

A SIMULATION MODEL FOR CONTINUOUS MINING SYSTEMS

by

Devanathan Ramachandran

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APPROVED:

E. Topuz, Chairman

C. Havcocks

L.J. Prelaz

J.R. Lucas, Head

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Blacksburg, Virginia

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Chapter 1

INTRODUCTION

Until recently most of the operational decisions made by the mining industry were based upon previous experience, analysis, and intuition. These decisions were highly subjective depending on the quality and experience of managerial personnel. As mining operations grew larger and more complex in nature, a large number of variables and the interaction among these variables became an important factor in the decision making process. In addition to the size and complexity of the operations, such external factors as Federal Safety and Health Regulations, deterioration of labor-management relations, inflation and competition required management to control costs more effectively and to minimize risks involved in decision making. It became apparent that less subjective methodologies were needed to address the problems of planning mine layouts, selecting equipment, scheduling operations, and comparing alternatives.

Because of the large number of variables involved in mining and the variability and interaction among them,

many analytical modeling techniques have not been developed or adopted in the mining industry. However, computer simulation has been one of the most widely used techniques of operations research in mining because of the ability of computers to store, retrieve and manipulate much data in the modeling mining systems. Computer simulation models are used by mine management to aid in solving design, engineering, managerial and operational problems. Significant progress has been made in the design and the selection of equipment for new mining operations, in the analysis of existing operations for possible improvements, in the design of material handling systems, and in calculations of the ore reserves.

Most of the computer simulation models in use require computers possessing generous memories and rapid execution. Along with a user experienced in computers and simulation models, the models have required extensive data preparation and long execution time resulting in significant cost implementing these models. Consequently, they have limited the use of computer simulation models in the mining industry. With the availability of the improved micro- and mini-computers, these difficulties have been largely overcome and have become more valuable to mine management for decision making.

With the computer program entitled FACESIM, the computer simulation model of face operations in room-and-pillar mining used widely in the mining industry, it was decided to adapt this versatile and useful program in the following manner:

1. Modification of FACESIM to simulate continuous mining systems on microcomputers equipped with a minimum of 64K random access memory and a FORTRAN compiler;
2. Reduction in the data to be prepared for input into FACESIM to assist the user, who may not possess experience in simulation and data preparation;
3. Modification of the program to be able to simulate equipment breakdowns without greatly adding to the complexity of the program.

The objective of the careful adaptation of the computer program FACESIM hopefully would result in a computer program capable of being able to achieve the design and selection of equipment for continuous mining operations, the design of mining layouts, and the analysis of existing operations.

To assist the mining engineer in the design process, the adopted simulation model may provide output data on coal production with the analysis of the time required for the equipment to perform the various activities.

Chapter II

COMPUTER SIMULATION

2.1 GENERAL

As the industry has grown in size and complexity, the methodology to solve the problems faced in mine planning, scheduling and operations has to include more and more details of the system to obtain realistic results. When using analytical methods to solve the problems, it is difficult, if not impossible, to include a large amount of details. These difficulties in using analytical methods to get reasonably accurate results have made computer simulation the most widely used management science and operations research technique.

Computer simulations have been used in analyzing various systems. They are used to better understand the existing system, to evaluate changes proposed in the existing system, to evaluate the proposed alternatives or to forecast and aid in planning.

The wide use of computer simulation is due to many technical attractions that it can offer compared to other management techniques available. Some of these advantages are (Fishman, 1978, and Law and Kelton, 1982) as follows:

1. Several years of activities can be simulated in minutes without disturbing the real system.
2. The detailed structure of changes in real system over small intervals of simulated time, which can not be observed in real time, can be studied.
3. Sources of variation can be identified and studied. This is important when statistical analysis of the relations between the input and output variables is to be performed.
4. Measurement errors do not occur.
5. Simulation experiment can be stopped to review the results to date and then the experiment can be resumed without the loss of continuity.
6. The state of simulation can be restored.
7. Replication of an experiment is possible.
8. Greater amounts of detail of the system can be included in the model.

In general, the greater the amount of details to be included in the model, the more realistic the model is. Consequently, the results from the simulation model conform to

reality more closely. However, judicious restraint on the part of the modeler in regard to details is often the better policy for the following reasons:

1. To include details, time and effort need to be devoted to preliminary observations of individual characteristics of the system. This introduces a cost that must be justified with respect to the objective.
2. Added details require added programming, especially for the contingencies that the details specify; it also makes it difficult to locate sources of error because of many potential trouble spots.
3. Added details in the model increase computer time and memory requirements and, therefore, the cost. Testing for special situations, along with the need to update and manipulate system attributes, contributes to this cost.

The following are the disadvantages associated with simulation studies that one should keep in mind when developing a simulation model:

1. Greater confidence is placed on simulation results

than is justified because of large volume of numbers produced. However, if the model is not a 'valid' representation of the system, the results will be of no use.

2. The simulation model is often used to predict beyond the range of its applicability without proper qualification.
3. Though simulation models are expensive and time-consuming to develop, there is no guarantee that the time, effort and money spent will return useful results with satisfactory-benefits.
4. Since a stochastic simulation model produces estimates of the model's true characteristics, several independent runs of the model will be required for each set of input parameters. For this reason, simulation models are not as good as analytical models for optimization.
5. There is sometimes the tendency of the investigator to defend his particular depiction of the problem as the best representation of reality.

2.2 SIMULATION PROCESS

A model may be defined as a description of a system. A system is a group of interdependent objects which perform a specified function (Shannon, 1975). To build a model of a system, an objective must be developed and the essential features of the system must be abstracted by defining significant elements and the relationships among them. The computer simulation model should also include the desired performance measures and design alternatives to be evaluated. Model-building is an interactive process requiring redefinitions and redesigns. Typically, the development of simulation model begins with a simple model which is embellished in an evolutionary fashion to meet the problem-solving requirements. The model-building approach to problem solving is illustrated in Figure 1.

Simulation model building is a part of simulation process in which Shannon (1975) identified several stages. The following stages are slightly modified from the one presented by Shannon.

1. Problem formulation: Definition of the boundaries of the systems, restrictions and measures of performance including the statement of objective.
2. Model formulation: The abstraction of the real system

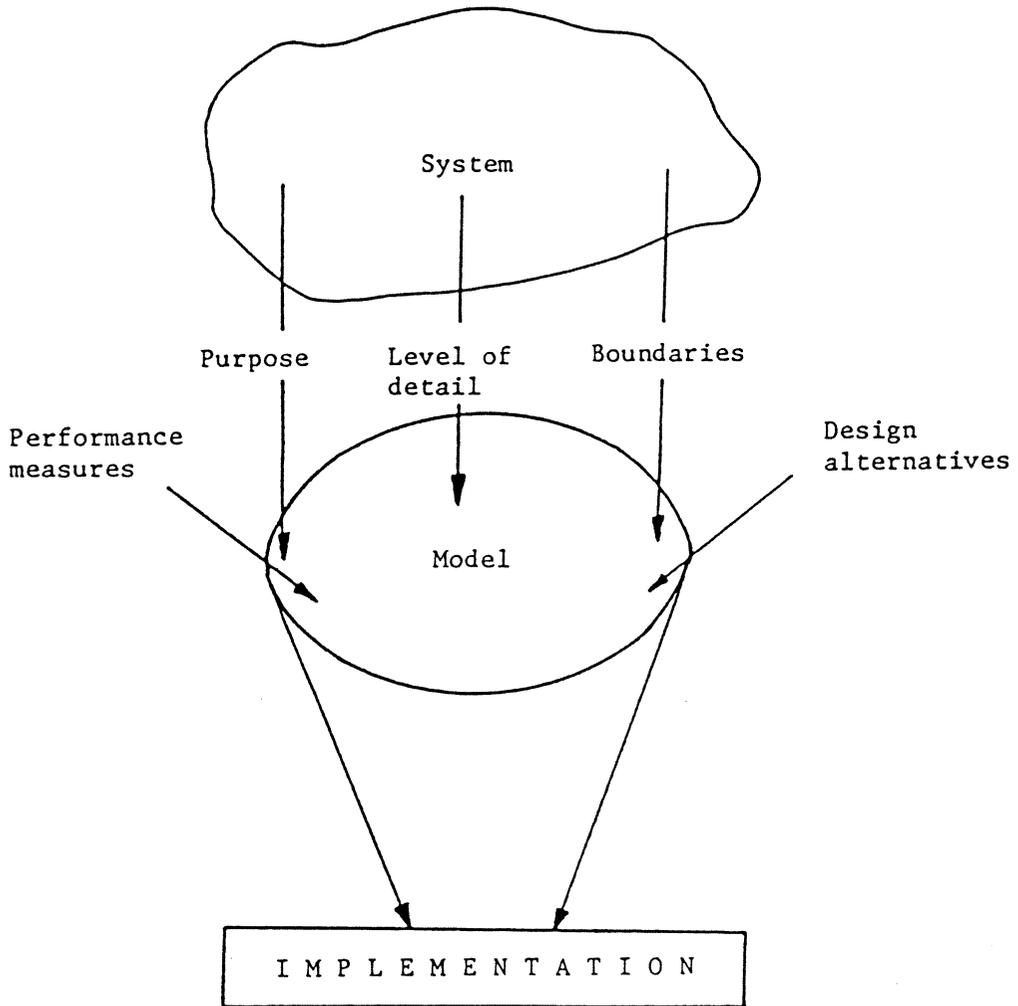


Figure 1
A Model-building Approach for Problem Solving
(Pritsker and Pegden, 1979)

into mathematical and logical relationships in accordance with the objective. The crucial decisions are what simplifying assumptions are valid, what elements to be included and what interactions occur among the elements. The amount of details to be included should be based on the purpose of the model.

3. Data preparation: The identification, specification and collection of data.
4. Model translation: Coding the simulation model in a computer language.
5. Verification and validation: Verification is the process of determining that the simulation model functions as intended, that is, debugging the computer program. See Law and Kelton (1982) for different verification techniques and Fishman and Kiviat (1967) for statistical methods used in the verification process.

Validation is the process of determining that the simulation model is a reasonable representation of the real world system under study (Van Horn, 1971). See Law and Kelton (1982), Fishman (1973, 1978) and Kleijnen (1974, 1975) for details on model validation.

6. Strategic and tactical planning: This refers to

the task of establishing the experimental conditions for simulation runs. Strategic planning is developing an efficient experimental design to determine the relationship between input and output variables or to optimize the desired output variables.

Tactical planning is the determination of how each of the simulation runs is to be made to obtain the most information from the data. Two specific issues are the starting conditions and methods of reducing the variance of output variables (Pritsker and Pegden, 1979).

7. Experimentation: Experimentation is the execution of the computer program.
8. Analysis of Results: Analysis of simulation results is done to draw inferences about the system or to compare alternatives. See any of the following: Law and Kelton (1982), Fishman (1967, 1973, 1978) and Kleijnen (1974, 1975) that provide detailed procedures for statistical methods to analyze simulation results.
9. Implementation and documentation: This process puts the results from the simulation model to use and documents the model and its use. The successful implementation of the results is largely dependent on

the degree of success achieved in the previous stages of the simulation process, involvement of the user in model development and the degree of his understanding of the model and its results.

Stages in the simulation process rarely occur in the sequence mentioned above because of changes made in assumptions, reformulation of the problem, redefinitions and redesigns of the model as the model builder understands the system better and develops insight into the problem, and difficulties involved in different stages. The relationship among the stages in the simulation process and how one advances through them are shown in Figure 2.

