning and the end of the day). The DHI readings were also compared with the AOD_{550} values in **Figure 5.14** as shown in yellow lines and the right y-axis. As can be clearly seen, the DHI readings increase as the AOD_{550} value increases. This is mainly because of the radiation scattering caused by the AOD_{550} particles in the air. Overall, a significant improvement has been achieved when the new features were added to the model, that's due to the fact that DHI is moderately sensitive to AOD_{550} as shown in Fig. 16. Hence, feeding the tested models with the new set of features (i.e., x_i^{10} and x_i^{11}), would lead to an improved accuracy for the DHI forecasting model across all the implemented methods. **Figure 5.15** shows the MLP

model sensitivity for (GHI/DNI/DHI) under different AOD values. As can be seen from the figure and as discussed earlier in **Figure 5.9**, the DNI is the most sensitive radiation variable to dust; DHI is less sensitive to dust when compared to DNI; and GHI is the least sensitive to dust.

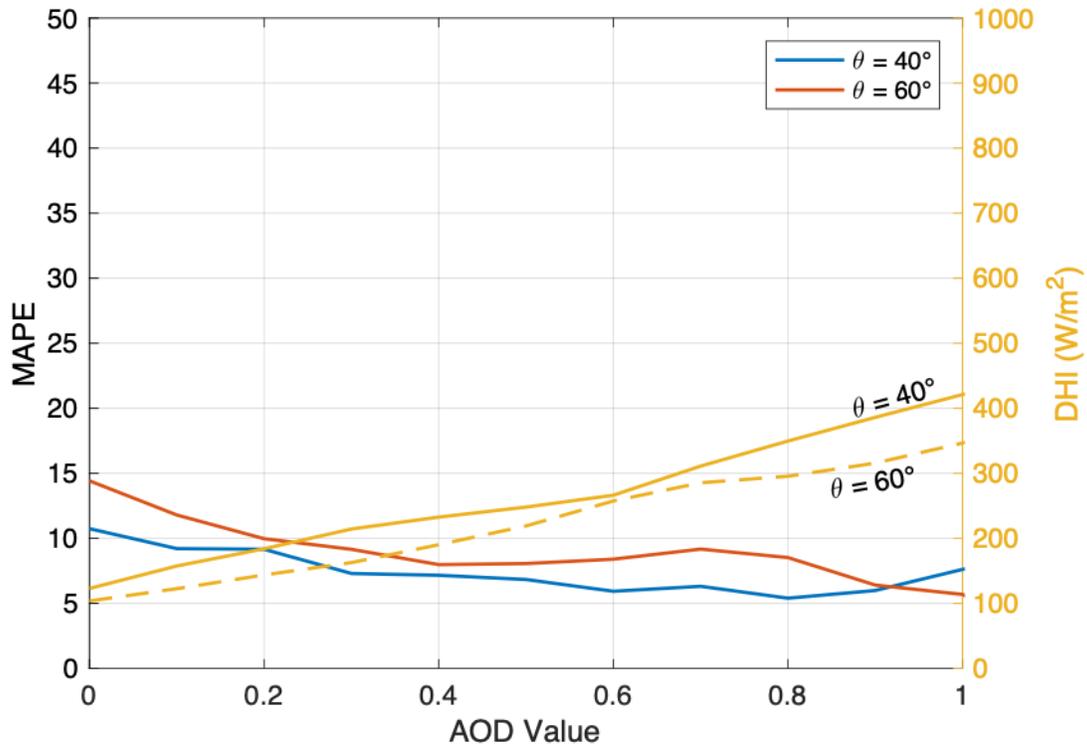


Figure 5.14 Left y-axis shows MAPE for DHI vs AOD, right y-axis shows DHI value vs. AOD. The results were computed at different solar zenith angles $\theta = 40^\circ$ and 60° .

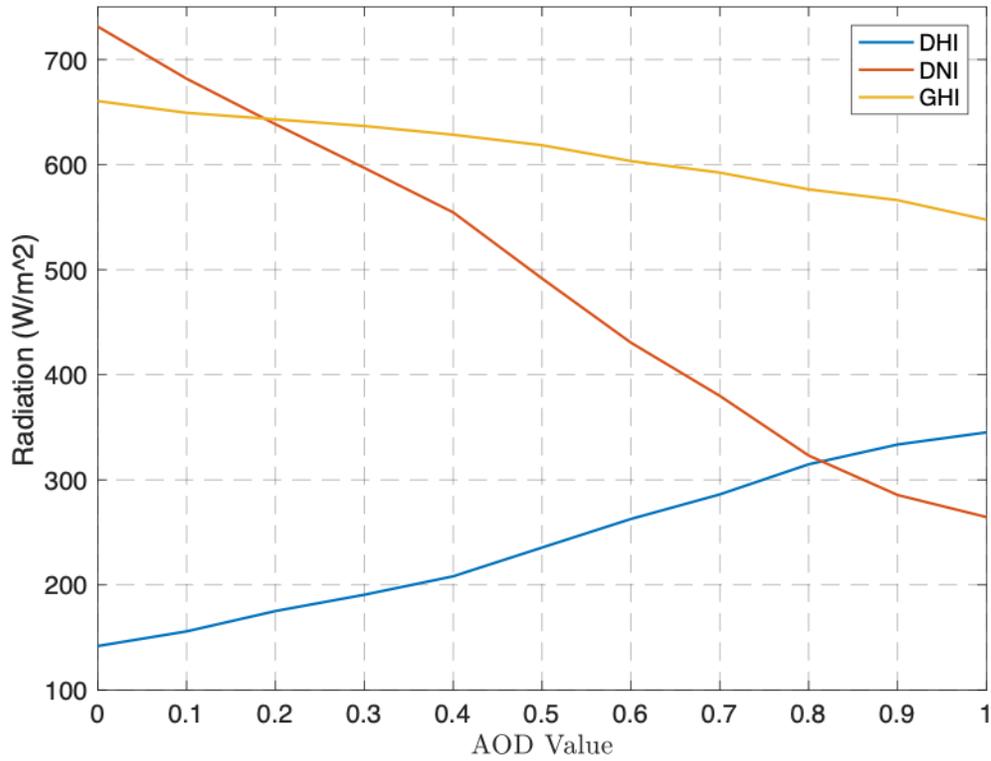


Figure 5.15 MLP sensitivity under different AOD values for GHI, DNI and DHI.

All implemented models were tested under different ratios of training/testing datasets. **Table 5-9** shows the resulted RMSE values averaged over all implemented models for all radiation variables (GHI/DNI/DHI) when tested under the best feature selection scheme. Overall, the error variation under different allocations of training/testing datasets is limited.

Table 5-9 RMSE results (W/m^2) for (GHI/DNI/DHI) models under different training and testing splitting ratios averaged using all methods.

Split Ratio (training/testing)	Radiation Variables		
	GHI	DNI	DHI
85/15	47.44	71.68	29.93
80/20	43.75	70.60	30.14
75/25	44.60	71.62	31.14

The performance of all methods has been tested under high and low AOD. Low values are when $AOD \leq 0.5$, whereas high values are when $AOD > 0.5$. **Table 5-10** shows the performance of all tested models under the high and low AOD values for all

radiation variables (GHI/DNI/DHI). As shown, MLP has the best performance among all methods under all radiation variables, for both the high and low AOD value cases. As can be seen from results, the accuracy of all methods decreases when AOD values are high. **Figure 5.16** shows the MAPE performance for (GHI/DNI/DHI) for each month of the year. MAPE has a slight increase for high AOD months for both GHI and DNI, whereas for DHI the MAPE decreases during these months. The models' performance has been analyzed for periods with above average variability values. The average and standard deviation for these inputs are shown in **Table 5-5**. Only periods with at least 10% standard deviation values above the average were tested. The variables that were considered are the variables that change inconsistently over the day, these variables are the AOD, wind speed, wind direction. **Table 5-11** shows the performance of the different radiation variables across all the models when tested under high variability periods. As can be seen from **Table 5-11**, the MLP and Decision Tree models are the most robust models during high variability periods.

Table 5-10 RMSE results (W/m^2) for all methods under low and high AOD values.

Radiation Variables	AOD Range	Method			
		MLP	kNN	SVR	Decision Tree
GHI	AOD \leq 0.5	25.28	31.90	52.42	41.72
	AOD $>$ 0.5	43.43	56.47	66.46	59.52
DNI	AOD \leq 0.5	51.43	65.86	67.49	74.13
	AOD $>$ 0.5	67.27	90.46	73.77	81.19
DHI	AOD \leq 0.5	21.25	26.49	35.37	25.72
	AOD $>$ 0.5	27.97	36.92	35.99	39.37

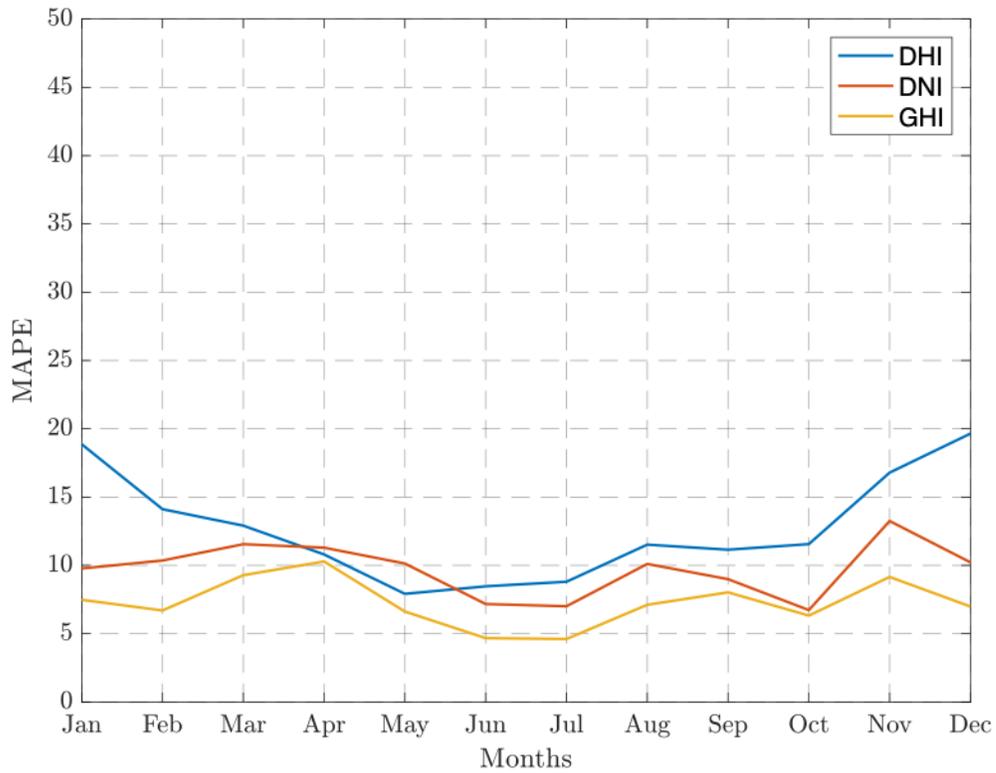


Figure 5.16 MAPE Averaged over all methods for each month of the year.