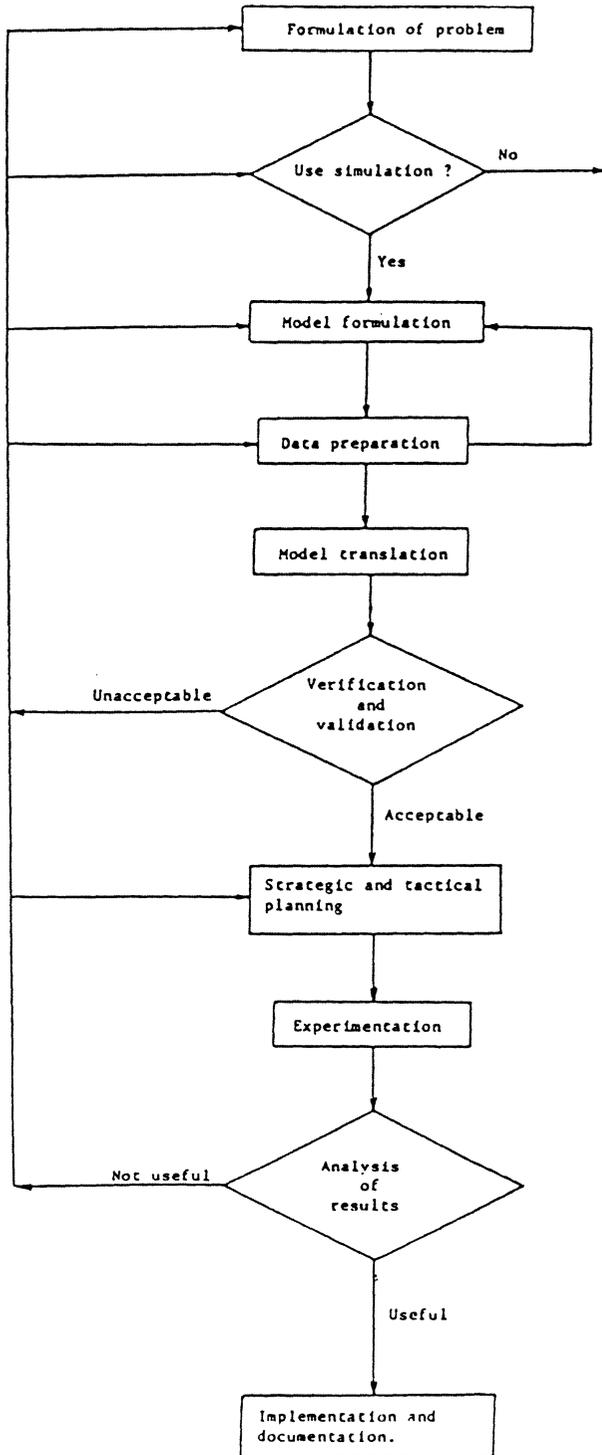


Figure 2
 Interaction Among Stages in Simulation Process
 (Shannon, 1975)

Chapter III

FACESIM

FACESIM (FACE operations SIMulator) is a computer simulation model developed at Virginia Polytechnic Institute under the sponsorship of the Office of Coal Research during the period 1962-64 primarily to simulate room-and-pillar mining systems with the maximum capability to use three shuttle cars with a loader or a continuous miner.

3.1 CONVENTIONAL MINING SYSTEMS

The conventional room-and-pillar mining of coal involves five operations at the face. They are (1) cutting, (2) drilling, (3) blasting, (4) loading and hauling and (5) roof bolting. Since loading and hauling of coal take place simultaneously in a cut, they are considered as one operation for the purpose of building a simulation model. These operations are performed by the coal-cutting machine, drilling crew, blasting crew, loader and conveying equipment (shuttle cars or conveyors) and roof bolter respectively. All these operations are carried out in the same sequence mentioned above in each cut. Of these five operations, loading-and-hauling is the primary operation and the rest are supporting operations necessary to loosen coal in the seam and to provide safe operating conditions.

The number of headings advanced in a panel must be greater than or equal to the number of operations to be performed at each cut to mine coal. Therefore, in conventional mining, the minimum number of headings is five, one operation per face. The conventional mining system may be compared to the pure flow shop in production scheduling where jobs are routed through machines to perform operations on jobs in a predetermined order. However, in conventional mining, unlike in a typical flow shop, the machines (the equipment in the mine face) move from one job (face) to another while jobs are stationary as shown in Figure 3.

In the mining context, the number of jobs waiting for machines is limited by the number of headings advanced and there may be jobs waiting in queue for the loading-and-hauling operation. This comparison of a production scheduling system and a conventional mining system is useful for developing and understanding a mine simulation model like FACESIM.

3.2 ASSUMPTIONS MADE IN FACESIM

As in any model building process, there are assumptions made in developing FACESIM. It is appropriate to mention them here to understand modifications made in FACESIM to build CONSIM. This will also help the users familiar with

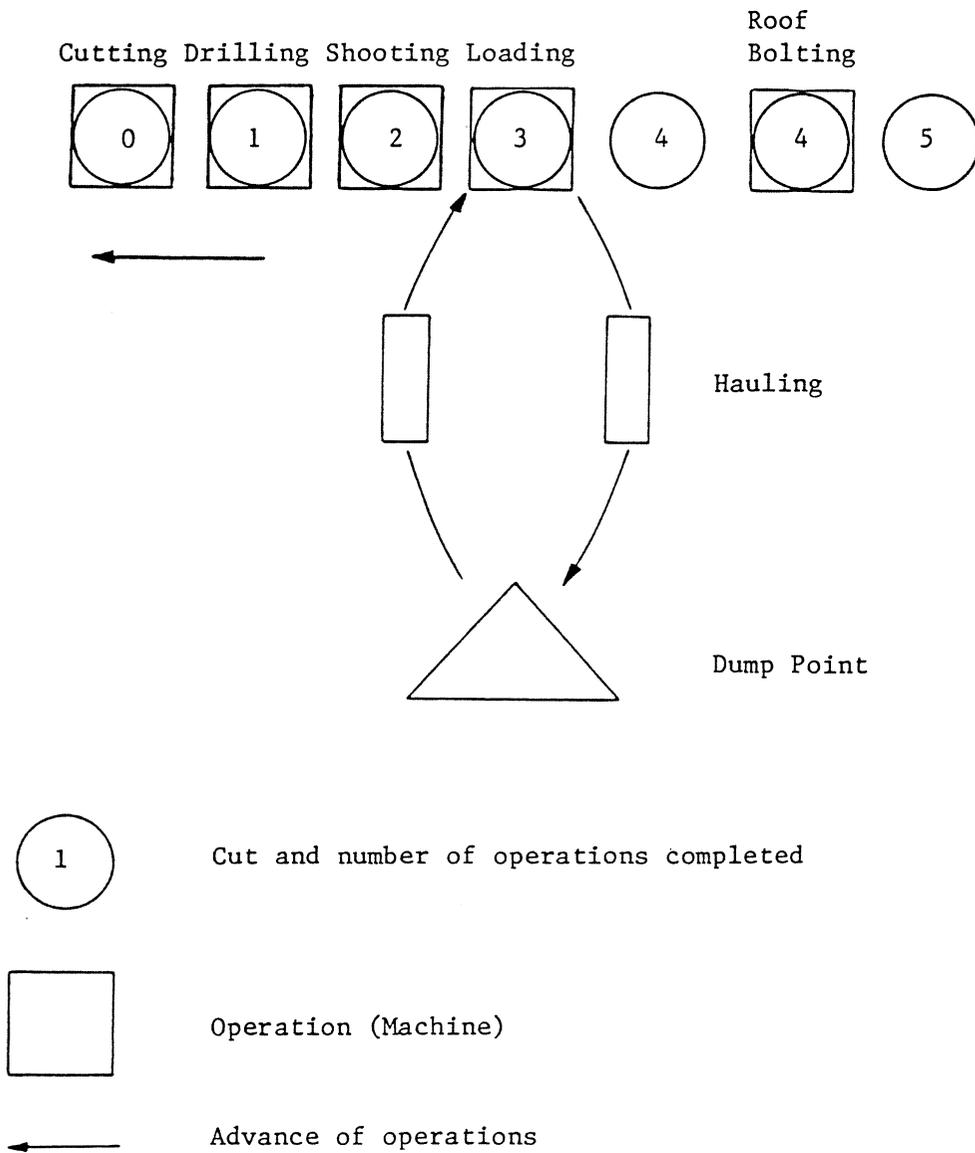


Figure 3
Schematic Diagram of a Conventional Mining Operation

FACESIM to understand and use CONSIM and vice-versa. It is not to be construed that the assumptions made in FACESIM are wrong because they are modified in CONSIM. The changes were necessitated because of the simplification that was to be achieved in CONSIM and additional details incorporated in CONSIM. To facilitate understanding of different distances and times discussed under the assumptions some of the variables are schematically shown in Figure 4.

The following are the assumptions made in FACESIM:

1. A shuttle car is available for loading immediately after tramming of the miner is completed.
2. All shuttle cars change out at the same location.
3. All shuttle cars discharge at the same location.
4. All shuttle cars have the same operational characteristics such as haul rates and payload.
5. When only one shuttle car is used in conjunction with the miner, the shuttle car is left in the cut after loading for the last time. However, when more than one shuttle car is used, the last shuttle car loaded in the cut is unloaded at the discharge point hauled to the change point of the same cut.

6. More than two shuttle cars can be discharged simultaneously in a two-way dump (Note that a maximum of three shuttle cars can be used with loader).
7. Shuttle cars may switch in and out only when the loader is in the transport heading, i.e., the heading where the dump is located.
8. The change-out time includes, in addition to the time spent by the shuttle car hauling over the change-out distance, the time required for switch-in and switch-out and the time shuttle cars have to wait for the loader to maneuver.

When only one shuttle car is used in conjunction with the loader, the change-out time also includes the discharge time and trip change time, if a push-pull system is in use.

9. All the coal in the cut will be loaded into shuttle cars even if the last load is negligibly small.

For example, if the last load is only 0.01 tons, which may be left in the cut without any problem in practice, FACESIM will load it into a shuttle car.
10. The supporting operations will be advanced forward only one cut when the loader is to be moved to the

next cut, though not necessarily at the same time on simulation clock.

11. Shuttle cars are loaded and unloaded in a predetermined order. For example, the shuttle car numbered one is loaded before car number two which is loaded before car number three.

3.3 EQUATION FOR LOADER CYCLE TIME

FACESIM is constructed with the assumption that the cycle time (i.e. the time between starting operation at one cut and the next) of the loader satisfies the following equation:

$$LCT = LT + WL + CT + TT + WP$$

where

LCT - the loader cycle time,

LT - the time the loader spends in loading coal during the cycle,

WL - the time the loader waits because no shuttle car is available at the change point during the cycle,

CT - the change-out time during the cycle, and

TT - the time spent on tramming the loader to the next cut.

WP - the time the loader waits for coal, i.e., for entry into the next cut,

The above relation also holds for shift time and the time required to mine all the cuts.

3.4 FACESIM INPUT AND OUTPUT

The input data required to run FACESIM program are essentially the empirical distributions of the loading rate of the loader, the travel rates -- loaded and empty -- of shuttle cars and the discharge rate; the tram rates, tram functions, etc. of the loader and other auxiliary equipment; dimensions of cuts and pillars; and the data required for each cut, called G-card data. The number of data cards required depends on the number of cards required to define the empirical distributions and to input G-card data. Prelaz, et al. (1964) provide details of the input data required for FACESIM. All the input data must be prepared and input manually. FACESIM simulates the operations in a conventional mining system over a specified number of cuts and it stops

when all the cuts are mined and roof bolted. The macro flowchart for FACESIM is shown in Figure 5.

To show how to use FACESIM, a seven heading system (Figure 6) with 70 X 62.5 feet center-to-center distance mined conventionally was simulated (Prelaz, et al., 1964). The input data for this system are shown in Table 1. Card type A contains the data to define the empirical distribution for loading rate, shuttle car payload, shuttle car haul rates and discharge time. Card type B contains the cycle times and tram functions for auxiliary operations and cut dimensions. The number of the first and last cut to be mined are given in card type C. Seed numbers for random number generator, shift time, density of coal, time required to start and stop work in a shift, etc. are given in card type D. Card type E provides tram rates and in-place constants for auxiliary operations and switch-in and switch-out times. The relative position of the preparation cycle and the first cut to be loaded are indicated on card type F. One card of type G is required for each cut. This card contains haul and tram distances, codes for cut dimensions and for cycle times and tram functions of auxiliary operations, loader tram constants and roof support work sequence and number of shuttle cars. In the example twenty-four cards were used to input card type A; nine cards for card type B; and twenty-nine cards for card type G. With the data shown in Table 1

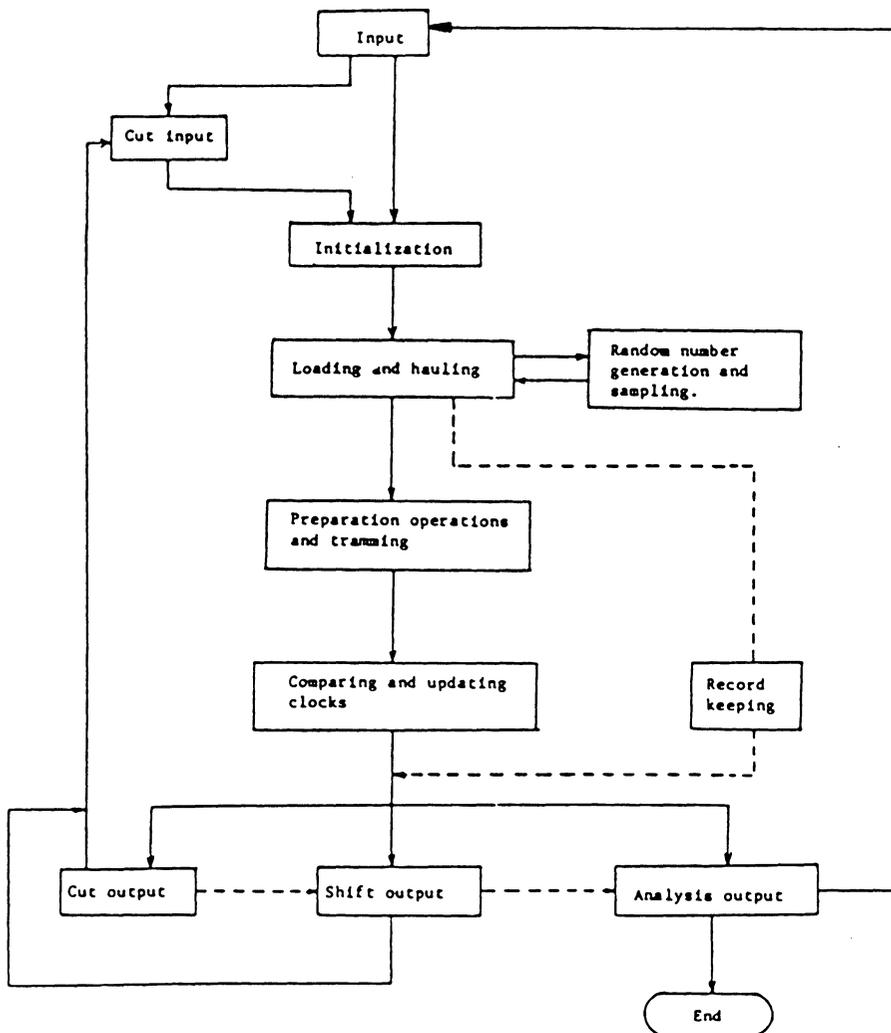


Figure 5
 Macro Flowchart for FACESIM
 (Prelaz, et al., 1964)

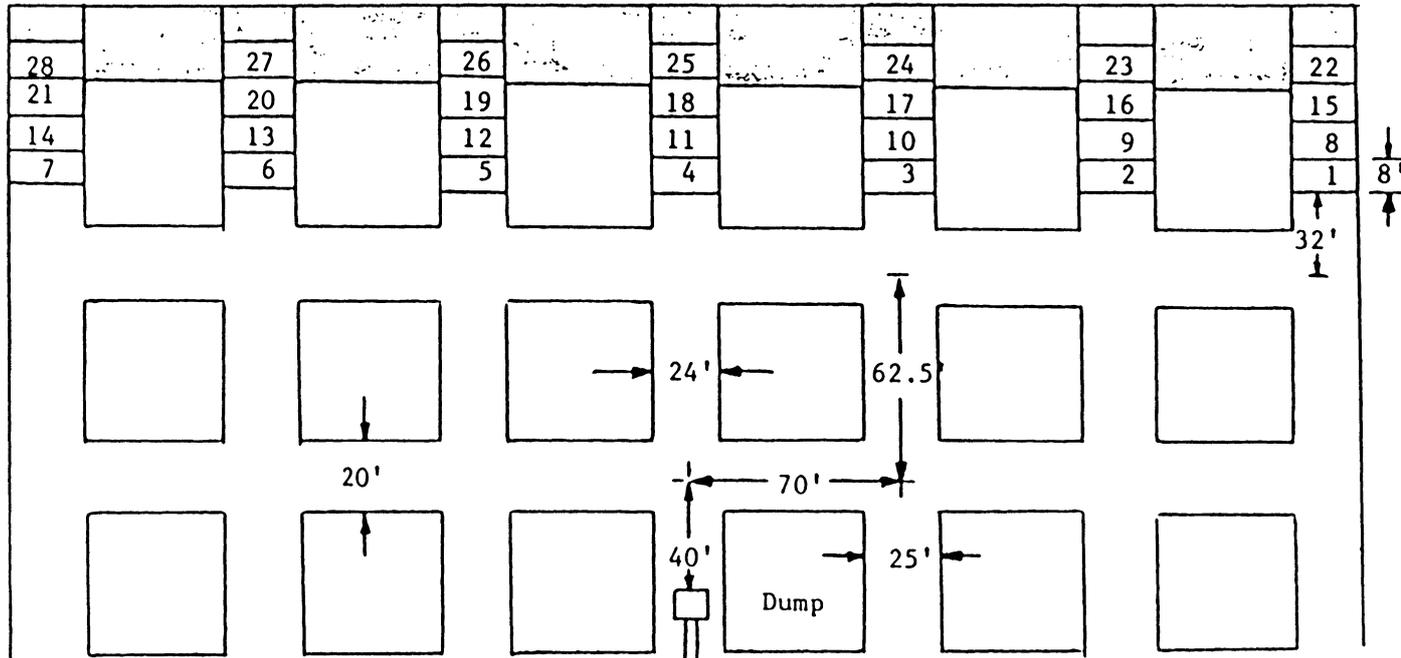


Figure 6
 Layout for FACESIM Input Data
 (Prelaz, et al., 1964)

Table 1
A Sample Input for FACESIM

Input Data														Card Type	
9	40	24	23	22	21	58	40	267	14	13	29	45	21	A	
11	41	25	24	23	25	62	173	467	27	38	71	119	62		
13	42	26	25	24	26	64	260	733	110	288	86	179	124		
15	44	27	26	25	27	66	380	933	205	425	186	299	206		
17	45	28	27	26	28	68	433	1000	315	550	271	328	247		
19		29	28	27	29	70	520		329	625	429	373	289		
21		30	29	28	30	72	553		507	675	529	463	361		
23		31	30	29	31	74	640		589	775	657	522	412		
25		32	31	30	32	76	713		658	788	743	627	495		
27		33	32	31	33	78	787		671	850	814	687	536		
29		34	33	32	34	80	827		726	863	900	716	577		
31		35	34	35	35	82	847		808	875	914	731	639		
33		36	35	36	36	86	880		822	888	943	776	691		
35		37	37	37	37	88	893		849	900	971	791	742		
37		38	38	40	38	90	913		863	925	1000	821	784		
39		39	39		39	92	927		904	938		866	825		
41		40	43		40	94	933		959	950		925	856		
43		41	47		43	96	953		973	963		940	887		
45		43	50		45	98	967		986	988		970	918		
47		48	52		47	100	973		1000	1000		1000	928		
51						104	980						938		
53						106	987						959		
57						110	993						979		
65						118	1000						1000		
1168	0000	1341	142	915	000	1482	0000	04.83	25.00	008.00					B
2000	520	1309	611	2785	200	2317	70	7.67	24.00						
1060	590	1146	000	688	180	1200	460		20.00						
1890	450	2073	469	1230		2267			40.00						
1910	660	2167	318	1317		2352			45.00						
2040		2362		1631		2528			57.50						
2740		3143		2004		3114			45.25						
2500		3108		3874		3979			58.75						
1894		2108		1364		2021			37.50						
0001002901															

Table 1 (Continued)
 A Sample Input for FACESIM

Input Data														Card Type				
87.	87.	480.	0.04315.	0015.00	7.50	7.50						.37	1			D		
	0094.	0050.	0088.	0069.	0106											E		
	00010008															F		
1	1	1	1	248.	248.	0.	12.	40.	70	32	101	101	102	102	0.2	0.0	7	7
2	1	1	1	178.	178.	0.	12.	40.	70	32	101	101	102	102	0.2	0.0	1	8
3	1	1	1	108.	108.	0.	12.	40.	70	32	102	102	102	102	0.2	0.0	2	9
4	2	2	1	0.	0.	0.	50.	40.	70	32	203	203	201	201	0.2	0.0	3	10
5	1	1	1	108.	108.	0.	12.	40.	70	32	101	103	101	101	0.2	0.0	4	11
6	1	1	1	178.	178.	0.	12.	40.	70	32	101	104	101	101	0.2	0.0	5	12
7	1	1	1	248.	248.	0.	12.	40.	420	32	104	105	103	103	1.9	0.0	6	13
8	1	1	1	248.	248.	0.	20.	40.	70	40	101	101	102	102	0.2	0.0	7	14
9	1	1	1	178.	178.	0.	20.	40.	70	40	101	101	102	102	0.2	0.0	8	15
10	1	1	1	108.	108.	0.	20.	40.	70	40	102	102	102	102	0.2	0.0	9	16
11	2	2	1	0.	0.	0.	58.	40.	70	40	203	203	201	201	0.2	0.0	10	17
12	1	1	1	108.	108.	0.	20.	40.	70	40	101	103	101	101	0.2	0.0	11	18
13	1	1	1	178.	178.	0.	20.	40.	70	40	101	104	101	101	0.2	0.0	12	19
14	1	1	1	248.	248.	0.	20.	40.	420	40	104	105	103	103	1.9	0.0	13	20
15	1	1	1	248.	248.	0.	28.	40.	70	48	101	101	102	102	0.2	0.0	14	21
16	1	1	1	178.	178.	0.	28.	40.	70	48	101	101	102	102	0.2	0.0	15	22
17	1	1	1	108.	108.	0.	28.	40.	70	48	102	102	102	102	0.2	0.0	16	23
18	2	2	1	0.	0.	0.	66.	40.	70	48	203	203	201	201	0.2	0.0	17	24
19	1	1	1	108.	108.	0.	28.	40.	70	48	101	103	101	101	0.2	0.0	18	25
20	1	1	1	178.	178.	0.	28.	40.	70	48	101	104	101	101	0.2	0.0	19	26
21	1	1	1	248.	248.	0.	28.	40.	420	48	104	105	103	103	1.9	0.0	20	27
22	1	1	1	248.	248.	0.	36.	40.	70	56	101	101	102	102	0.2	0.0	21	28
23	1	1	1	178.	178.	0.	36.	40.	70	56	101	101	102	102	0.2	0.0	22	29
24	1	1	1	108.	108.	0.	36.	40.	70	56	102	102	102	102	0.2	0.0	23	30
25	2	2	1	0.	0.	0.	74.	40.	70	56	203	203	201	201	0.2	0.0	24	31
26	1	1	1	108.	108.	0.	36.	36.	70	56	101	101	101	101	0.2	0.0	25	32
27	1	1	1	178.	178.	0.	36.	36.	70	56	101	104	101	101	0.2	0.0	26	33
28	1	1	1	248.	248.	0.	36.	36.	420	56	104	105	103	103	1.9	0.0	27	34
-1									70	64	101	101	102	102				

FACESIM was run and the output, shown in Table 2, was obtained. From Table 2, it may be read that in the first shift 995.5 tons of coal was loaded in 222.2 minutes by the loader and the loader spent 96.7 minutes on waiting for shuttle cars, 8.1 minutes waiting for entry into next cut, 52.6 minutes for tramming and 56.3 minutes on change-out. The shuttle cars travelled 20.5 miles.

Table 2
A Sample Output from FACESIM

SHIFT NO.	1	SHIFT TONS	995.5	TIME	435.89
TONS PER FACE MINUTE			2.28		
TOTAL LOADING TIME		222.21	PERCENT FACE TIME		50.97
TOTAL TRAM TIME		52.57	PERCENT FACE TIME		12.06
TOTAL WAIT TIME-NO SC		96.71	PERCENT FACE TIME		22.18
TOTAL WAIT TIME-COAL		8.10	PERCENT FACE TIME		1.85
TOTAL CH.OUT TIME		56.29	PERCENT FACE TIME		12.91
TOTAL TRIP CHANGE TIME			.00		
TOTAL WAIT-OPERATION 2			35.11		
TOTAL WAIT-OPERATION 3			17.90		
TOTAL WAIT-OPERATION 4			72.50		
TOTAL WAIT-OPERATION 5			10.70		
TOTAL HAUL DIST.	FEET =		94664.	MILES =	17.92
TOTAL CH.OUT DIST.			13522.		2.56

Chapter IV
MODEL FORMULATION

4.1 CONTINUOUS MINING SYSTEMS

Since the continuous miners were first introduced to the coal mining industry in 1948, the trend has been toward their greater use because of high productivity that can be achieved and less auxiliary equipment and manpower requirements. Though the continuous miner was initially introduced for use in coal mines, it also finds application in various sedimentary type of ore deposits such as potash and soda ash mines.