Table 5-11 RMSE results (W/m^2) for all methods during high variability periods.

Method	Radiation Variables		
	GHI	DNI	DHI
MLP	25.76	39.72	20.74
kNN	39.29	48.24	23.92
SVR	45.07	53.83	27.88
Decision Tree	20.98	37.78	18.10

Chapter 6 Case Study

In this chapter the main case study is presented. The chapter is divided into three main sections. In the first section, the internal architecture of the neural networks were tested under different number of neurons for each hidden layer, to investigate what would be the best internal NN architecture for each of the forecasted variables (i.e. PV panel system, mosque, clinic and office building).

In the second section, the different combination of input features (shown in **Table 3-1** and **Table 3-2**) were tested for each of the forecasted variables, these tested models were also tested under four different forecasting techniques as discussed in the Methodology chapter. The total number of the test cases is 124 models for each one of the forecasted variables, a total of 496 test cases for all of the four forecasted variables. The third section in this chapter investigates the total savings achieved when implementing the proposed forecasting model combined with the CTES (shown in Figure 1.1 and Figure 3.1), the test cases include different chiller and CTES capacity values.

6.1 Neural Networks Internal Architecture Results

As discussed earlier, the implemented neural networks method in this work is the feedforward network. In order to find the best architecture for each forecasted variable (i.e. PV panel system, mosque, clinic and office building), each one of these forecasted variables was tested under different internal NN architectures. The meaning of architecture in this context is the number of neurons in each hidden layer in the NN, while the internal neurons between each two consecutive layers are fully connected. Each forecasted variable has been tested under three hidden layers and a different number of neurons on each layer, then the best architecture was chosen for each forecasted variable. All the forecasted variables were tested under the feature selection scheme labelled as 31 in **Table 3-2**. This feature combination was chosen as it represents the most complex set of features when compared to the other sets of features, even though

other feature combinations might have better forecasting results for some of the forecasted variables.

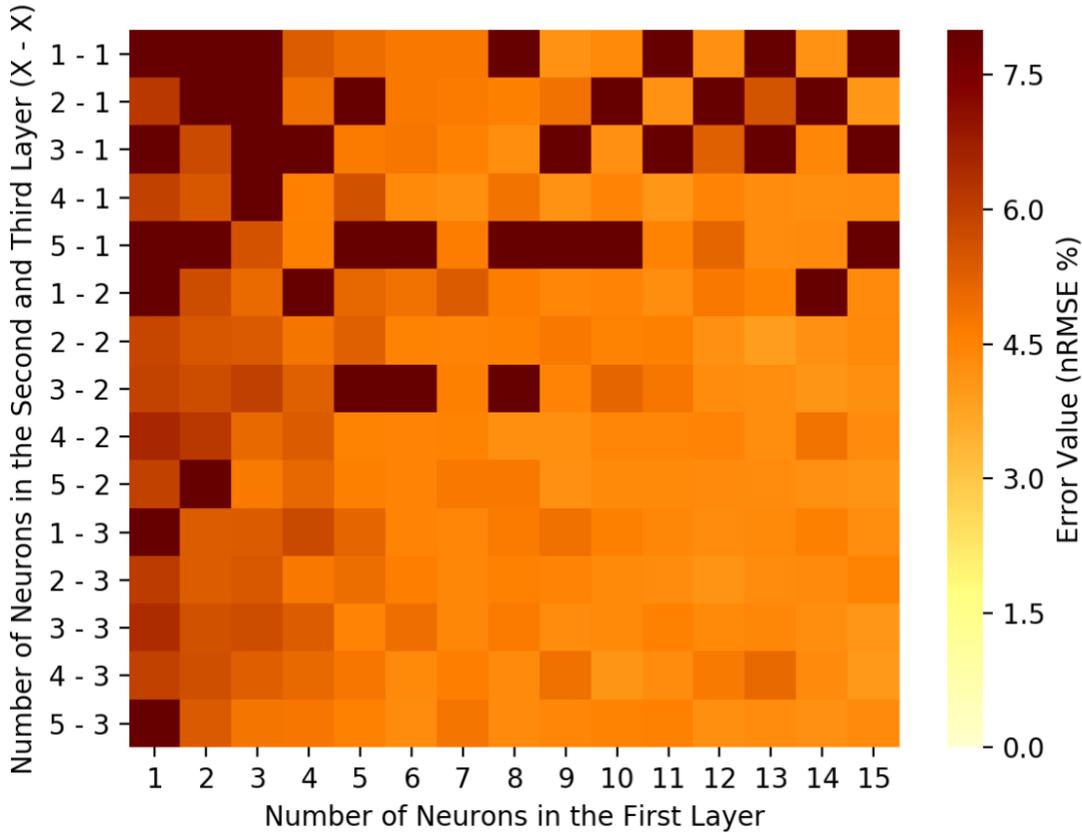


Figure 6.1 PV panel system forecasted generation results under different neural networks architectures.

The total number of input features for the tested feature set is 12 for each of the forecasted variables. Each forecasted model has been tested under different number of neurons for the first layers, second layer and the third layer. These different combinations are shown as a heatmap in **Figure 6.1** to **Figure 6.4** for each of the forecasted variable. The x-axis represents the number of neurons in the first layer, starting from 1 to 15 neurons. The y-axis represents the different combinations of the second and third layer, so, the first number on the y-axis represents the number of neurons in the second layer, while the second number on the y-axis represents the number of neurons on the third layer. The second layer has different combinations starting from 1 to 5 neurons, while the third layer has different combinations starting from 1 to 3 neurons. The total number of

the different architectures is 225 for each of the forecasted variables. The results in **Figure 6.1** to **Figure 6.4** are shown in nRMSE(%) discussed earlier.

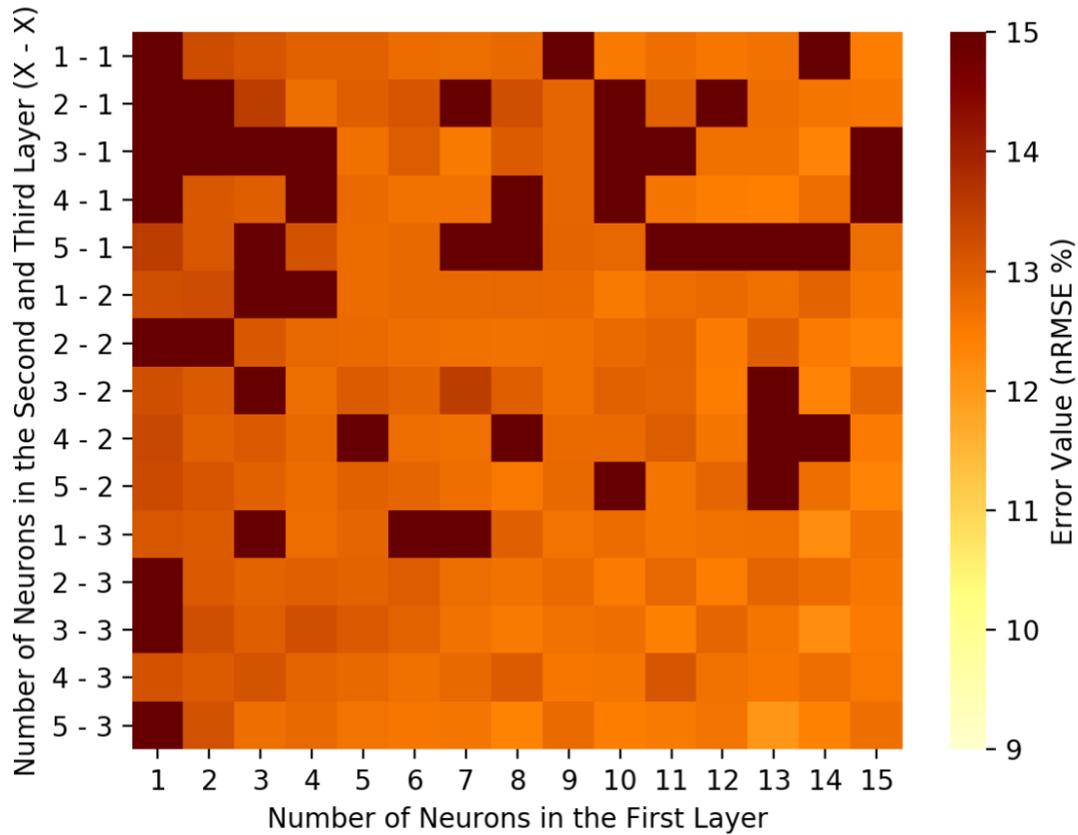


Figure 6.2 Mosque load forecasted results under different neural networks architectures.

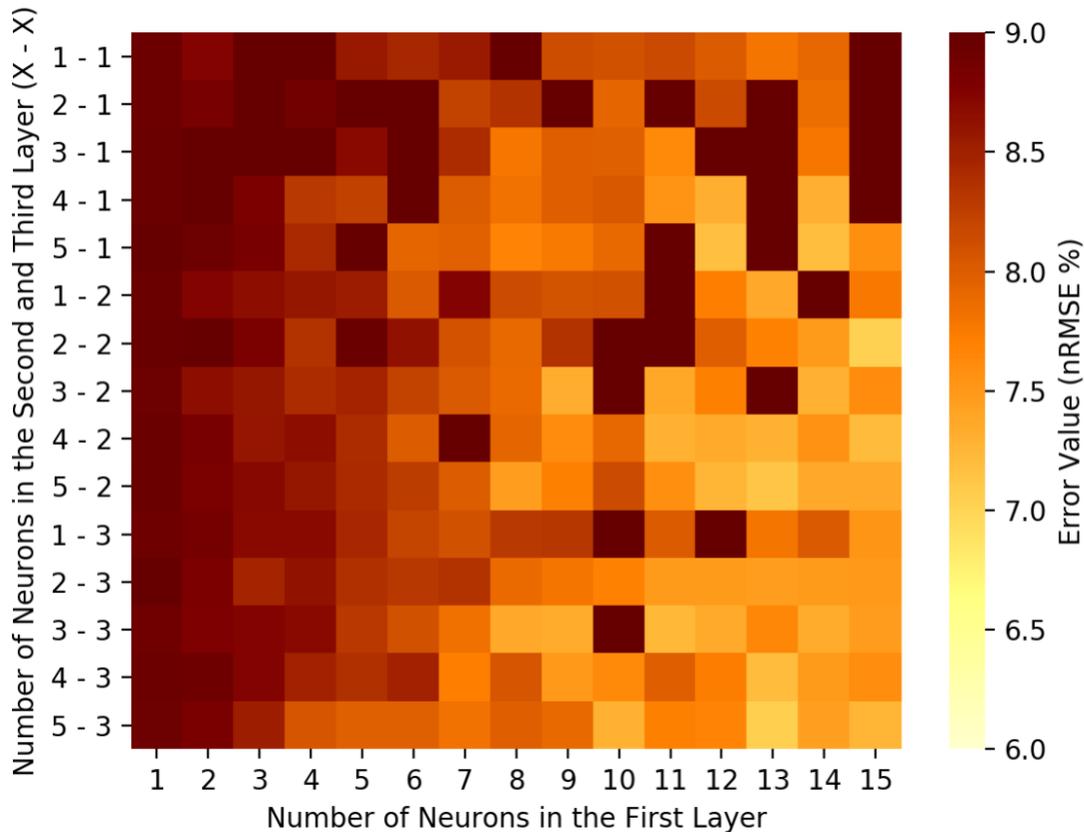


Figure 6.3 Clinic load forecasted results under different neural networks architectures.