The continuous miner eliminates the need for cutting, drilling and blasting. It mechanically breaks and loads coal. The coal may be directly loaded on to shuttle cars or a conveyor system or dumped behind and subsequently loaded by a loader. The coal loaded on the shuttle cars or conveyors is discharged into the dump, located at or more than a center-line distance between pillars. The depth of cut is limited by the length of the continuous miner so as to keep the operator under a supported roof at all times. The depth of cut by continuous miners with a roof bolter mounted on them is limited only by the ventilation requirements. The number of headings driven by a continuous miner in a section may be three or more.

There are four types of continuous miners in use -- the ripper-type, the boring-type, the milling or drum-type and the auger-type. Of these, the milling-type machines are most widely used.

As with conventional mining operations, the operations in continuous mining systems can be compared to pure flow shop. Unlike conventional mining, there are only two operations -- (1) cutting and loading (by miner) and hauling (by shuttle car) and (2) roof-bolting (by bolter). Since cutting and loading and hauling are carried out simultaneously in a cut, they are grouped as one operation. This is schematically illustrated in Figure 7. The difference between the continuous mining system and the conventional mining system is the number of operations to be performed in each face.

4.2 OBJECTIVES OF THE RESEARCH

The following three objectives were to be achieved in development of CONSIM, the CONtinuous mining SIMulator:

1. Modification of FACESIM for the simulation of a continuous miner operation and simplification of the program for use on microcomputers and ease of understanding by the user.
2. To augment the capability of the simulation model to

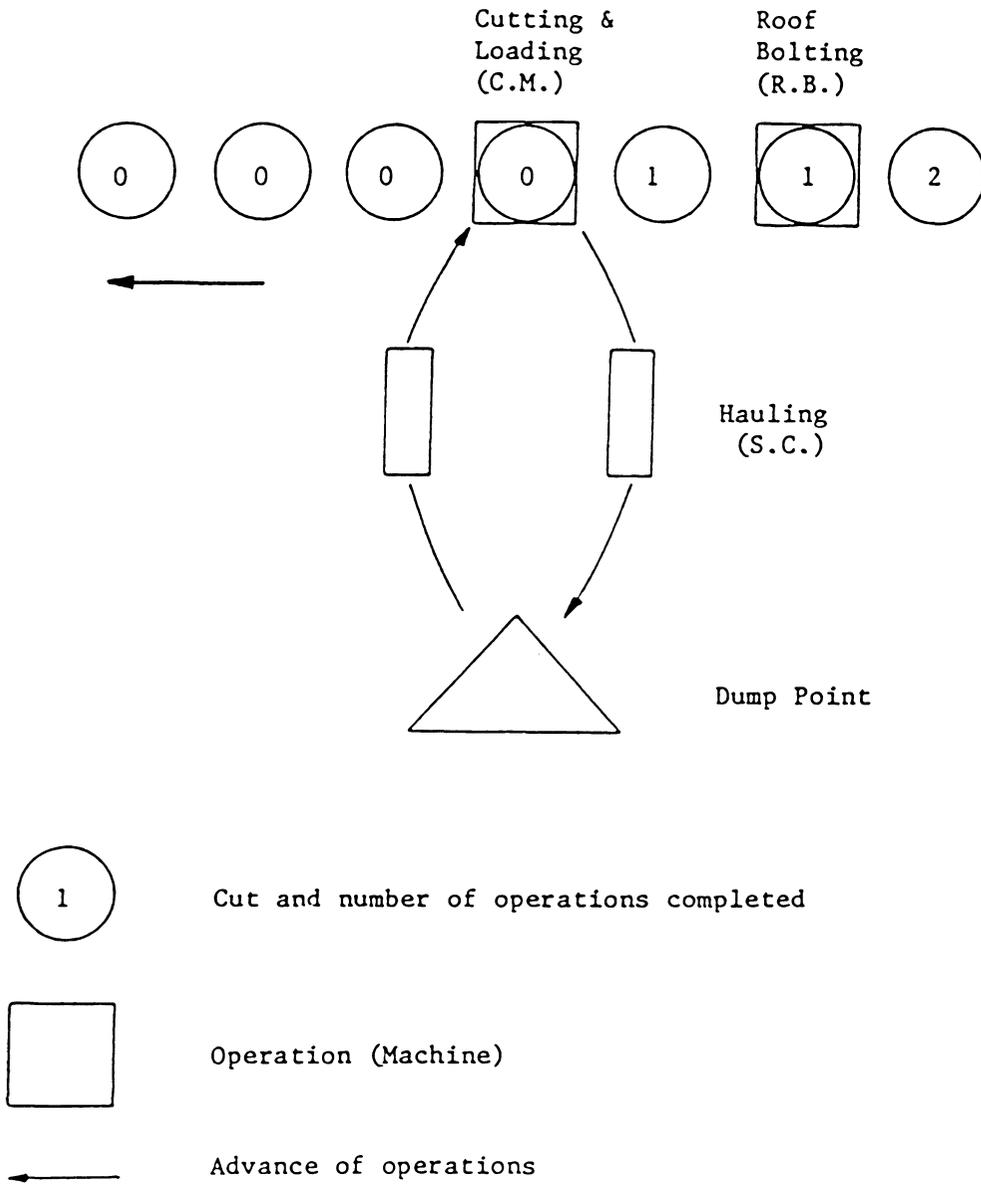


Figure 7
Schematic Diagram of a Continuous Mining Operation

simulate equipment breakdowns without greatly adding to its complexity.

3. To minimize the input data requirements by internally generating them with the minimum data that the user has to input.

4.3 MODEL DEVELOPMENT

Initially, modification of FACESIM for a continuous mining system essentially involved removal of the unnecessary parts from the FACESIM program. Further work required to achieve the first two objectives were carried out simultaneously since they were interrelated, often the work involving the second objective necessitating more work to satisfy the first objective. The third objective to minimize the input data requirements was achieved by adding subroutines to generate data internally with the minimum data to be input by the user.

4.3.1 Assumptions made in CONSIM

Simplification of the program required changes in some of the assumptions made in FACESIM. Additional assumptions were made to include more details in the model. The assumptions made in FACESIM, therefore, also hold true in CONSIM with the exception of the following:

1. The change-out time is the time spent by shuttle cars hauling over the change-out distance and that required for switch-out. This time is considered zero if it occurs while the miner is under breakdown. The change-out also includes the time spent hauling the last shuttle car over the change-out distance.
2. The shuttle car may switch in and out when the continuous miner is in any heading.
3. The last shuttle car loaded in a cut is unloaded at the discharge point and hauled back to the change point of the cut, irrespective of the number of shuttle cars assigned to the loader.
4. A maximum of two shuttle cars can unload simultaneously in a two-way dump. The alternate shuttle cars unload from the same location at the dump. Only one shuttle car can unload at a time in a one-way dump.
5. Any maneuver of a continuous miner in the cut is considered part of production work.
6. The breakdown time of any equipment is the production time lost due to breakdown, i.e., the total shift time the equipment is under breakdown minus the time required to start work at the beginning of the shift

and the time required to stop work at the end of the shift, if the time of breakdown overlaps these times.

Time between breakdowns of equipment is the production time between consecutive breakdowns of the equipment, excluding the breakdown time.

Production time in a shift refers to the duration of the shift from the time when work is started at the beginning of the shift to the time when work is stopped at the end of the shift.

7. The time between breakdowns and breakdown time are exponentially distributed.

This assumption is made because exponential distribution has been widely used to fit these variables and its parameter can be easily estimated by anyone without much knowledge in statistics.

If the exponential distribution does not fit the data satisfactorily, some other distribution can be used without much difficulty by merely changing the function subprogram with an appropriate one.

8. The shuttle cars may have different failure characteristics, i.e., different mean times between

breakdowns and different mean breakdown times.

9. Breakdown of a continuous miner may occur only after the loading of a shuttle car is completed.
10. Breakdown of a shuttle car may occur only at the change point after switching in when it is empty.
11. Breakdown of a roof bolter may occur only after moving into the cut to be roof-bolted.
12. At the start of simulation all the equipment at the face is in working condition and the shuttle car numbered one is ready to be loaded. The continuous miner is initially in cut number one which may be the first or last heading.
13. The shuttle cars are loaded in a predetermined order as in FACESIM. If the shuttle car to be loaded is under breakdown, the next shuttle car in working condition is loaded.

When all the shuttle cars are under breakdown, the one which will be repaired the earliest is the shuttle car to be loaded next. If this happens after loading the last load in a cut and if the time on the the shuttle car is greater than the time on the miner clock after it is moved to the next cut, then the

difference is accumulated as miner waiting time for the shuttle car during the next cut.

14. The loading rate, shuttle car payload, shuttle car haul rates and discharge time are continuous random variables. Their cumulative distribution functions are defined empirically, i.e., by observed data in the field.

4.3.2 Changes Made in FACESIM

With these modifications in assumptions made of FACESIM, the resulting computer simulation model, CONSIM is simpler, more efficient and easier to understand. CONSIM can also simulate breakdowns of a continuous miner, shuttle cars and roof bolter. Unlike in FACESIM, during the time that the miner mines one cut, the roof bolter may roof-bolt more than one cut and vice-versa. This change was incorporated in CONSIM since it has the capability to simulate equipment breakdowns. It is realistic to expect the equipment in working condition to continue to operate, if they can, while some equipment is under breakdown. For example, the following situations can be simulated in CONSIM:

1. Suppose the roof bolter is under breakdown. If there are cuts available for mining and if the continuous

miner is in working condition, the miner will mine all the cuts that are available and vice versa.

2. Suppose three shuttle cars are used in conjunction with the miner and two of them are under breakdown sometime during operation. The roof bolter will roof-bolt available cuts and the miner will continue mining by using the available shuttle car.

The push-pull system for transportation of coal from panels, which is not popular anymore, is omitted in CONSIM. The CONSIM can make multiple runs and produce statistics (mean and standard deviation) for performance measures of the system by shift and/or by the time required for mining all the specified cuts. The CONSIM program can be run interactively or in batch mode. Running the program in batch mode is faster, but running it interactively makes it easier to input data and gives insight into what is going on in the program.

4.3.3 Equation for Continuous Miner Cycle Time

In CONSIM, the cycle time (i.e. the time between starting operation at one cut and the next) of the continuous miner satisfies the following equation:

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4.3.4 Subroutine GCARD

When using FACESIM, it is time consuming to prepare input data, called G-card data for each cut. This requires a lot of effort and time on the part of user. This problem is solved for the CONSIM user by adding the subroutine GCARD which generates these data internally. The input data required by subroutine GCARD are the dimensions of the workings and the equipment. Subroutine GCARD has the following features incorporated in it:

1. Any number of headings may be driven.
2. Any of the headings can be used as the transportation heading.
3. It can generate data for single cuts in headings and single or multiple cuts in breakthroughs.
4. The breakthrough need not be at a right angle to the heading.
5. The discharge point may or may not be advanced as the development work advances.
6. A specified number of cuts may be made or a multiple of center-line distance between pillars may be advanced during the development.

If a specified number of cuts are to be made in development, the multiple of center-line distance between pillars is specified just large enough that all the cuts will be within that distance. If the development is to be advanced a specified multiple of the center-line distance, input a large number for number of cuts to be made.

4.3.5 Uniform Random Number Generator

A uniform (0,1) random number generator is required to generate random variates from any distribution. The uniform (0,1000) random number generator in FACESIM was replaced by RANDOM(L), a uniform (0,1) random number generator (Wichman and Hill, 1982). This random number generator has better statistical properties and is faster than many currently available random number generators. The sequence of random numbers generated by this are independent of the machine. The three variables IX, IY, IZ in RANDOM(L) should be set integer values in the range 1 through 30000. The sum of IX, IY, IZ should not be greater than 30323.

4.4 CONSIM

4.4.1 The Model

CONSIM is a discrete, event-oriented computer simulation model, i.e., the status of the system and the simulation clock are updated when an event takes place. The following are the events in CONSIM: (1) cutting and loading, (2) hauling, (3) roof-bolting, (4) equipment breakdown, (5) completion of cut, and (6) end of job. At the beginning of simulation all equipment are assumed to be in working condition and the miner is in the first or last heading numbered as one. The roof-bolter may be in any heading to be roof-bolted -- not necessarily the one next to where the miner is in.

A macro flowchart for CONSIM is shown in Figure 8. The variables used in CONSIM are defined in APPENDIX A and a detailed flowchart of CONSIM is given in APPENDIX B. The functions and subroutines used in CONSIM, with their purpose, are given in Table 3. The CONSIM program is listed in APPENDIX C.

CONSIM requires a minimum amount of data to be input by the user. These data are essentially the dimensions of workings, the operational and maintenance characteristics of the equipment.

Format of the output used in FACESIM was changed. The output may be obtained by cut, shift or the simulation time

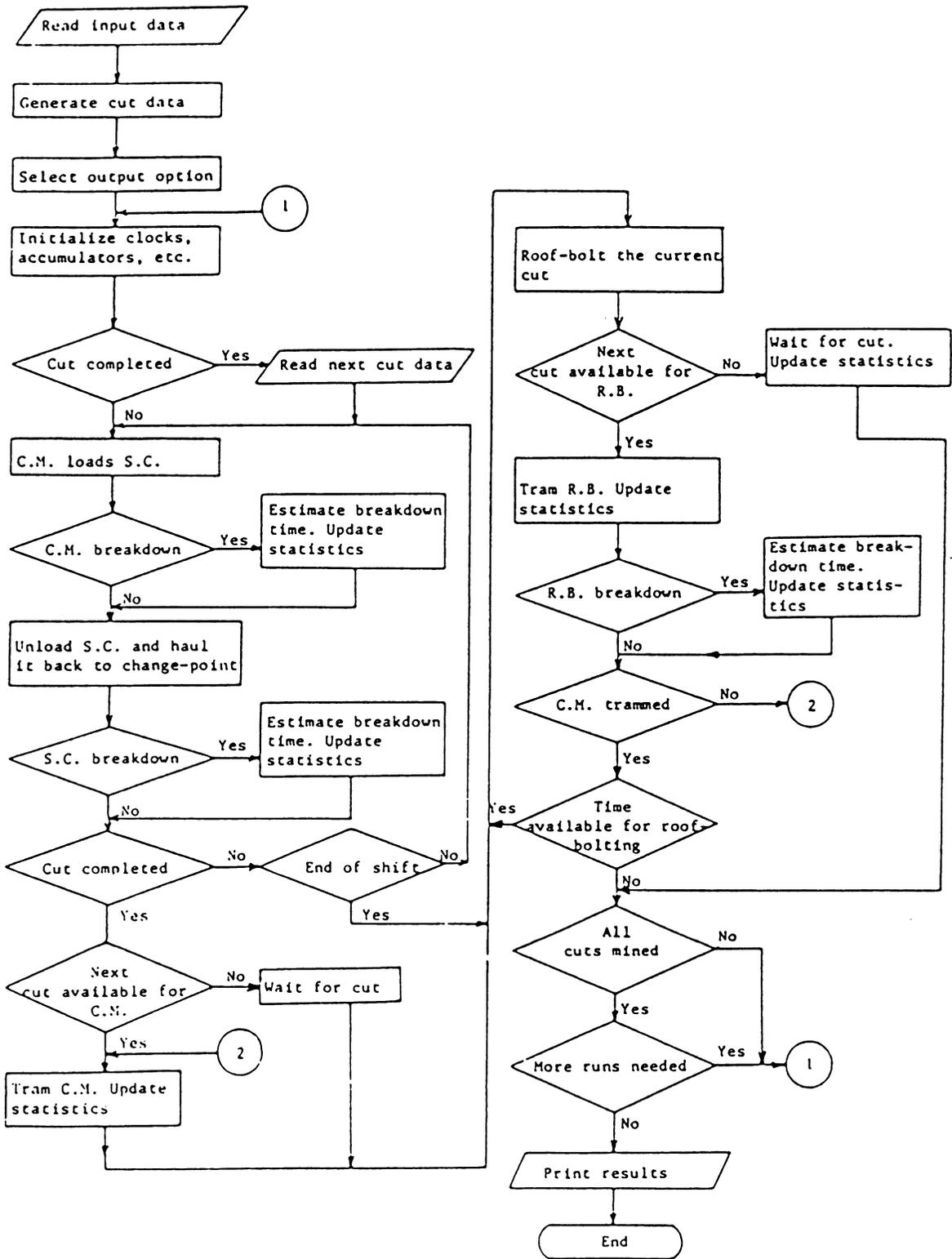


Figure 8
Macro Flowchart for CONSIM

TABLE 3

Subprograms in CONSIM and Their Purposes

SUBPROGRAM	PURPOSE
RANDG	Subroutine to generate continuous random variates from empirical distributions defined by observed values of loading rate, shuttle car payload, haul rates and discharge time.
RANDOM(L)	Function which generates uniform (0,1) random numbers.
EXPON(XM)	Function to generate an exponential random variate with mean XM.
GCARD	Subroutine which generates input data for cuts made in development.
DIST	Subroutine called in subroutine GCARD to calculate distances.

to mine all cuts. The performance measures of the system that can be obtained from CONSIM are more than what one gets from FACESIM. Though the simulation output by cut may not be of any use to make inferences, they will be of help in finding any error in the input data due to some unknown reason. This serves the same purpose as the TRACE command in many simulation languages.

4.4.2 Input Data Preparation

The performance measures (the output) of the system obtained from a simulation model are dependent upon the values of the input variables. Since the user is interested in evaluating the changes in performance measures as a result of the changes in input variables, it is important for the successful simulation study that the user prepares the input data, making certain that errors are eliminated and accuracy in estimation is improved as far as possible. Therefore, preparation of input data is discussed in this chapter.

4.4.2.1 Input Data Cards

Nine different type of input data cards are needed for CONSIM. These cards named Card Type A through Card Type I in alphabetical order. The definitions of input variables are given are in Table 4 through Table 12. They are listed in the order that they are to be input. The formats of input

data are given in parantheses. The number of input data cards equals eight plus the number of cards required to define the empirical distributions (Card Type H) and to input data for roof bolter operation and cut dimensions (Card Type I). Data preparation for Card Type H is explained in 4.4.2.2 Empirical Probability Distributions.

The Table 13 defines the codes (KODE(I) for cut I) for cuts developed by subroutine GCARD. These codes are used in the main program to obtain the dimensions of cuts and roof bolter cycle times and tram functions. First eight codes are used to obtain values of these variables in development and the last one is used for dummy cut(s).

When inputting cut dimensions for multiple cuts taken in breakthroughs during the development, depth of cut should not be changed; however, appropriately modify the width of cut so that the amount of coal mined from the cut remains unaltered. If one of the cuts made in multiple cuts is of reduced depth, use the regular cut depth, but change the width of cut. In addition, a card should be inserted for dummy cuts. This last input data card should have zeros for RNRSUP(I) and RMRSUP(I) and any positive numbers for the dimensions of cut.

TABLE 4

Input Data Card Type A

VARIABLE	DEFINITION
KT	The first cut to be worked by the roof bolter. This can be any cut numbered less than or equal to the number of headings but not '1' which is the first cut worked by the continuous miner (I5).
NTSC	If different mean breakdown times (and mean time between breakdowns) are used for shuttle cars, enter the number of shuttle cars, NSC. If all the shuttle cars have the same breakdown characteristics, enter '1' (I5).
NSC	Numbers of shuttle cars to be used with continuous miner (I5).
NDUMP	Type of dump. Enter one for one-way dump, two for two-way dump (I5).
ICBCO	Type of output. Enter -1 for output by cut, 0 for output by shift, 1 for output by the total time required to mine all the cuts (I5).
NA	Maximum number input cards used to define empirical distributions for loading rate, shuttle car payload, shuttle car haul rates and discharge rate (I5).
NB	Number of input data cards used to input dimensions of cuts and cycle times and tram functions of roof bolter. It is equal to 9 (I5).
NREP	Replications to be made. Replications are independent runs of the program with the same data but different sets of seeds for random number generator. This is required to calculate the mean and standard deviation of output variables (I5).

TABLE 5
Input Data Card Type B

VARIABLE	DEFINITION
SHFT	Production time in a shift in minutes. This equals the scheduled shift time minus the time required to start work at the face and the time required to get out of the mine at the end of shift (F5.1).
DENS	Density of coal in tons/cu.ft (F5.3).
TL	Tram rate of continuous miner in minutes/ft (F5.4).
TR	Tram rate of roof bolter in minutes/ft (F5.4).
SWI	The time required by an empty shuttle car to provide clearance for a loaded car by tramping into an entry at the change point in minutes (F5.2).
SWO	The time required by the shuttle car to return to the haulage road after switch-in in minutes (F5.2).
CL1	The time required for any function other than production done by miner in by the passing point in minutes. This is called in-place constant. Examples of these functions are gas check, hang brattice. This should be specified in minutes (F5.2).
CR1	Same as above, but for roof bolter, in minutes (F5.2).

TABLE 6
Input Data Card Type C

VARIABLE	DEFINITION
XM1	Mean time between breakdowns for continuous miner (F10.2, 2X).
XM3	Mean time between breakdowns for roof bolter (F10.2, 2x).
XM4	Mean breakdown time for continuous miner (F10.2, 2X).
XM6	Mean breakdown time for roof bolter (F10.2, 2X).

TABLE 7

Input Data Card Type D

VARIABLE	DEFINITION
XM2(I)	Mean time between breakdowns for shuttle car type I. I takes the values 1 through NTSC. See Table 4 (F10.2, 2x).
XM5(I)	Mean breakdown time for shuttle car type I. I takes the values 1 through NTSC (F10.2, 2X).

TABLE 8

Input Data Card Type E

VARIABLE	DEFINITION
L	Dummy variable for uniform (0,1) random number generator (I10).
IX, IY, IZ	Initial seeds for uniform (0,1) random number generator. The sum of IX, IY, IZ should not be greater than 30323. For example, IX = 12345, IY = 6678 and IZ = 7890 (3I10).

TABLE 9

Input Data Card Type F

(Read in Subroutine GCARD)

VARIABLE	DEFINITION
W(I)	Width of cut: in non-transport heading, for I=1; in transport heading, for I=2; in breakthrough for I=3 (3(F5.1)).
DTH	Depth of cut in development in feet (F5.1).
WHPIL	Width of pillar along heading in feet (F5.1).
WPIL	Width of pillar along breakthrough in feet (F5.1).
ALM	Length of continuous miner in feet (F5.1).
SCL	Length of shuttle car in feet (F5.1).
SDIST	Center-line distance of the first cut from the center of breakthrough along the heading in feet (F5.1).
DCPD	Discharge change-out distance in feet (F5.1).

TABLE 10

Input Data Card Type G

(Read in Subroutine GCARD)

VARIABLE	DEFINITION
NCM	Number of cuts to be made in development (I5).
MULTI	Control variable for type of cut to be made in breakthrough. Enter '1' for single cut and '2' for multiple cut (I5).
KHEAD	Number of headings in a panel (I5).
NHT	Number of the transport heading (I5).
KT	The first cut to be worked by the roof bolter. This can be any cut numbered less than or equal to the number of headings but not '1' which is the first cut worked by the continuous miner (I5).
NPC	Distance to be advanced in development in terms of number of center-line pillar distance (I5).
LPC	Control variable for movement of dump. Enter '0', if the dump is not to be moved; otherwise, any positive number (I5).

TABLE 11

Input Data to Define Empirical Distributions

(Card Type H)

VARIABLE	DEFINITION
(Note RLA(.) through RH(.) should be specified in each card. There are NA such cards.)	
RLA(.)	Upper limit of interval for loading rate of the miner in minutes/shuttle car (F5.2).
RLB(.)	Upper limit of interval for shuttle car payload in tons (F5.2).
RLC(.)	Upper limit of interval for loaded shuttle car haul rate from miner to change point in min/ft (F5.4).
RLD(.)	Upper limit of interval for loaded shuttle car haul rate from change point to dump in min/ft (F5.4).
RLE(.)	Upper limit of interval for empty shuttle car haul rate from dump to change point in min/ft (F5.4).
RLG(.)	Upper limit of interval for empty shuttle car haul rate from change point to miner in min/ft (F5.4).
RLH(.)	Upper limit of interval for discharge time in minutes (per shuttle car) (F5.2).
RA(.)	Cumulative distribution function for RLA(.) (F5.3).
RB(.)	Cumulative distribution function for RLB(.) (F5.3).

Table 11 (Continued)
Input Data to Define Empirical Distributions
(Card Type H)

VARIABLE	DEFINITION
RC(.)	Cumulative distribution function for RLC(.) (F5.3).
RD(.)	Cumulative distribution function for RLD(.) (F5.3).
RE(.)	Cumulative distribution function for RLE(.) (F5.3).
RG(.)	Cumulative distribution function for RLG(.) (F5.3).
RH(.)	Cumulative distribution function for RLH(.) (F5.3).