As can be clearly seen in all of the tested models, the error rate decreases as the number of neurons increases. This can be clearly seen in the first layer, when we go from left to right on the x-axis in all of the figures. Similarly this also applies to the second and the third layer can as be seen in **Figure 6.1** to **Figure 6.4**. Some forecasted variables are more sensitive to the internal architecture than the others. This can be clearly seen in **Figure 6.3**, for the clinic it is very apparent that the error decreases as we go to the bottom right (i.e. more neurons on each layer), this also can be seen in **Figure 6.1**. However, when compared to **Figure 6.2** for the mosque, it can be seen that the mosque is less sensitive to the changes in the internal architecture when compared to the other forecasted variables.

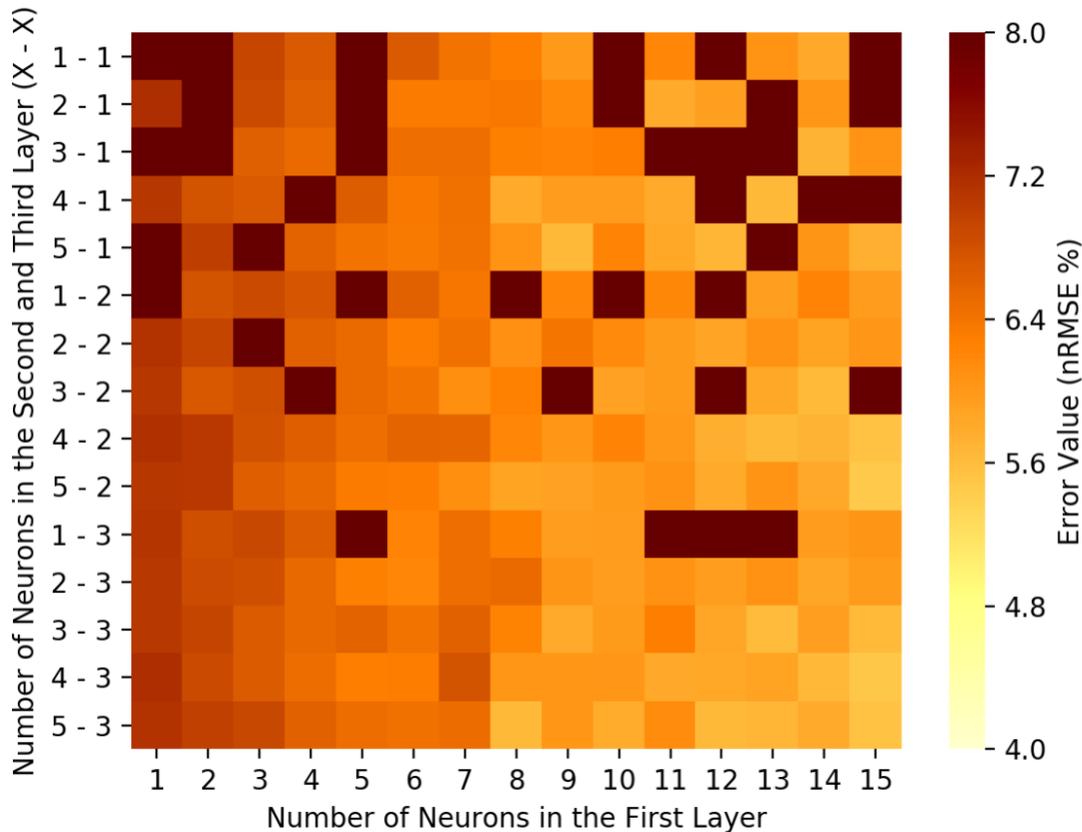


Figure 6.4 Office building load forecasted results under different neural networks architectures.

6.1.1 Conclusion

This section investigates the performance of different architectures of the feedforward NN for each of the forecasted variables (i.e. PV panel system, mosque, clinic and office building). The forecasting accuracy using nRMSE was tested for each forecasted variable under 225 different NN architecture. In general, the accuracy of the forecasted variables increases as the number of neurons in the NN increases. However, some forecasted variables are less sensitive to the NN architecture than the other forecasted variables. Mosque is the least sensitive the different architectures in the NN as can be seen in **Figure 6.2**.

6.2 Forecasting Results

6.2.1 PV panel results

The PV panel forecasting results are shown in **Figure 6.5**, each row in the heat map refers to a feature combination as shown in **Table 3-2**, each column refers to a forecasting method as described in earlier. The first 16 feature refer to individual feature selection combination, meaning that, only one variable was used to build and test the that specific forecasting model. The remaining features are different combinations of these individual features. The best individual feature when performing the PV panel power forecasts is the $x_i^{historical}$ which is x_i^{18} when doing forecasting for the PV panels. The best results for the model are shown in **Table 6-1** under different error metrics, this was achieved using the SVR model, when using the set of features as indicated by number 30 in **Table 3-2**. The set of features include the forecasted GHI, DNI, time and date variables, high cloud cover, dust AOD, wind speed, wind direction and the previous day PV power generation at the same hour. The individual features 1,2,3,4,13 and 19 have good results when they are used alone without combining them with other features. These features are the clear sky GHI, clear sky DNI, forecasted GHI, forecasted DNI, the hour of the day and the previous day PV power generation. That's expected when building a forecasting model for the PV panels, as these features contribute more to the output power of the PV panels when compared with the other features. It is also worth noting that the remaining individual features have a big error gap compared to these 5 best individual features. This gap in the error is also present when comparing these individual features with the remaining different combinations of the features. The weakest model occurs when using the wind speed and the wind direction alone as inputs without using other input features under the kNN forecasting model.

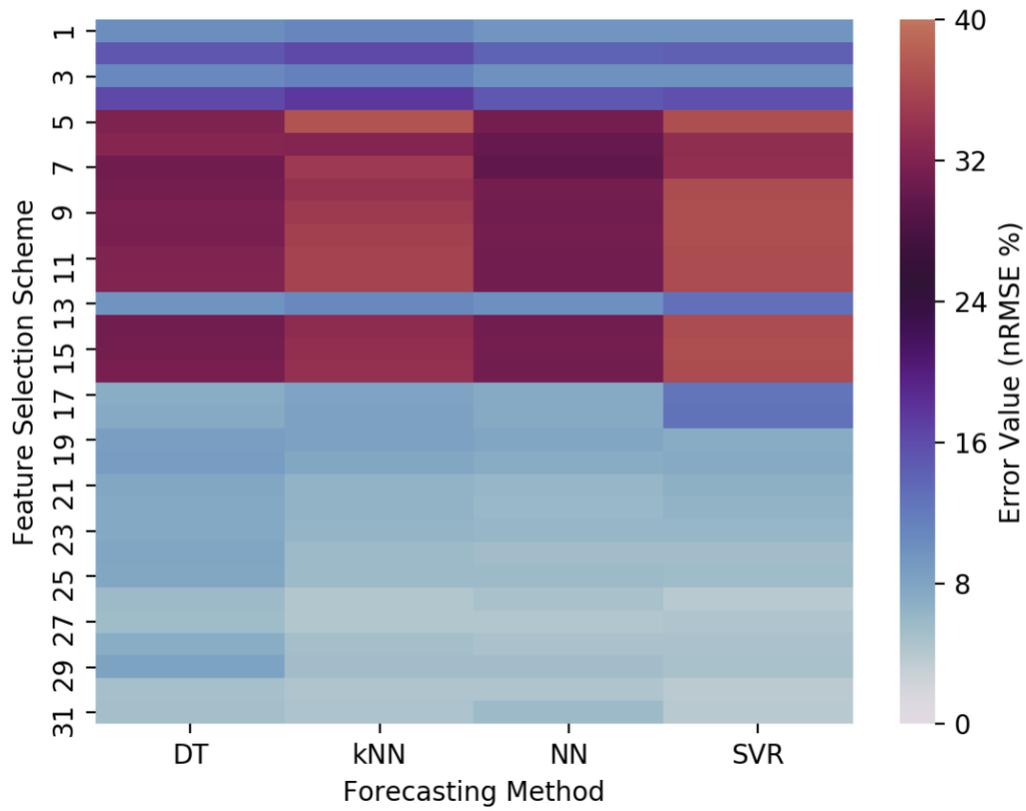


Figure 6.5 PV Panel forecasting results under different methods and features.

Table 6-1 PV best forecasting results using SVR and multiple error metrics.

Error	RMSE (W/M ²)	nRMSE (%)	MAE	nMAE (%)
	3834.95	3.72	2502.66	2.36

6.2.2 Buildings Load results

Similarly, as the PV forecasts, all the building types were tested under different features combinations as shown in **Table 3-2**. The following subsections will discuss the forecasting results for each of these building types (i.e. mosque, clinic and office building)

6.2.3 Mosque

The mosque forecasting results tested under different forecasting methods and feature selections schemes are shown in the heatmap in **Figure 6.6**. The different feature combinations were discussed earlier in **Table 3-2**. The top individual features in terms of accuracy when building the forecasting model are two features, the hour of the day and the previous week power consumption for the mosque at the same hour, this can be clearly seen in the heatmap as features 13 and 19. Unlike the PV forecasts, the individual features have a lower error gap when compared to the combined feature combinations. When compared to the other forecasted variables (i.e. PV panel system, clinic and office building), the mosque is the hardest to forecast, this can be seen in the relatively high error rate when compared with the other forecasted variables. This relatively high error rate is because of the high variability in the load profile of the mosque, meaning that the mosque has 5 different peaks, these 5 load peaks are dependent on the solar time and less on the hour of the day. The high error in the mosque is also caused by the unpredictability of the cooling load, as the number of people attended the prayers is varied, hence, this causes an increase in the variability of the cooling load. The load profile of the mosque is also dependent on the on the weekday and weekend schedule, that's because on Friday noon the Jumaa prayer takes place. Moreover, the mosque is usually crowded during the weekend, as people pray in the mosque instead of their working place. The best model when building a forecasting was achieved when applying the kNN under the feature combination numbered as 29 in **Table 3-2**. The set of features for this model include the temperature, previous week power consumption at the same hour, hour of the day, month of the year, the day of the year, cloud cover and the dust AOD information. The kNN model results are shown in **Table 6-2** under different error metrics. It can be seen from **Table 6-2** that the gap in the error between the RMSE and the MAE is relatively

high, as the RMSE is more sensitive to the outliers in the results, this means that the outliers in the mosque load profile are high, and hence is harder to forecast compared to the other methods.

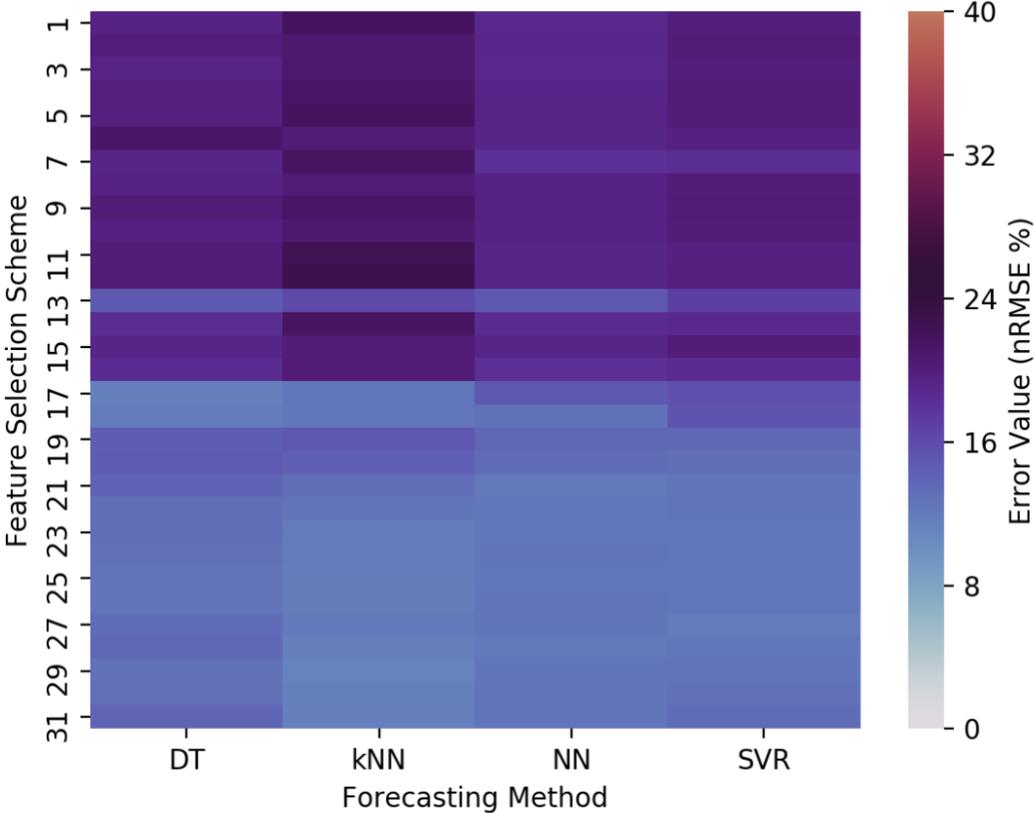


Figure 6.6 Mosque load forecasting results under different methods and features.

Table 6-2 Mosque best forecasting results using kNN and multiple error metrics.

Error	RMSE (Watts)	nRMSE (%)	MAE(Watts)	nMAE (%)
	17305.2	11.39	11815.2	7.34

6.2.4 Clinic

The clinic forecasting results tested under different forecasting methods and feature selections schemes are shown in the heatmap in **Figure 6.7**. The different feature combinations were discussed earlier in **Table 3-2**. The top individual features in terms of accuracy when building the forecasting model for the clinic are three features, the temperature, the previous week power consumption for the clinic at the same hour and the month of the year, this can be clearly seen in the heatmap as features 7, 14 and 19. Similar to the mosque forecasting models, the individual features have a lower error gap when compared to the combined feature combinations, unlike the PV panels shown in **Figure 6.5**. Also, the error gap between the best and worst model in the clinic models is narrower than the gap in the mosque results, meaning that the features in **Table 3-1** have weights close to each other when building the forecasting model for the clinic. Also it means that the clinic load profile is smoother than the mosque load profile as shown earlier in **Figure 4.2**, so, as the load profile gets smoother the effect of the input features decrease as we reach to straight line, at that point the input feature has no effect on the model output, and the output of the model is the same regardless of the input feature. When compared to the other forecasted variables (i.e. PV panel system, clinic and office building), the clinic has the smoothest load profile, so the gap between the maximum and the minimum load is the smallest among all the other forecasted variables. The load profile of the clinic is also dependent on the on the weekday and weekend schedule. The best model when building a forecasting was achieved when applying the SVR under the feature combination numbered as 30 in **Table 3-2**. The set of features for this model include the temperature, previous week power consumption at the same hour, hour of the day, month of the year, the day of the year, cloud cover, the wind data, GHI alongside with the dust AOD information. The SVR model results are shown in **Table 6-3** under different error metrics. It can be seen from **Table 6-3** that the gap in the error between the RMSE and the MAE is relatively small as when compared to the mosque gap, as the RMSE is more sensitive to the outliers in the results, this means that the outliers in the clinic load profile are small when compared to the mosque, and hence is easier to forecast compared to mosque.

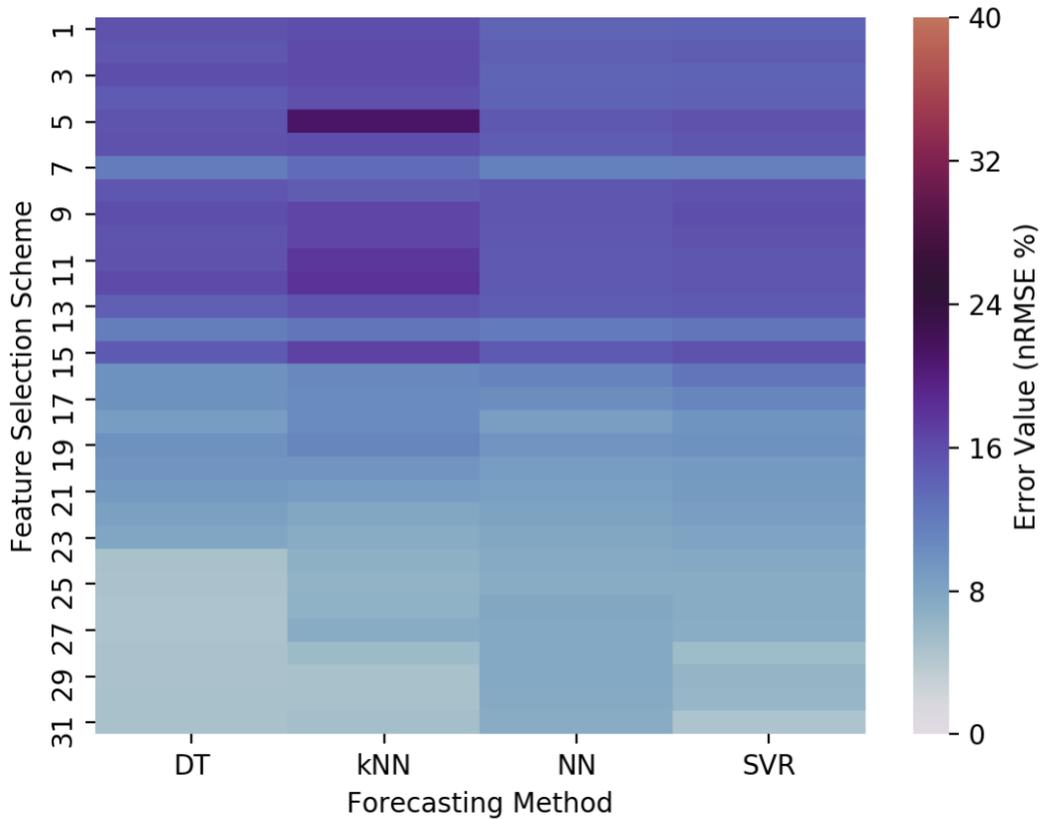


Figure 6.7 Clinic load forecasting results under different methods and features.

Table 6-3 Clinic best forecasting results using SVR and multiple error metrics.

Error	RMSE (Watts)	nRMSE (%)	MAE(Watts)	nMAE (%)
	4629.0	4.56	2829.0	2.76

6.2.5 Office building

The office building forecasting results tested under different forecasting methods and feature selections schemes are shown in the heatmap in **Figure 6.8**. The different feature combinations were discussed earlier in **Table 3-2**. The top individual features in terms of accuracy when building the forecasting model for the office building are three features, the temperature, the previous week power consumption for the office building at the same hour and the month of the year, this can be clearly seen in the heatmap as

features 7, 14 and 19, these top features are similar to the top features for the clinic forecasting model. Also, as the mosque and the clinic forecasting models, the individual features have a lower error gap when compared to the combined feature combinations, unlike the PV panels shown in **Figure 6.5**. Also, the error gap between the best and worst model in the office building models is narrower than the gap in the mosque and clinic results, meaning that the features in **Table 3-1** have weights close to each other when building the forecasting model for the office building. The load profile of the office building is similar to the mosque and the clinic, as it also dependent on the on the weekday and weekend schedule. The best model when building a forecasting was achieved when applying the SVR under the feature combination numbered as 30 in **Table 3-2**. The set of features for this model include the temperature, previous week power consumption at the same hour, hour of the day, month of the year, the day of the year, cloud cover, the wind data, GHI alongside with the dust AOD information. The best set of features are similar to the best set of features for the clinic. The SVR model results are shown in **Table 6-4** under different error metrics. It can be seen from **Table 6-4** that the gap in the error between the RMSE and the MAE is relatively small as when compared to the mosque gap, as the RMSE is more sensitive to the outliers in the results, this means that the outliers in the office building load profile are small when compared to the mosque, and hence is easier to forecast compared to mosque. Moreover, this gap is smaller in the office building when compared with the clinic as well, as the gap between nRMSE and nMAE is 1.79% in the clinic, while in the office building this gap is only 1.25%. Meaning that the outliers in the building results are the lowest among all the other forecasted variables. This can be seen also in the results, as the office building has the lowest error when compared to the remaining forecasted variables (i.e. PV panel system, mosque and clinic).