TABLE 12

Data for Roof Bolter Operation and Cut Dimensions

(Card Type I)

VARIABLE	DEFINITION
(Note that RNRSUP(.) through DTH(.) should be specified in each card. There are NB such cards.)	
RNRSUP(I)	Roof bolter cycle time for code I in minutes (F6.2).
RMRSUP(I)	Roof bolter tram function for code I in minutes (F6.2).
HT(I)	Height of cut for code I in feet (F6.2).
W(I)	Width of cut for code I in feet (F6.2).
DTH(I)	Depth of cut for code I in feet (F6.2).

TABLE 13

Definition of Codes for Cut Dimensions and Roof Bolter
Operation

KODE(I)	Description
1	Non-transport heading.
2	Transport heading.
3	Single cut in breakthrough.
4	Single cut in breakthrough with reduced depth of cut.
5	Multiple cut in breakthrough with regular depth of cut in the first and last heading.
6	Multiple cut in breakthrough with regular depth of cut in headings other than mentioned above.
7	Multiple cut in breakthrough with a reduced depth (the last one in breakthrough, if the last cut of reduced depth) of cut in the first and last headings.
8	Same as above, but in headings other than mentioned above.
9	For dummy cut(s).

4.4.2.2 Empirical Probability Distributions

The observed data are used to specify the probability distribution of the loading rate of the continuous miner, the haul rates (loaded or empty) of shuttle cars, and the discharge time. Different distributions for the haul rates of shuttle cars are used for the distance between the miner and the change point and the distance between the change point and dump both when loaded and empty. If they are expected to be the same (or they are statistically found to be the same) the amount of data required may be minimized by appropriately modifying the subroutine RANDG.

The haul rates of shuttle cars can be obtained by dividing haul time by haul distance. The loading rate of the miner is the loading time divided by the shuttle car load. Loading time includes any unproductive work that has to be done while loading. It is suggested that if the determination of the shuttle car load is difficult or impossible it may be assumed to be its design capacity or a fraction of it, the fraction being the fill factor determined from experience or by some other means.

Since the variables requiring empirical probability distribution are continuous variables, the observed values of each variable are to be grouped into one of k adjacent intervals, say, $[a_0, a_1]$, $(a_1, a_2]$, $(a_2, a_3]$, \dots , $(a_{k-1}, a_k]$ so that the j th interval contains n_j observations, where

$n_1+n_2+n_3+\dots+n_k=n$ where n is the number of observations. The intervals need not be equally spaced. A piecewise linear empirical distribution function F is specified by $F(a_0)=0$ and $F(a_j)=(n_1+n_2+\dots+n_j)/n$ for $j=1, 2, \dots, k$ (Law and Kelton, 1982). Interpolating linearly between the a_j 's,

$$\begin{aligned}
 F(x) &= 0 && \text{if } x < a_0 \\
 &= F(a_{j-1}) + (x - a_{j-1})[F(a_j) - F(a_{j-1})] / (a_j - a_{j-1}) && \text{if } a_{j-1} < x < a_j \\
 &&& \text{for } j=1, \dots, k \\
 &= 1 && \text{if } a_k < x
 \end{aligned}$$

Note that the interval is closed at the upper limit, i.e., the upper limit is included in the interval and each observation enters only one group.

The first data card of NA data cards used to define the empirical probability distributions establish the lower limits of the distributions and the last set of data for each random variable define the upper limit of the distribution (There is no need to have NA intervals for each random variable). Note that the cumulative distribution function for each random variable is zero at the lower limit of the distribution and one at the upper limit of the distribution.

4.4.2.3 Estimation of Parameters for Equipment Breakdowns

In the estimation of distribution parameters for the time between breakdowns and the breakdown times of equipment, only the production time is to be accounted for, i.e. exclude the time required to start work at the beginning of shift and the time required to stop the work at the end of shift.

For the exponential distribution used to generate time between the breakdowns and breakdown times, only one parameter needs to be estimated. This parameter of exponential distribution is the population mean. The maximum likelihood estimator of the population mean for exponential distribution is the sample mean.

If all the shuttle cars have the same mean time between breakdowns and the same mean breakdown time, the input variable NTSC should be assigned the value '1' and one value should be entered for each of these variables. If they are not the same, NTSC should equal NSC, the number of shuttle cars hauling coal from continuous miner to dump.

4.4.2.4 Switch-in and Switch-out Times

If only one shuttle car is being loaded by the continuous miner, the shuttle car does not need to switch-in. Therefore, the input values for switch-in and switch-out should be zero.

Since it was assumed that the shuttle cars may switch in and out of a breakthrough when the continuous miner is in any heading, the number of times the shuttle car does not switch in or out of a breakthrough is also to be counted and the time should be entered as zero when making a time study.

4.4.2.5 Simulation of Conveyor Operation

If conveyors are used to haul coal from the face, the haul rates of shuttle cars, the discharge rates and switch-in and switch-out times should be zero. For the empirical distribution of the pay-load of a shuttle car enter one with a probability of one. For the empirical distribution of the loading rate of a continuous miner, the average loading rate may be entered with a probability of one, if the variation in the loading rate is insignificant or not of interest to the user. The one-way dump is to be used with a conveyor system.

4.4.2.6 Simulation of Automated Miner-Bolter

To simulate the operation of a miner with roof bolter mounted on it, the values of the input variables for the roof bolter should be zero and the loading rate should be adjusted to include the time required for roof bolting or it may be entered as CL1.

4.4.2.7 Estimation of Distribution Parameters in the Absence of Data

If data are not available for times between breakdowns and breakdown times and/or one does not wish to simulate breakdowns of equipment, enter 'infinity' (i.e., a very large number) for mean time between breakdowns and zero for mean breakdown times. This may be done for one or more equipment. In this case, the production time in a shift should be reduced by the average total breakdown time of miner in a shift.

It is not always possible to collect data on random variables of interest because the system being studied does not exist or adequate data may not be available for the system under study. In such cases, if a deterministic simulation is not desired, the heuristic procedures mentioned by Law and Kelton (1982) may be used. These procedures are described here.

In the first method, identify an interval $[a, b]$ (a and b are real numbers such that $a < b$) in which the random variable of interest will lie with probability close to one. Obtain a probability density function on $[a, b]$ which is thought to be representative of the random variable. If the probability density function is expected to be unimodal, the mode being the most likely value, then a triangular probability density function may be considered.

Alternately, beta(α_1 , α_2) distribution may be placed over the interval (a, b) since the time to perform a task has been found to be skewed to the right and the beta distribution has been found to fit it satisfactorily. Given subjective estimates of mean u and mode m , the parameters of beta distribution α_1 and α_2 can be obtained from the following expressions:

$$\alpha_1 = \frac{(u-a)(2m-a-b)}{(m-u)(b-a)} \quad \text{and}$$

$$\alpha_2 = \frac{(b-u)\alpha_1}{(u-a)}$$

Note that if $u > m$, the probability density function is skewed to the right; if $u < m$, it will be skewed to the left. Note that a uniform distribution over an interval (a, b) corresponds to a beta(1, 1) distribution over the same interval. Algorithms to generate random variates from triangular, beta and Weibull distributions are given in APPENDIX D.

4.4.3 Sample Input and Output

CONSIM requires a minimum amount of data to be input by the user. These data are essentially the dimensions of workings, the operational and maintenance characteristics of the equipment. To provide an example for use of CONSIM, a hypothetical three heading continuous mining section was simulated (Figure 9). The pillars are at 90 X 90 feet centers. The widths of headings and breakthroughs are 19 feet. The depth of a cut is 20 feet. The dump is located at the intersection of heading and breakthrough. Two shuttle cars of 7-ton payload are used to haul coal from the miner to dump. One roof bolter is used for roof-bolting. Initially the miner is in the first heading and the bolter in the third heading. The distance of the cut from breakthrough is 80 feet. It was specified to make eleven cuts. The production time in a shift is 430 minutes. The input data for the example are shown in Table 14.

CONSIM was run once and the output is given in Table 15. From Table 15, it may be read that the duration of the first shift is 430.1 minutes of which the miner spent 208.1 minutes loading 829.2 tons of coal, 121.1 minutes on change-out, 0.5 minutes on waiting for shuttle cars, 45.8 minutes on waiting for entry into next cut because the roof bolter has not completed bolting the cut, 25.0 minutes tramping

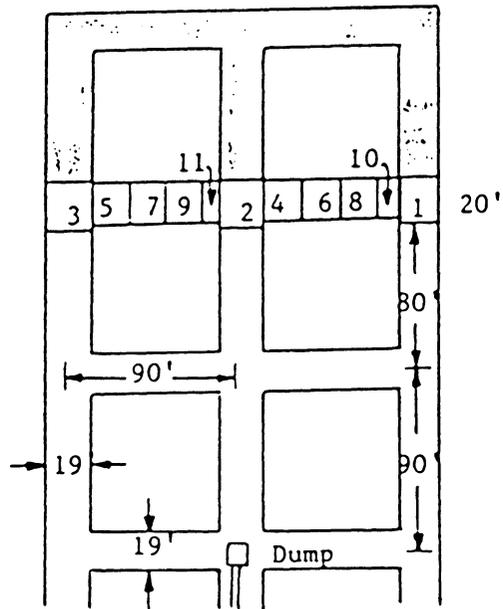


Figure 9
Layout for CONSIM Input Data

Table 14
A Sample Input for CONSIM

Input Data													Card Type
3	1	2	1	0	22	9	1						
430.00	.043	.0094	.0106	00.0000	.0000	.0000	.0000						A (Table 4)
481.10		1462.80			25.10		66.60						B (Table 5)
419.70		10.5											C (Table 6)
	25	12345			6678		7890						D (Table 7)
19.0	19.0	19.0	20.0	71.0	71.0	32.0	28.0	80.0	00.0				E (Table 8)
11	1	3	2	3	2	1						F (Table 9)	
0.80	6.0	.0024	.0023	.0022	.0021	0.59	.000	.000	.000	.000	.000	.000	G (Table 10)
0.90	7.0	.0025	.0024	.0023	.0025	0.59	.0191	.000	.041	.051	.164	.0221	.000
1.00		.0026	.0025	.0024	.0026		.112		.110	.288	.136	.179	
1.10		.0027	.0026	.0025	.0027		.292		.205	.425	.186	.299	
1.20		.0028	.0027	.0026	.0028		.442		.315	.550	.271	.328	
1.30		.0029	.0028	.0027	.0029		.572		.329	.625	.429	.373	
1.40		.0030	.0029	.0028	.0030		.609		.507	.675	.529	.463	
1.50		.0031	.0030	.0029	.0031		.628		.589	.775	.657	.522	
1.60		.0032	.0031	.0030	.0032		.646		.658	.788	.743	.627	
1.70		.0033	.0032	.0031	.0033		.683		.671	.850	.814	.687	
1.80		.0034	.0033	.0032	.0034		.702		.726	.863	.900	.716	
1.90		.0035	.0034	.0035	.0035		.720		.808	.875	.914	.731	
2.00		.0036	.0035	.0036	.0036		.776		.822	.888	.943	.776	
2.10		.0037	.0037	.0037	.0037		.794		.849	.900	.971	.791	
2.20		.0038	.0038	.0040	.0038		.813		.863	.925	1.000	.821	
2.40		.0039	.0039		.0039		.850		.904	.938		.866	
2.50		.0040	.0043		.0040		.887		.959	.950		.925	
2.60		.0041	.0047		.0043		.905		.973	.963		.940	
2.80		.0043	.0050		.0045		.924		.986	.988		.970	
3.00		.0048	.0052		.0047		.961		1.000	1.000		1.000	
4.00							.979						
5.00							1.000						

Table 14 (Continued)
 A Sample Input for CONSIM

Input Data	Card Type
56.00 00.00 06.00 19.00 20.00	I (Table 12)
56.00 00.00 06.00 19.00 20.00	
56.00 00.00 06.00 19.00 20.00	
56.00 00.00 06.00 19.00 11.00	
56.00 00.00 06.00 19.00 20.00	
56.00 00.00 06.00 19.00 20.00	
56.00 00.00 06.00 19.00 20.00	
56.00 00.00 06.00 19.00 20.00	
00.00 00.00 06.00 19.00 20.00	
/	
//	

Table 15
A Sample Output from CONSIM

ANALYSIS OF CONTINUOUS MINING SYSTEM

ALL TIMES IN MINUTES

RUN 1 OF 1

SYSTEM PERFORMANCE BY SHIFT

SHIFT NO.	TIME	LOAD	CHANGE OUT	WAIT-CAR	WAIT-COAL	TRAM	REPAIR (CM)	HAUL DIST	TONS	T/M	CM AT	WAIT-RB	REPAIR RB	RB AT
1	430.1	208.1	121.1	0.5	45.8	25.0	29.7	13.0	829.2	1.93	9	0.0	0.0	7
2	163.4	43.6	32.1	0.0	77.5	10.2	0.0	3.2	161.0	0.99	11	0.0	0.0	9

SYSTEM PERFORMANCE OVER SIMULATION TIME

TIME	LOAD	CHANGE OUT	WAIT-CAR	WAIT-COAL	TRAM	REPAIR (CM)	HAUL DIST	TONS	T/M	WAIT-RB	REPAIR RB	TIME RB	TONS /MILE
593.5	251.6	153.2	0.5	123.3	35.2	29.7	16.2	990.2	1.67	0.0	0.0	596.1	61.3

between cuts and 29.7 minutes for repairs. The shuttle cars hauled 13.0 miles between the miner and the dump. The rate of mining was 1.93 tons/minute. At the end of the first shift, the miner is in the ninth cut and the bolter is in the seventh cut. Note that the shift time is more than the specified shift time of 430 minutes. This is because operation in progress at the end of the shift time is allowed to be completed.