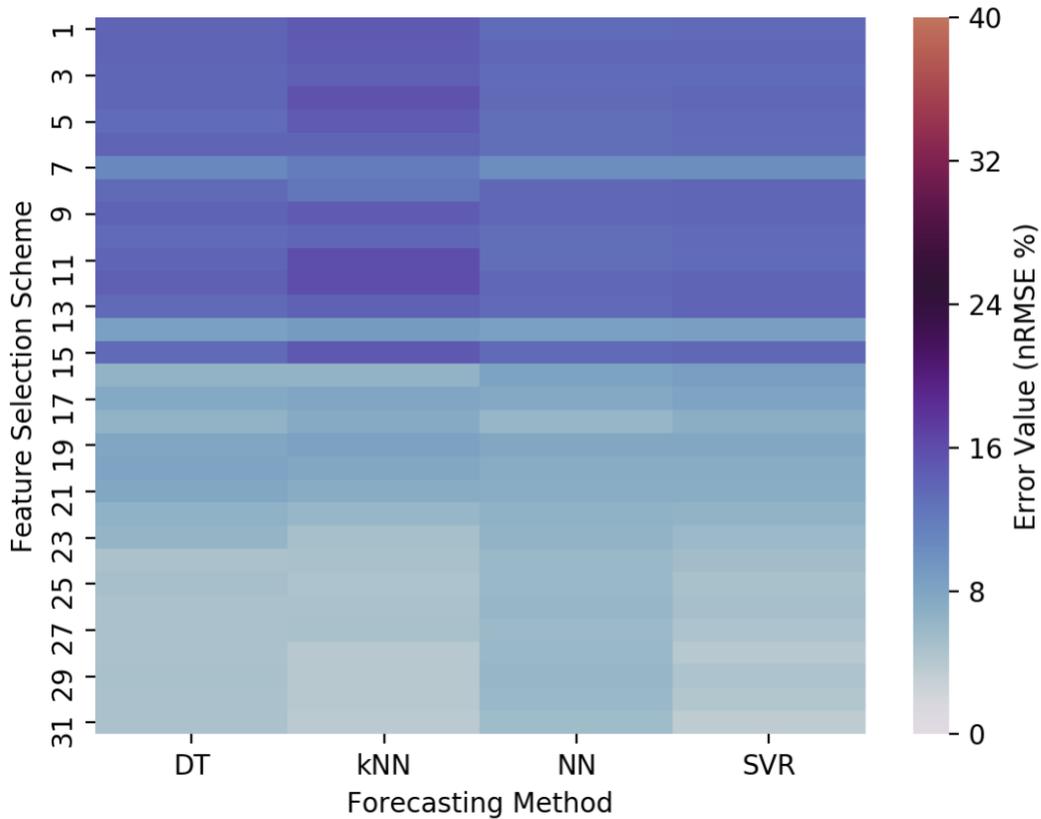


Figure 6.8 Office building load forecasting results under different methods and features.

Table 6-4 Office building best forecasting results using SVR and multiple error metrics.

Error	RMSE (Watts)	nRMSE (%)	MAE(Watts)	nMAE (%)
	4761.6	3.53	3368.0	2.28

6.2.6 Conclusion

In this section, different combinations of features were tested for each of the forecasted variables (i.e., PV panel system, mosque, clinic and office building). Individual features as well as different feature combinations were tested. Each set of features was tested under four different forecasting methods Decision Trees, kNN, NN and SVR. A

total of 124 test cases were conducted for each forecasted variable. nRMSE of 3.73%, 11.39%, 4.56% and 3.53% were achieved for the PV panel system, mosque, clinic and the office building, respectively.

6.3 Total savings using the proposed method

In this section the total savings is discussed by comparing the proposed method with the baseline model. The proposed method is where building-level load forecasts and PV forecasts are taken into account to determine CTES charge schedule for the next day. The baseline model is where the CTES charge for tomorrow is scheduled to be fully charged to cover loads of the entire district.

The baseline and the proposed system were tested under different scenarios. The first test case includes changing the maximum chiller capacity that met the cooling load. Any cooling load that exceeds the maximum chiller capacity is met using the CTES charge. As described earlier, the CTES charge for the baseline system is fully charged during the night regardless of the total cooling demand for tomorrow. On the other side, the proposed system is charged based on the total forecasted load plus the error factor, which was chosen to be close to the worst forecasting error, which is around 10%. The total cooling load is forecasted from 07:00 a.m. to 05:00 p.m., the CTES is charged based on the demand during this period plus 10% of the total forecasted load. Both the baseline and the forecasting systems were tested under different maximum chiller capacity scenarios, as discussed below.

6.3.1 Systems tested under different chiller values

In this section, the baseline system and the forecasting system were both tested under different chiller capacity values.

6.3.1.1 180 kW maximum chiller capacity

6.3.1.1.1 Baseline method

In this test case, the maximum chiller capacity is 180 kW, while the peak cooling load is 219,16 kW at 01:00 p.m., taking into consideration that the load is forward averaged as described earlier in the data section. **Figure 6.9** shows the overall system under the baseline method. The CTES is charged during the night from 12:00 a.m. to 06:00 a.m., then during the day, the CTES charge is discharged when the cooling load exceeds the chiller capacity. And finally, any charge that's remaining after 05:00 p.m. is calculated. As can be seen from the plot, the CTES is being charged during the night at a steady rate until 06:00 a.m., after that, the CTES stopped charging and in standby mode. As can be seen from the plot, the standby mode is active at 07:00 a.m., as the maximum cooling load is around 156 kW, which is less than the maximum chiller capacity. Hence, the cooling load is met using only the chiller, and the CTES charge is preserved for the upcoming hours. Now, at 08:00 a.m., the total cooling load starts increasing, and the load is 191 kW, which is higher than the maximum capacity. Hence, the total cooling load must be met using both the maximum chiller capacity and the preserved charge in the CTES. As can be seen at 08:00 the CTES charge starts decreasing at a rate equal to the difference between the load and the maximum chiller capacity, which is around 10 kWh at 08:00 a.m.. The system starts discharging during the subsequent hours as can be seen in the plot. The maximum discharge rate occurs at 01:00 p.m., as the maximum cooling load is around 220 kW, hence, the difference between the cooling load and the maximum chiller capacity is 20 kWh. The discharge rate starts decreasing after 01:00 p.m. as shown in the plot. After 05:00 p.m. there is still a remaining charge in the CTES that has not been fully utilized yet, the remaining charge in the CTES is equal to 64 kWh when applying the baseline method.

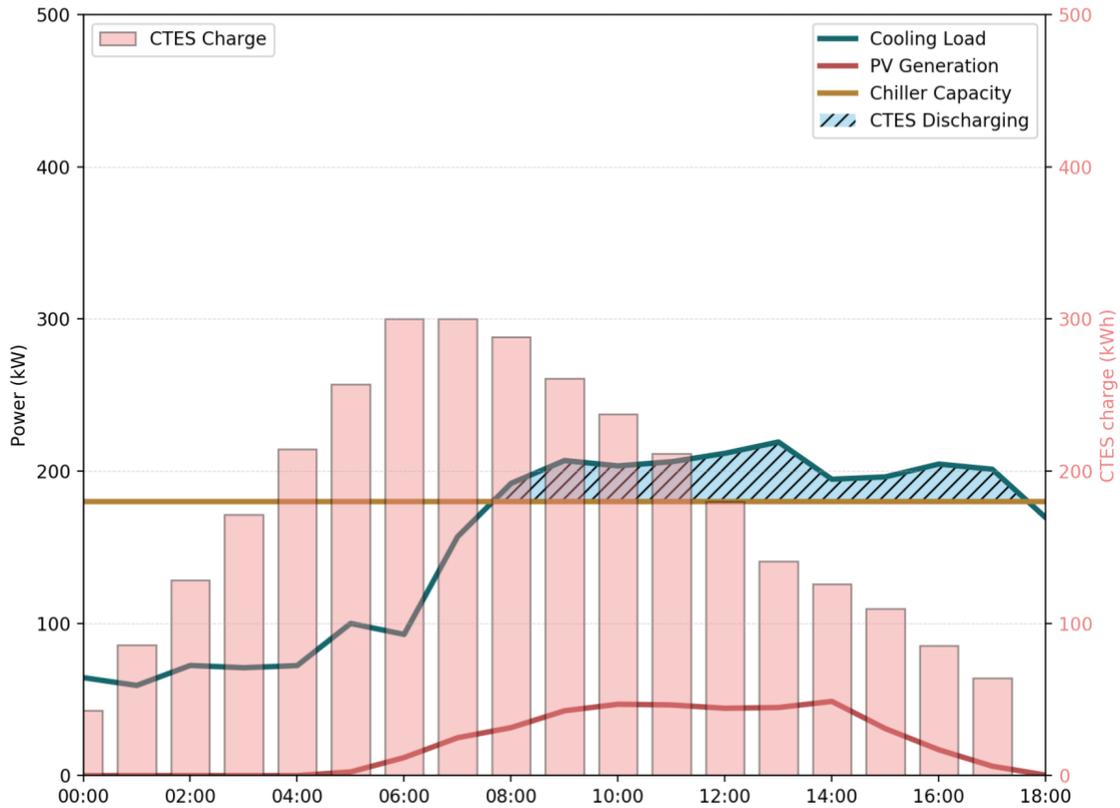


Figure 6.9 CTES charge and discharge rate using the baseline system under 180 kW chiller.

6.3.1.1.2 Forecasting method

In this test case, the maximum chiller capacity is 180 kW, while the peak cooling load is 219,16 kW at 01:00 p.m. **Figure 6.10** shows the overall system under the forecasting method. The CTES is charged during the night from 12:00 a.m. to 06:00 am., then during the day, the CTES charge is discharged when the cooling load exceeds the chiller capacity. And finally, any charge that's remaining after 05:00 p.m. is calculated. As can be seen from the plot, the CTES is being charged during the night at a steady rate until 06:00 a.m., the charge of CTES during the night is equal to the total cooling demand forecasted for tomorrow plus the 10% error factor. After that, the CTES will stop charging and will be in standby mode similar to the baseline method. The standby mode is active

during 07:00 a.m., while the total cooling load is around 156 kW, which is less than the maximum chiller capacity. Hence, the cooling load is met only using only the chiller, and the CTES charge is preserved for the upcoming hours. Now, at 08:00 a.m., the total cooling load starts increasing, and the load is 191 kW, which is higher than the maximum capacity. Hence, the total cooling load must be met using both the maximum chiller capacity and the preserved charge in the CTES. As can be seen at 08:00 the CTES charge starts decreasing at a rate equal to the difference between the load minus the maximum chiller capacity, which is around 10 kWh at 08:00 a.m.. The system starts discharging in the subsequent hours as can be seen in the plot. The maximum discharge rate occurs at 01:00 p.m. The discharge rate starts decreasing after 01:00 p.m. as shown in the plot. After 05:00 p.m. there is still a remaining charge in the CTES that has not been fully utilized yet, the remaining charge in the CTES is equal to 23 kWh when applying the forecasting method.

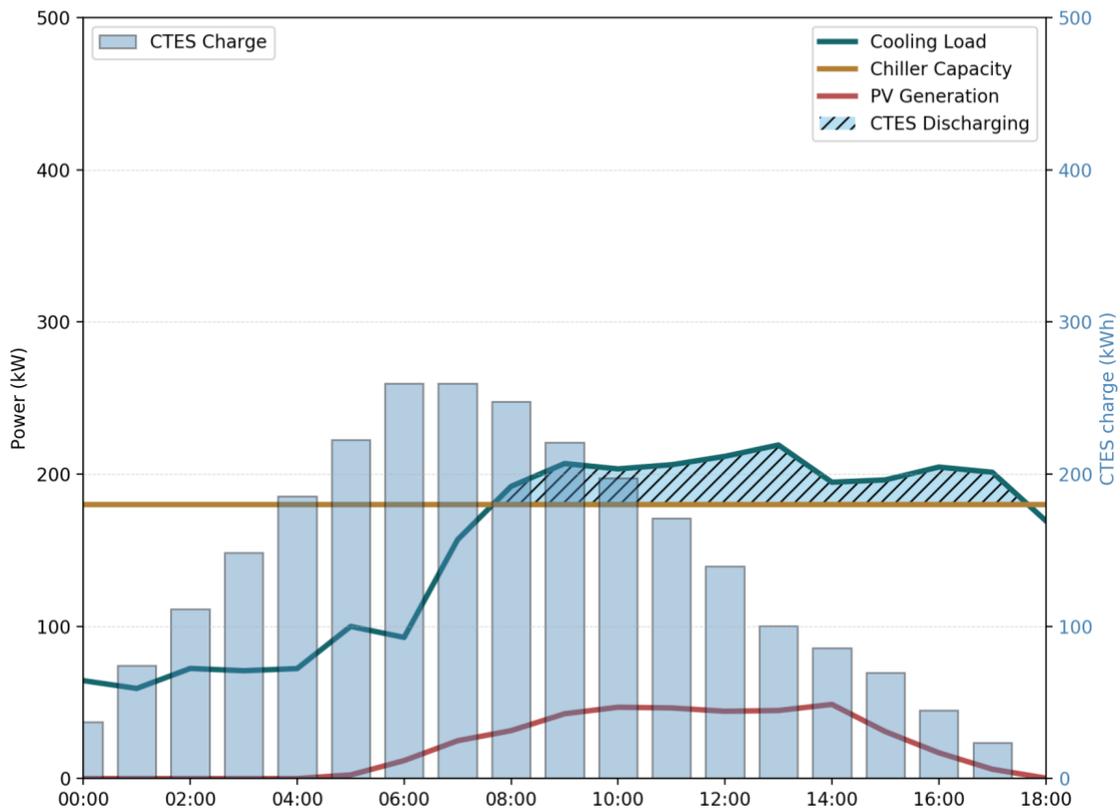


Figure 6.10 CTES charge and discharge rate using the forecasting system under 180 kW chiller.

6.3.1.2 190 kW maximum chiller capacity

In this test case, the maximum chiller capacity has been increased to be 190 kW for both the baseline method and the forecasting method. As the chiller capacity increase, the required CTES charge for the next day decreased. **Figure 6.11** shows the baseline system under the 190 kW maximum chiller capacity. Similar as the previous scenarios, the CTES is charging at the previous night at a steady rate, and the CTES charge is used when the total cooling load exceeds the maximum chiller capacity. However, the main difference when comparing this scenario and the 180 kW chiller capacity scenarios is the total CTES charge that is used in the next day. In the baseline method, the CTES is

charged fully during the night regardless of the required CTES charge. As can be seen from the plot, the CTES charge is used starting at 08:00 a.m., similar to the previous scenario. However, in this scenario, the discharge rate at 08:00 is lower, as the total cooling load is 191 kW and the maximum chiller capacity is 190 kW, hence, the required discharge is only 1 kWh. This also applies to the subsequent hours. The CTES is discharging until 05:00 p.m., similar to the previous scenario. However, the remaining charge in the CTES is higher in this case, as the CTES discharge rate is lower during the peak hours. The remaining charge in the CTES at 05:00 p.m. is 164 kWh, which is much higher than the previous case.

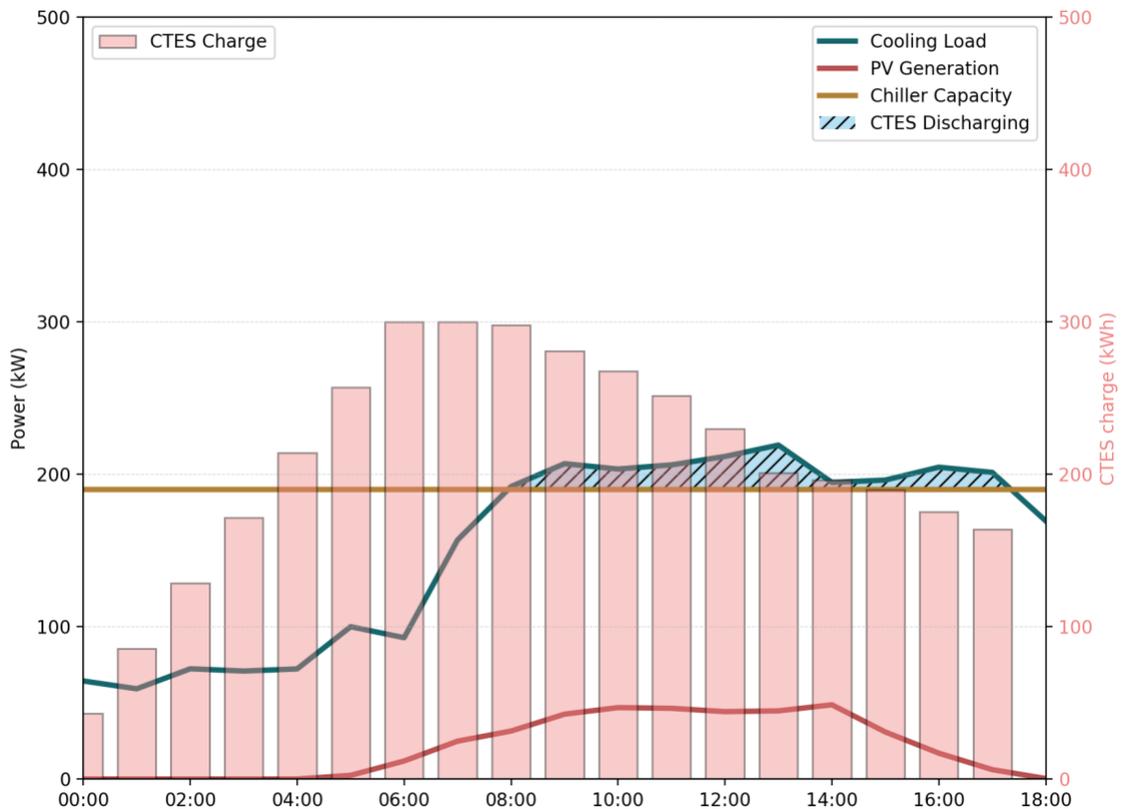


Figure 6.11 CTES charge and discharge rate using the baseline system under 190 kW chiller.

Figure 6.12 shows the system applied using the forecasting method. The system is charging the CTES during the night based on the next day cooling demand plus the 10% error factor. The CTES starts discharging from 08:00 a.m. until 05:00 p.m., when the cooling load exceed the maximum chiller capacity. At the end of the day, at 05:00 p.m., the remaining CTES charge is equal to 13 kWh, which is lower than the previous case, because the total charge required in the scenario is lower, hence, the total error in the CTES is lower as well.

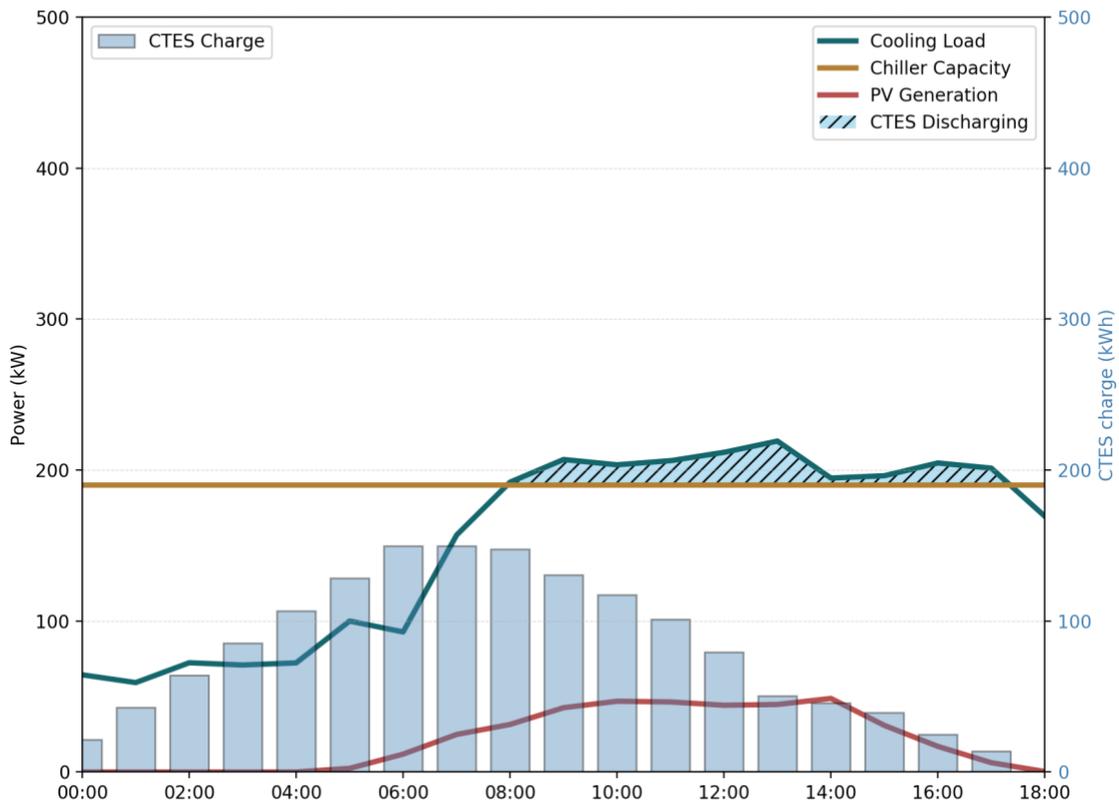


Figure 6.12 CTES charge and discharge rate using the forecasting system under 190 kW chiller.