4.4.4 Special Features of CONSIM

The special features of CONSIM are the following:

1. It can be run on microcomputers.
2. It is inexpensive to use.
3. It is simple and easy to understand.
4. It can be run interactively or in batch mode.
5. The input data requirements are minimal.
6. It can simulate breakdowns of equipment.
7. It can be used to simulate continuous mining systems with conveyors by specifying tram and discharge rates of shuttle cars as zero. It can also simulate continuous miners with roof bolter mounted on them by

specifying the values of the input variables for the roof bolter as zero.

8. It can be used to simulate development in longwall mining and mining room-and-pillar panels, without the need to make extensive data preparation.

The limitations of CONSIM are the following:

1. It can not simulate miner operation in more than one panel simultaneously.
2. It can not be used if pillars are of irregular sizes.
3. It can not be used for more than two shuttle cars.
4. Time study is required to collect data.

If one prefers deterministic simulation to stochastic simulation and wants to avoid time study, it is still possible to use CONSIM by inputting average performance characteristics of equipment instead of empirical probabilistic data. A stochastic simulation model requiring time study, however, is to be preferred to deterministic simulation for the following reasons:

1. The results obtained from a deterministic simulation does not consider the probabilistic nature of the performance measures of the system.
2. When comparing alternatives by performance measures obtained from a deterministic simulation using equipment characteristics, it is understandable that what can be realized with a system of equipment may not be proportional to these performance measures because of human and environmental factors influencing actual system performance. Therefore, incorporation of of these factors in some way in the simulation model is preferable.

Chapter V

MODEL VALIDATION AND CASE STUDIES

5.1 MODEL VERIFICATION

The model verification was done by going through the computer program with the flowchart to determine if the model translation into FORTRAN was correct. Having confirmed that translation into the FORTRAN program was correct, the program was run to see if it performed as intended in different artificially created conditions. The program was checked and found to function as intended in all possible simulation conditions.

5.2 MODEL VALIDATION

To validate CONSIM, the program was run with the same set of data used in FACESIM without simulating the breakdowns of equipment and other changes made in CONSIM that are not in FACESIM. Identical results were obtained from FACESIM and CONSIM. Therefore, CONSIM is validated with respect to FACESIM. FACESIM has been found to produce sufficiently accurate results in the mining industry (Prelaz, et al, 1964). Since the assumptions made in CONSIM are not grossly different from those in FACESIM, CONSIM is expected to produce reasonably accurate results for real mining systems. These

arguments lead to the conclusion that CONSIM is a reasonably accurate representation of a real continuous mining system.

5.3 CASE STUDIES

To validate CONSIM with respect to real continuous mining systems, i.e., to check if the results obtained from CONSIM are reasonably close to the actual performance of real system, data were collected from two mining operations in West Virginia. For validation purposes, only the coal production per shift from CONSIM was statistically compared with the actual shift production of the operations.

Since no data were available for the time between breakdowns of equipment and time for each breakdown, the breakdowns of equipment could not be simulated. The production time of the miner in a shift was obtained by subtracting the average breakdown time of the miner per shift from the available face time.

On the advice of the industrial engineer familiar with the operations of the equipment in both of the mines and because of the difficulties involved in making time studies to calculate the travel rates of shuttle cars between different points on their haul between the miner and the dump, and to obtain switch-in, switch-out and change-out times, it was assumed that the haul rates of shuttle cars do not vary

significantly whether the shuttle car is loaded or empty and that switch-in, switch-out and change-out times are zero. Since the change-out time was assumed to be zero, the change-out distance is zero. In other words, the shuttle cars change out at the miner and the haul distance is the distance between the miner and the dump change point and any switch-in and switch-out times are included in the time required to haul to and from the miner.

In both the mines, the dump is located at the intersection of the heading and breakthrough. Therefore, the dump change-out distance is zero. Since the discharge rate of shuttle cars is mainly dependent on the belt speed which is kept constant, the discharge rate was assumed constant. The discharge time for a shuttle car was 25 seconds and 35 seconds in the first and second mine respectively.

On the advice of the industrial engineer, the shuttle car load was assumed to be distributed as the shuttle car payload minus uniformly distributed load between zero and one ton.

5.3.1 Case Study I

In the first mining operation, the miner drives six headings in a 42-inch thick seam. The width of the heading and breakthrough is 18 feet. The pillars are at 90 x 90 feet

centers. The miners makes a 20-foot cut in headings and breakthroughs. Single cuts are made in breakthroughs. The dump is located in heading number three. The layout of the section is shown in Figure 10. Two shuttle cars of 5-ton capacity are used to haul coal from the miner to the dump. One roof bolter is in operation in this section of the mine.

When the time study was made, the miner was driving headings three through six; the miner was initially in heading number six and the roof bolter was waiting to move into heading number six. Headings one and two were not mined. Therefore, for the purpose of validation, it was assumed that there were four headings, the dump being located in heading number four. The miner was assumed to be in heading number four initially, the bolter waiting for the miner. The initial conditions were set to simulate the operations as closely as possible when the time study was made.

The program was run with the data from this mine and the mean and standard deviation of production per shift were obtained. The mean shift production from CONSIM IS 418.5 tons. The 90% confidence interval for production per shift (in tons) is (403.4, 433.6). The actual production of the miner when the time study was made was 420 tons. The 90% confidence interval for production per shift obtained from CONSIM covers the actual production realized.

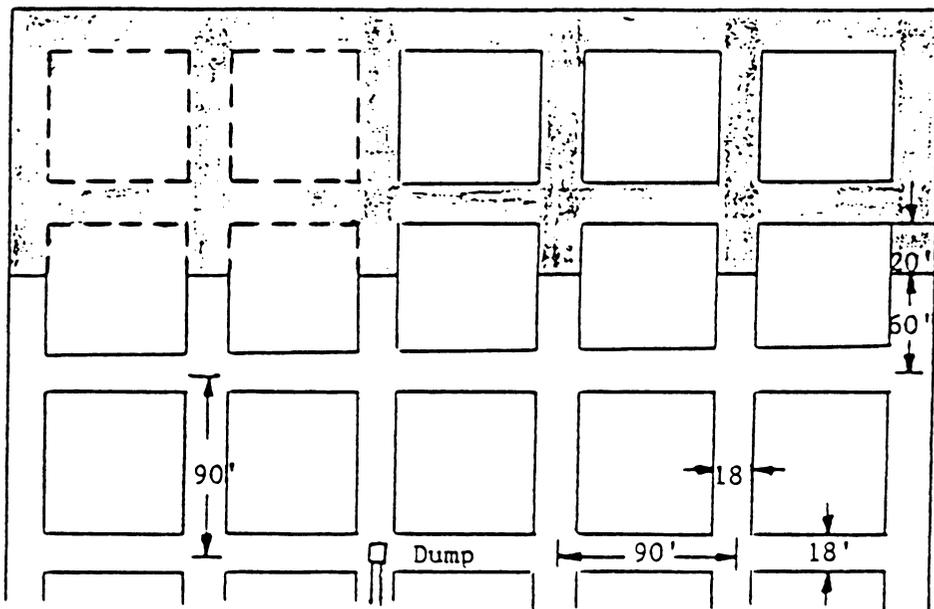


Figure 10
Layout for Case Study I

5.3.2 Case Study II

In the second mining operation, the miner makes chain pillars with three headings in a 6-foot thick seam. The dump is located in the second heading. The width of heading and breakthrough is 19 feet. The pillars are at 90 x 90 feet centers. The miner makes 20-foot cut in headings and breakthroughs. Single cuts are made in breakthroughs. The layout of the section is shown in Figure 11. Two shuttle cars of 7-ton capacity are used to haul coal from the miner to the dump. One roof bolter is in operation in this section of the mine. The initial conditions were set to simulate the operations as closely as possible when the time study was made.

The program was run to get statistics on shift production. The mean shift production from CONSIM is 393.7 tons. The 90% confidence interval for production per shift (in tons) was (376.1, 411.3). The actual production of the miner when the time study was made was 400 tons. The 90% confidence interval for production per shift obtained from CONSIM covers the actual production realized.

From the two case studies, it is concluded that CONSIM simulates the continuous mining systems satisfactorily.

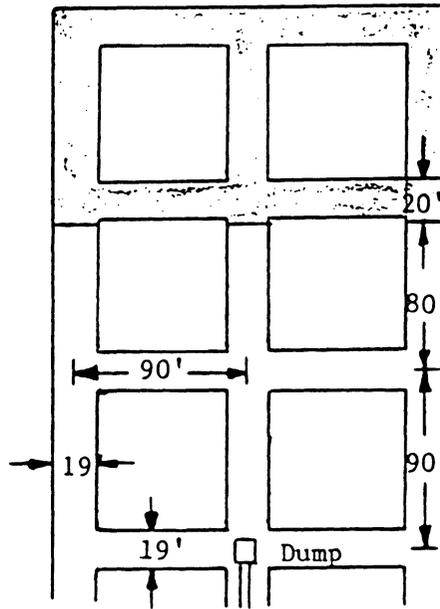


Figure 11
Layout for Case Study II

5.3.3 Analysis of Mining Operations

To illustrate some possible uses of CONSIM in analyzing existing face operations in continuous mining systems, CONSIM was run making changes in the input data collected from case studies and the change in shift production level was noted. No attempt was made to check the technical feasibility of implementing the changes made, or to analyze all possible changes or their combination, since it is only aimed to show a few possible uses of CONSIM. The changes made in input data and the results from CONSIM are shown in Table 16.

For the first mine, the following changes in the face operation were analyzed:

1. Reduce loading time of shuttle car by 25%.
2. Increase the center-line distance between pillars to 110 feet and the width of cut to 25 feet.

In the first case, the miner spent less time loading shuttle cars and more time waiting for them. Only 1% improvement in shift production level was achieved. In the second case, more coal could be mined in a cut because of increased width of cut. This resulted in fewer place changes per shift and lower shift tram time. However, because of longer haulage distance between the miner and the dump, the

TABLE 16

Analysis of Mining Operations

Change analyzed	Shift production (tons)		Change in shift production
	Actual	Mean from CONSIM	
<u>Mine No.1</u>	420.0		
1. Original system		418.5	
2. Load time/S.C. reduced by 25%		426.0	1.4%
3. Width of cut & pillar: 25 & 110 ft		371.6	-11.5%
<u>Mine No.2</u>	400.0		
4. Original system		393.7	
5. S.C. payload: 9t		480.6	20.2%
6. 50% reduction in breakdown time		405.8	1.5%

miner had to wait longer for shuttle car lowering the shift production by 12%. Therefore, increasing the size of pillars and width of cuts is not desirable or reducing the shuttle car loading time is not attractive. Since, in both the cases, the miner spends a lot of time waiting for shuttle car, reducing it by putting more shuttle cars to haul coal or reducing shuttle car hauling time by increasing shuttle car haul rate may improve the shift production.

For the second mine, the following changes were analyzed:

1. Increase the shuttle car payload from 7 tons to 9 tons.
2. Decrease the miner breakdown time by 50%.

Lowering the miner breakdown time per shift by 50%, i.e., 15 minutes does not greatly improve the shift production since the miner already spends a large percentage of its time waiting for shuttle car. There is sharp improvement in shift production in the first and the last case. In the first case, the miner spent more time tramming between cuts per shift while the time the miner spent on other activities remained essentially the same. The increase tramming time per shift is due to more number of cuts that could be mined. Since only the shuttle car payload was changed in the input data, the increase in the shift production was achieved not

only by increased shuttle car payload but faster loading and unloading.