6.3.1.3 200 kW maximum chiller capacity

In this test case, the maximum chiller capacity has been increased to be 200 kW for both the baseline method and the forecasting method. Similar to the previous scenario, since the chiller capacity has increased, the required CTES charge for the next day has also decreased. **Figure 6.13** shows the baseline system under the 200 kW maximum chiller capacity. Similar as the previous scenarios, the CTES is charging at the previous night at a steady rate, and the CTES charge is used when the total cooling load exceeds the maximum chiller capacity. However, the main difference when comparing this scenario and the previous scenarios, is that in this case the CTES charge is used in two separate periods of the day, meaning that, the CTES started discharging when the cooling load exceeds the chiller capacity at 09:00 a.m., and stopped discharging at 02:00 p.m., when there is a drop in the load. Then again, the CTES started discharging at 04:00 p.m. In this scenario, the discharge rate at all hours is lower than the previous scenarios, since the chiller capacity is lower, hence, the required charge from the CTES is also lower. The remaining charge in the CTES is higher in this case than the previous cases. The remaining charge in the CTES at 05:00 p.m. is 246 kWh, which is higher than the previous cases.

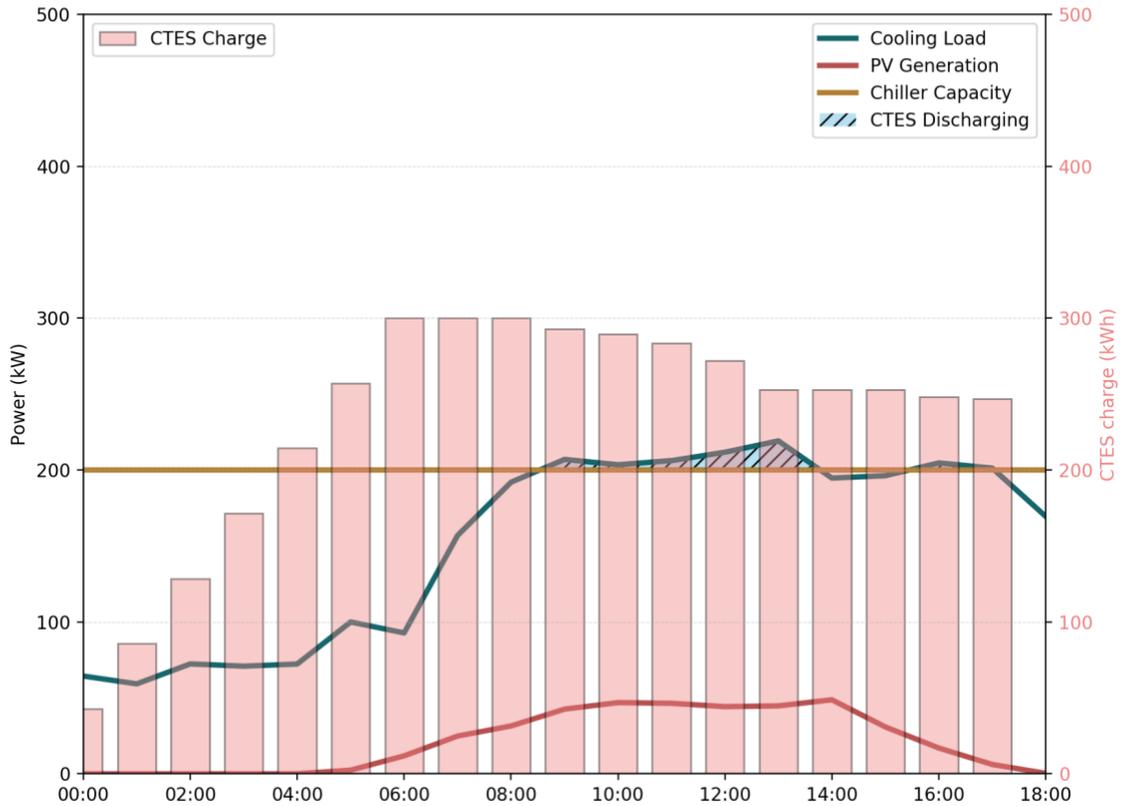


Figure 6.13 CTES charge and discharge rate using the baseline system under 200 kW chiller.

Figure 6.14 shows the system applied using the forecasting method. The system is charging the CTES during the night based on the next day cooling demand plus the 10% error factor. The CTES starts discharging from 09:00 a.m. until 01:00 p.m., then again at 04:00 p.m., when the cooling load exceed the maximum chiller capacity. At the end of the day, at 05:00 p.m., the remaining CTES charge is equal to 5,32 kWh, which is lower, than the previous cases, as the total CTES charge required in the scenario is lower, hence, the total error in the charge is lower as well.

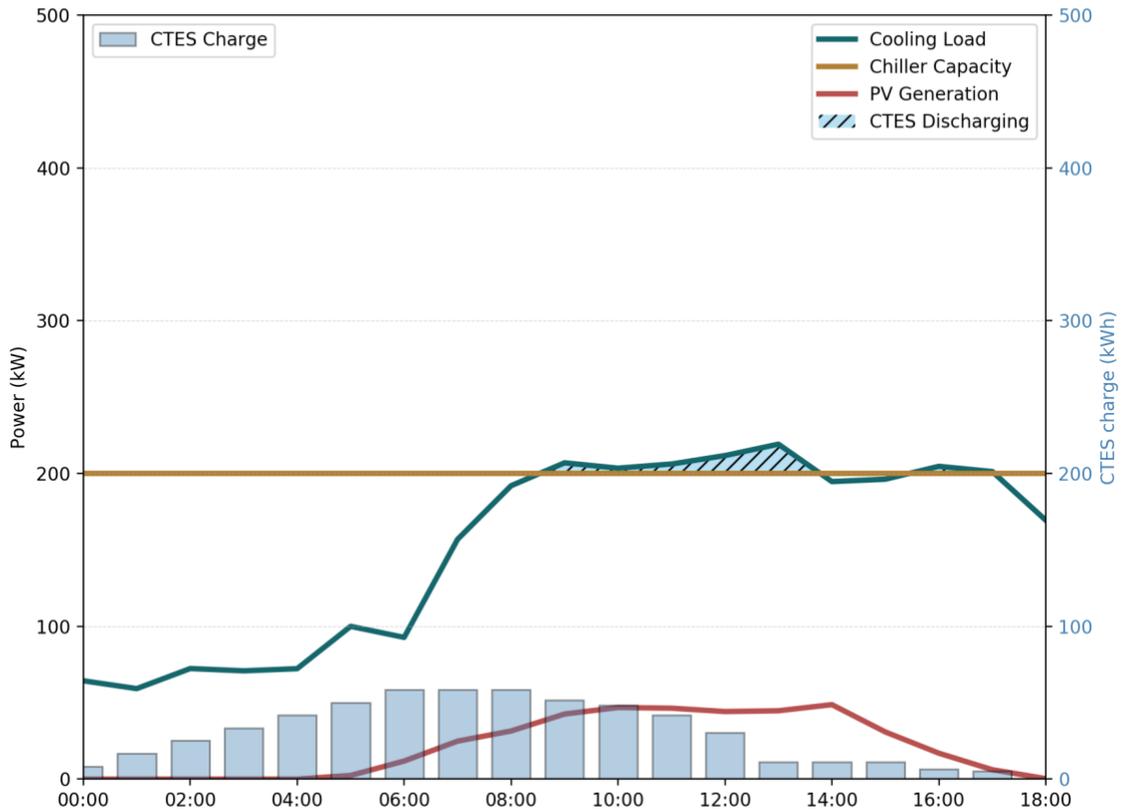


Figure 6.14 CTES charge and discharge rate using the forecasting system under 200 kW chiller.

6.3.2 Systems tested under different CTES capacity values

In this test case, the chiller capacity has been fixed at 180 kW, discussed earlier. The CTES capacity has been increased from 300 kWh to 500 kWh for both cases here, the baseline method and the forecasting method. The 180 kW chiller capacity was chosen as it has the highest need for high CTES capacity, as it cannot meet all the cooling load by itself and it needs the CTES charge to meet the cooling load.

Figure 6.15 shows the system when tested under the baseline method. Similar to the 180 kW case discussed earlier, the CTES started discharging at 08:00 a.m. and

stopped discharging at 05:00 p.m., the discharge value from the CTES is the same as the 180 kW chiller case. However, as the CTES capacity is higher in this case, and as the baseline method charge the CTES fully during the night regardless of the total cooling demand required for the next day, the remaining charge at 05:00 p.m. in the CTES in this case is higher than the previous case. In this scenario, the remaining charge is 264 kWh, while in the previous case when the CTES capacity was 300 kWh, the remaining charge was only 64 kWh.

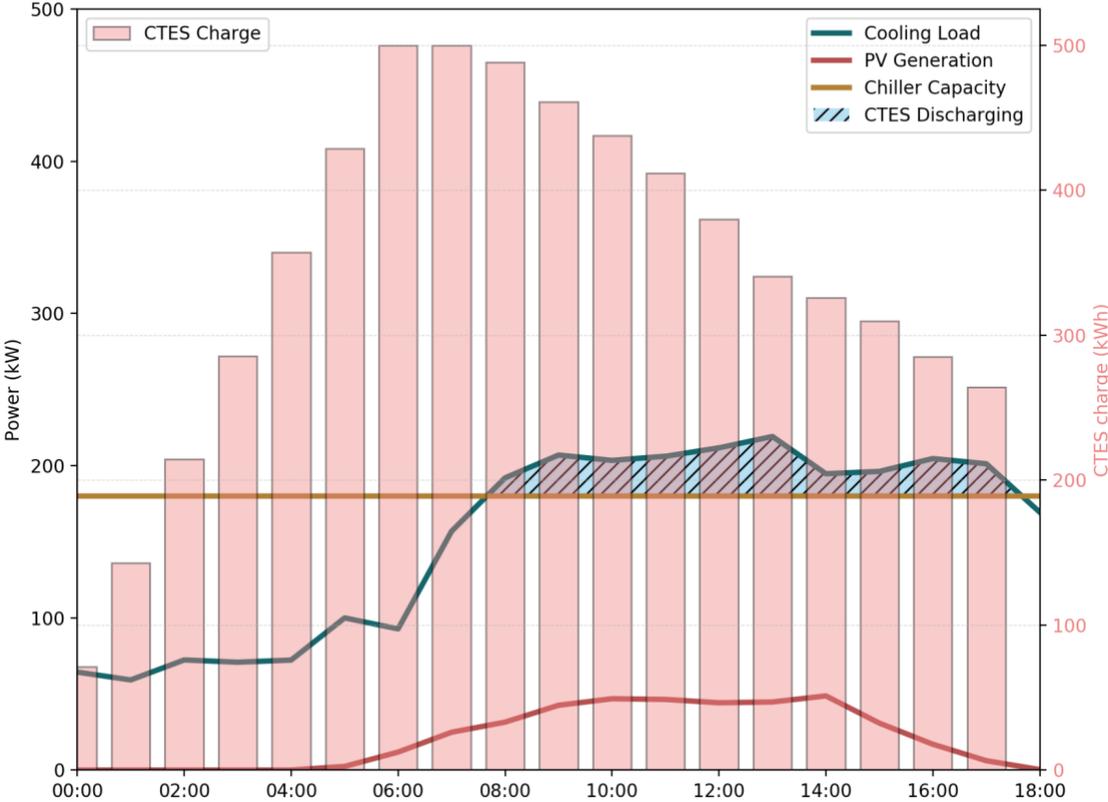


Figure 6.15 CTES charge and discharge rate using the baseline method under 180 kW chiller and 500 kWh CTES capacity.

Figure 6.16 shows system tested under the 500 kWh CTES capacity using the forecasting method. The required CTES charge during the day in order to meet the cooling load is the same as the baseline method. However, the main difference is the percentage of CTES that was charged during the night. In this case the forecasted cooling load plus the 10% error factor was charged during the night. At 05:00 p.m. the remaining charge is 23 kWh in the CTES, same as the case when the CTES capacity was 300 kWh and tested under the forecasting method. Meaning that the forecasting method is independent of the CTES capacity and is only charged based on the required load for the next day. However, the difference in the charge in the 300 kWh and 500 kWh chiller capacity between the baseline and the forecasting method has increased. In the 300 kWh case the difference was only 41 kWh, while in the 500 kWh case, the difference increased to 241 kWh. As can be seen in this case, the forecasting method is more desirable when the CTES capacity increases. Because the remaining charge in the CTES when using the baseline method increased with the CTES capacity.

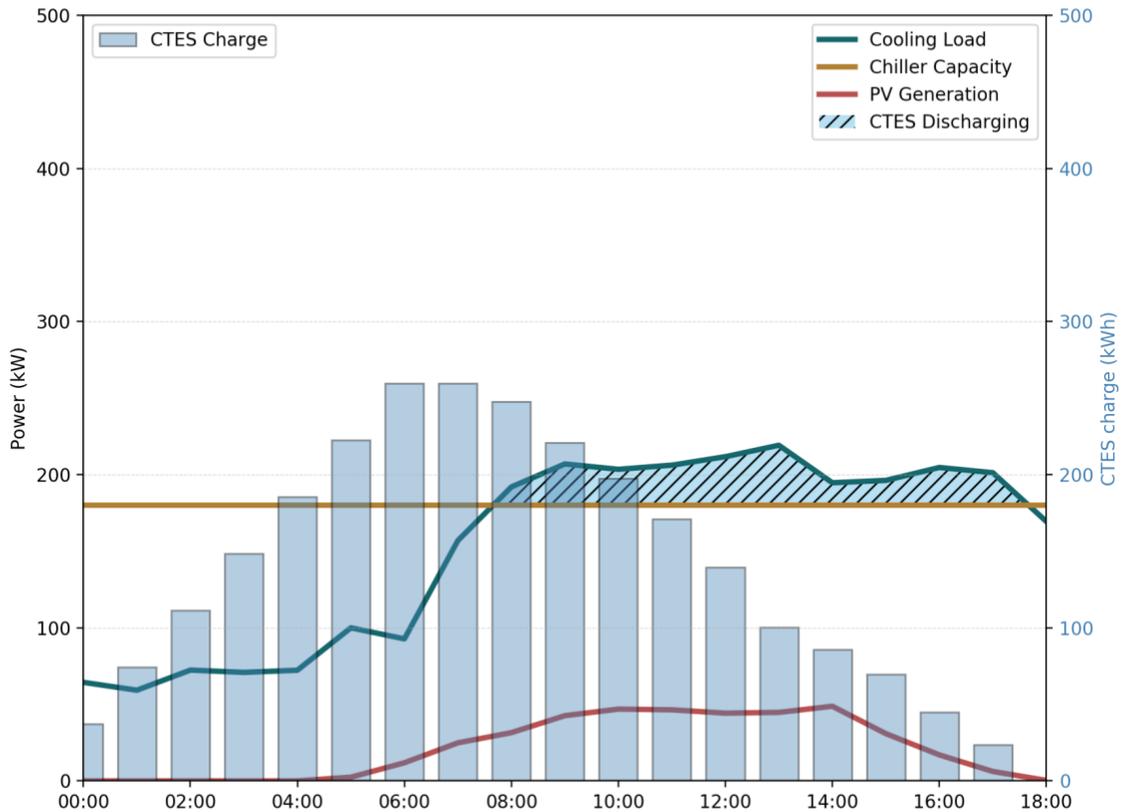


Figure 6.16 CTES charge and discharge rate using the forecasting method under 180 kW chiller and 500 kWh CTES capacity.

Table 6-5 shows the difference in the remaining charge between the baseline method and the forecasting method when tested under different scenarios. The scenarios include different CTES capacities and different chiller capacities. As can be seen from the table, the difference in the remaining charge increased as both the chiller and the CTES capacities both increased. That's mainly because the remaining charge in the baseline has increased, because the CTES capacity has increased, and also because the chiller capacity has increased, so the required CTES charge during the daytime has in turn decreased. On the other side, as the chiller capacity and the CTES capacity both decreased, the difference in the CTES also decreased, because most of the required

CTES charge is used during the peak hours in the baseline method, hence, the difference in the remaining charge also decreased.

Table 6-5 The difference in the remaining charge at 5:00 between the baseline method and the forecasting method, tested under different scenarios, results are in kWh.

		CTES Capacity (kWh)		
		300	400	500
Chiller Capacity (kW)	180	41	141	241
	190	151	251	351
	200	241	341	441

As can be seen from the table, the need for the forecasting system increased as the CTES and the chiller sizes both increased compared to the cooling load. While as the capacities of the CTES and the chiller decreased, the difference in the remaining charge also decreased.

6.3.3 Conclusion

In this section, the proposed overall forecasting model combined with the CTES at a district level was tested under different scenarios. These scenarios include different chiller and CTES capacities. The proposed forecasting model was tested against the baseline model where there is no forecasting and estimation for the next day charge. Overall, the proposed forecasting model outperformed the baseline model in terms of the achieved saving in the remaining charge as can be seen in **Table 6-5**.

Chapter 7 Conclusion and Future Work

7.1 Conclusion

In hot countries cooling systems consume a large portion of buildings' overall load. Moreover, these cooling systems are only fully utilized during the peak demand hours in a few very hot summer days. These large cooling systems increase the capital investment needed at the installation phase. CTES is a good option to lower these initial costs associated with the installation of large cooling systems, as the required cooling systems in this case has a lower peak capacity, hence, a lower price. A shared cooling system and CTES at a district level would allow for a better utilization of these resources. The integration of the shared cooling system with CTES at a district level improve the utilization of the cooling system, by lowering the peak of the cooling demand, hence, the cooling system is better utilized during the year.

In this dissertation a solution was presented to avoid creating a building peak demand, using Cool Thermal Energy Storage (CTES) deployed at a district level combined with PV and building load forecasting. It also answered one important question - how much of the CTES should be charged during the night, such that the cooling load for the next day is fully met and at the same time the CTES charge is fully utilized during the day.

The solution presented in this dissertation integrated the CTES with PV power forecasting and building load forecasting at district level for its better charge/discharge management. A district comprises several buildings of different load profiles, namely, mosque, clinic and the office building. All of these buildings are connected to the same cooling system and a shared CTES. The use of the forecasting for both the PV and the building cooling load allows the building operator to more accurately determine how much of the CTES should be charged during the night, in order to meet the cooling peak

demand of the next day. Using this approach, the charge of the CTES is utilized more efficiently during the day, also saving is achieved in the capital costs during the initial installation of the cooling capacity, as well as savings for the utility company by lowering their peak load.

The district presented in this dissertation has PV panel system and three types of buildings, mosque, clinic and office building. In order to have a good estimation for the required CTES charge for the next day, good forecasts for the PV panel system and the building load would be required. In this presented work, the dust was introduced as a new input feature in all of the forecasting models to improve the models' accuracy. Dust is an important input feature for the forecasts in areas with high dust values. All the forecasts were tested under four machine learning forecasting methods, namely Decision Trees, k-Nearest Neighbor, Neural Networks and Support Vector Regression. Each forecasting method was tested under 31 feature combinations to investigate which set of features are best for each forecasting variable (i.e., PV panel system, mosque, clinic and the office building). A total of 124 test cases were conducted for each forecasted variable. Individual features as well as different feature combinations were tested. A nRMSE of 3.73%, 11.39%, 4.56% and 3.53% was achieved for the PV panel system, mosque, clinic and the office building.

The overall solution used both the PV panel forecasts and the three buildings cooling load forecasts. These forecasts were aggregated to estimate the required CTES charge for the next day. The presented method was tested against the baseline method, where no forecasting system was present at the district level. Multiple scenarios were conducted with different cooling system sizes and different CTES capacities. The presented method utilized the CTES charge during the day more efficiently than the baseline method. This led to more energy savings at the district level, as well as more savings in the capital costs needed during the installation phase of the cooling system.

7.2 Future work

The possible future extensions of this work can build on generalization of the implemented work. This can be divided into two cases, the first one would include the addition of different building types, such as residential or industrial buildings. Going along this direction will require model training again, as these new buildings have different load profiles. And, in order to perform forecasting on these buildings, a new training for the models will be required. The second case can involve the generalization of the model with the same buildings used in this work. Using this approach will require scaling of the cooling load of each building type proportionally. As the addition of more buildings will scale up the cooling load for each building type, but will preserve the characteristics of the load profile. Also, another direction may involve trying different combinations of these buildings, the goal here is to see which sets of these buildings are better integrated into the same cooling system and the same CTES, such that, the cooling system is better utilized and more savings would be achieved.

Another future direction may include the savings achieved when the price of the electricity varies. This is generally known as Time of Use (TOU) prices, where electricity prices are high during the peak hours, and low during the off-peak hours. Using this scenario, the building operator can charge the CTES during the off-peak hours (usually at night) and discharge this CTES during the peak hours when the electricity prices are high.

One more direction may be to use a closed loop forecasting system, then update the forecasting results every hour. So, instead of generating the forecasts only once during the midnight, the forecasts will be generated at the midnight, and then will be updated every hour. Now, if the forecasting results change, a decision to increase or decrease the cool charge will be taken.

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