Chapter VI

CONCLUSIONS AND RECOMMENDATIONS

6.1 CONCLUSIONS

A computer simulation model was successfully built to simulate continuous mining systems on micro-computers. The computer program was run on an IBM personal computer (with a FORTRAN 77 compiler) and an Ithaca micro-computer (with a FORTRAN 80 compiler) without any problem. Both computer systems have 64K random access memory. The only change required to make in the program when using it on different micro-computers is to check if the input/output units are correctly specified because different computers have different unit numbers for the same input/output units. The printer should be able to print 132 characters in a line.

CONSIM is simple and inexpensive to use. It can be used by anyone without much experience in simulation. Input data required are minimum and not much effort is required on the part of the user to prepare the data. CONSIM can also be run interactively.

There are several options available to the CONSIM user. He can specify any number of headings and designate any of them as transport heading. The breakthroughs need not be at right angle to the heading. Single or or multiple cuts may

be made in breakthroughs. Simulation of automated miner-bolter, conveyor system and breakdowns of miner, shuttle cars and bolter are possible.

CONSIM can be used to design section layout, to select and evaluate equipment and to establish production standards.

6.2 RECOMMENDATIONS

The recommendations for future research in this area are the following:

1. Modifying CONSIM to simulate the miner operations in more than one panel. This makes possible simulation of all the face mining operations in a mine simultaneously.
2. Modifying CONSIM to simulate more than one miner bolter operation in a section.
3. Incorporation of a cost model to aid the user in financial analysis.
4. Development of simulation models of other mine systems such as ventilation systems, etc. and integrating them in CONSIM so that the entire mine system can be simultaneously optimized.

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APPENDIX A
DEFINITION OF VARIABLES

DEFINITION OF VARIABLES

The variables are given in the order they are executed in the program. To avoid repetition, the variable defined previously in the main program or in a subprogram is not defined again in another subprogram. All times are in minutes.

The variables used in the main program are the following:

KT	The first cut to be worked by the roof bolter.
NTSC	Number of mean times between breakdowns or mean breakdown times to be specified for shuttle car(s). This equals one or the number of shuttle cars used, NSC.
NSC	Numbers of shuttle cars to be used with continuous miner.
NDUMP	Type of dump. Enter one for one-way dump, two for two-way dump.
ICBCO	Type of output. Enter -1 for output by cut, 0 for output by shift, 1 for output

by the time required to mine all the cuts.

- NA Number of input cards used to define empirical distributions for loading rate, shuttle car payload, shuttle car haul rates and discharge rate.
- NB Number of input data cards used to input dimensions of cuts and cycle times and tram functions of roof bolter. It is equal to 9.
- NREP Number of replications to be made.
- SHFT Production time in a shift. This equals the scheduled shift time excluding the times required to start work and to get out of the mine at the end of shift.
- DENS Density of coal in tons/cu.ft.
- TL Tram rate of continuous miner in min/ft.
- TR Tram rate roof bolter in min/ft.
- SWI The time required by an empty shuttle car to provide clearance for a loaded car by tramping into an entry at change point.

SWO	The time required by the shuttle car to return to the haulage road after switch-in.
CL1	The time required for any function other than production done by miner in by the passing point. This is called in-place constant in development. Examples of these functions are gas check, hang brattice.
CR1	Same as above, but for roof bolter.
XM1	Mean time between breakdowns for continuous miner.
XM3	Mean time between breakdowns for roof bolter.
XM4	Mean breakdown time for continuous miner.
XM6	Mean breakdown time for roof bolter.
XM2(I)	Mean time between breakdowns for shuttle car I.
XM5(I)	Mean breakdown time for shuttle car I.
L	Dummy variable for uniform(0, 1) random

number generator.

IX, IY, IZ Initial seeds for Uniform(0, 1) random number generator. Their values should lie in the range 1 through 30000. Integer arithmetic upto 30323 is required.

RLA(.) Upper limit of interval for loading rate.

RLB(.) Upper limit of interval for shuttle car payload.

RLC(.) Upper limit of interval for loaded shuttle car haul rate in min/ft -- miner to change point.

RLD(.) Upper limit of interval for loaded shuttle car haul rate in min/ft -- change point to dump.

RLE(.) Upper limit of interval for empty shuttle car haul rate in min/ft -- dump to change point.

RLG(.) Upper limit of interval for empty shuttle car haul rate in min/ft -- change point to miner.

RLH(.) Upper limit of interval for discharge

rate in minutes per shuttle car.

RA(.)	Cumulative distribution function for RLA(.)
RB(.)	Cumulative distribution function for RLB(.)
RC(.)	Cumulative distribution function for RLC(.)
RD(.)	Cumulative distribution function for RLD(.)
RE(.)	Cumulative distribution function for RLE(.)
RG(.)	Cumulative distribution function for RLG(.)
RH(.)	Cumulative distribution function for RLH(.)
RNRSUP(I)	Roof bolter cycle time for code I.
RMRSUP(I)	Roof bolter tram function for code I.
HT(I)	Height of cut for code I.
W(I)	Width of cut for code I.

DTH(I)	Depth of cut for code I.
NREPM	Number of replications made so far (A replication is an independent run of the program).
KREST	Internal control variable.
PLACE(I)	Time when cut I available.
SST(I)	Sample standard deviation of TSP(I).
TTSP(I)	Accumulator for TSP(I) over several runs.
SS(I)	Sample standard deviation of SP(I).
TLOAD, TSP(1)	Accumulator for miner loading time.
TCOT, TSP(2)	Accumulator for shuttle car change-out time.
TWL, TSP(3)	Accumulator for miner wait time for shuttle car.
TWP, TSP(4)	Accumulator for miner wait time for coal.
TTON, TSP(5)	Accumulator for coal mined (in tons).
TTPM, TSP(6)	Accumulator for mining rate (in tons/min).
TWRS, TSP(7)	Accumulator for roof bolter wait time.

TREPTL, TSP(8) Accumulator for miner breakdown time.

TREPTR, TSP(9) Accumulator for roof bolter breakdown
time.

THD, TSP(10) Accumulator for haul distance of shuttle
car(s).

TCYCLE, TSP(11) Accumulator for cut cycle time.

ARC, TSP(12) Clock on roof bolter.

ALC, TSP(13) Clock on continuous miner.

RATE, TSP(14) Mining rate over the time required to
mine all the cuts.

TPMIL, TSP(15) Coal hauled (in tons) per mile of
shuttle car travel over the time required
to mine all the cuts.

TTRAM, TSP(16) Accumulator for miner tram time.

CLOAD Loading time in a cycle.

CCOT Change-out time in a cycle.

WL Miner wait time for shuttle car in a
cycle.

WP Miner wait time for place in a cycle.

CTON Coal mined in a cut (tons).

CTPM Mining rate in a cycle.

CWRS Roof bolter wait time for place during a miner cycle.

CHD Shuttle car haul distance in a cycle.

CYCLE Cycle time.

IDUMP Switch to route shuttle car in a two-way dump. Its initial value is one.

K Cut number.

LIN The first cut to be mined by miner.

M Number of the shuttle car whose operation is being simulated.

KT1 Storage for initial value of KT.

KE1 Next cut to be made available by roof bolter.

KE Cut made available by roof bolter.

FALTL Time at which continuous miner will breakdown. The time between breakdowns is

obtained by random sampling.

TREPTS(I)	Total breakdown time of shuttle car I when all cuts are mined.
ISUR(I)	Operating status of shuttle car I. Enter zero, if available; one, otherwise.
CREPTS(I)	Time the shuttle car I will be under breakdown at the beginning of the next shift.
FALTS(I)	Time at which shuttle car I will breakdown.
FALTR	Time at which the roof bolter is to breakdown.
IRS	Operating status of roof bolter. Zero if the roof bolter is in operation; if not, one).
NSHFT	Number of shifts simulated.
TPLAC	Coal remaining in cut being mined by the miner (in tons).
REM	Time remaining in shift.
CREPTL	Time the miner will be under breakdown in

the beginning of the next shift due to breakdown in a shift.

CREPTR	Same as CREPTL, but for roof bolter.
CTRAM1	Time required in the next shift to complete tramming.
WP1	Time the miner has to wait in the next shift for entry into the next cut.
WRS1	Time the bolter has to wait in the next shift for entry into the next cut.
TARC	Time to tram the bolter into the cut to be roof-bolted.
SLC	Miner loading time in a shift.
STRAM	Miner tramming time in a shift.
TTIME	Simulation clock, i.e., the variable giving current value of simulated time.
SWRS2	Roof bolter wait time for place in a shift when the miner completes mining the previous cut.
SLOAD, SP(1)	Miner loading time in a shift.
STCOT, SP(2)	Shuttle cars change-out time in a shift.

SWL, SP(3) Miner wait time for shuttle cars in a shift.

SWP, SP(4) Miner wait time for place in a shift.

STON, SP(5) Coal mined in a shift (tons).

STPM, SP(6) Shift mining rate.

SWRS, SP(7) Roof bolter wait for place in a shift.

SREPTL, SP(8) Time the miner was under breakdown in a shift.

SREPTR, sp(9) Time the roof bolter was under breakdown in a shift.

SHD, SP(10) Haul distance of shuttle cars in a shift.

SREPTS(I) Breakdown time of shuttle car I in a shift.

IIRS Control to read data for the next cut to be roof-bolted.

PTON Coal initially in a cut (tons).

KODE(I) Code for dimensions of cuts and roof bolter cycle times and tram functions for cut I.

SWL2 Miner wait time for shuttle car in a shift when it completed mining the previous cut.

SLOAD2 Miner load time in a shift when it completed mining the previous cut.

STON2 Coal mined in a shift when the miner completed mining the previous cut.

SHD2 Distance hauled by shuttle car(s) in a shift when the miner completed mining the previous cut.

STCOT2 Change-out time in a shift when the miner completed mining the previous cut.

SCC(I) Clock on shuttle car I.

ALC2 Time on miner clock when the miner completed mining the previous cut.

CPCHK Clock at the change point.

DCPCK, DCPCK2 Clocks at the dump change point.

ALOAD Continuous miner loading rate obtained by random sampling.

SCAPY Shuttle car payload obtained by random sampling.

REPTL Breakdown time of miner obtained by random sampling when it breaks down.

FALTL Time at which the miner will breakdown.

SREPTL Time the miner was under breakdown in a shift.

CPD Change-out distance for cut (ft).

VL1 Haul rate of loaded shuttle car between sampling and dump change point obtained by random sampling.

VL2 Haul rate of loaded shuttle car between dump change point and dump.

VE1 Same as VE1 when the shuttle car is empty.

HD Distance between change point and dump change point of cut.

DISCH Discharge rate obtained by random sampling.

DCPD Dump change-out distance.

REPTS(I) Breakdown time of shuttle car I obtained by random sampling when it breaks down.

J Counter for number of shuttle cars checked for operating status.

DMIN Variable to store the time on shuttle car which will return to operating status the earliest.

VE2 Same as VL2, but when shuttle car is empty.

LT1(I) Tram distance for cut I from passing point to passing point.

LT2(I) Tram distance for cut I from face to passing point.

K1 Cut to be mined next by the miner.

CTRAM Miner tram time in a cycle.

STRAM Miner tram time in a shift.

ICRS Number of cuts roof bolter is behind the miner initially.

KG Cut to be roof-bolted next.

KRS Storage for KODE(KT).

REPTR Roof breakdown time obtained by random
 sampling when the roof bolter breaks
 down.

SP1(I) Sample mean of SP(I).

The following are the variables used in subroutine GCARD:

W(I) Width of cut: in non-transport heading,
 for I=1; in transport heading, for I=2;
 in breakthrough, for I=3.

DTH Depth of cut in development.

WHPIL Length of pillar along heading.

WPIL Length of pillar along breakthrough.

ALM Length of continuous miner.

SCL Length of shuttle car.

SDIST Distance of the first cut from the center
 of the breakthrough in the heading.

NCM Number of cuts to be made in development.

MULTI Control variable for type of cut to be made in breakthrough. Enter one for single cut; two for multiple cut.

KHEAD Number of headings in a panel.

NHT Number of the transport heading.

NPC Distance to be advanced in development in terms of center-to-center pillar distance.

LPC Control variable for movement of dump. Enter zero, if the dump is not to be moved; otherwise, any positive number.

KIL, I, J Internal multipliers for distances.

MIL Control for calculation of distances.

TLT2 Storage for LT2(.).

TD1 Storage for change-out distance.

NP Counter for number of center-to-center pillar distance advanced.

DIST1 =WHPIL+W(3)

DIST2 =DIST1-SCL

DIST3 =WPIL+W(1)

KK Number of cuts to be made in each heading
 for advancement of a minimum of DIST1
 distance.

SDIST2 storage for SDIST.

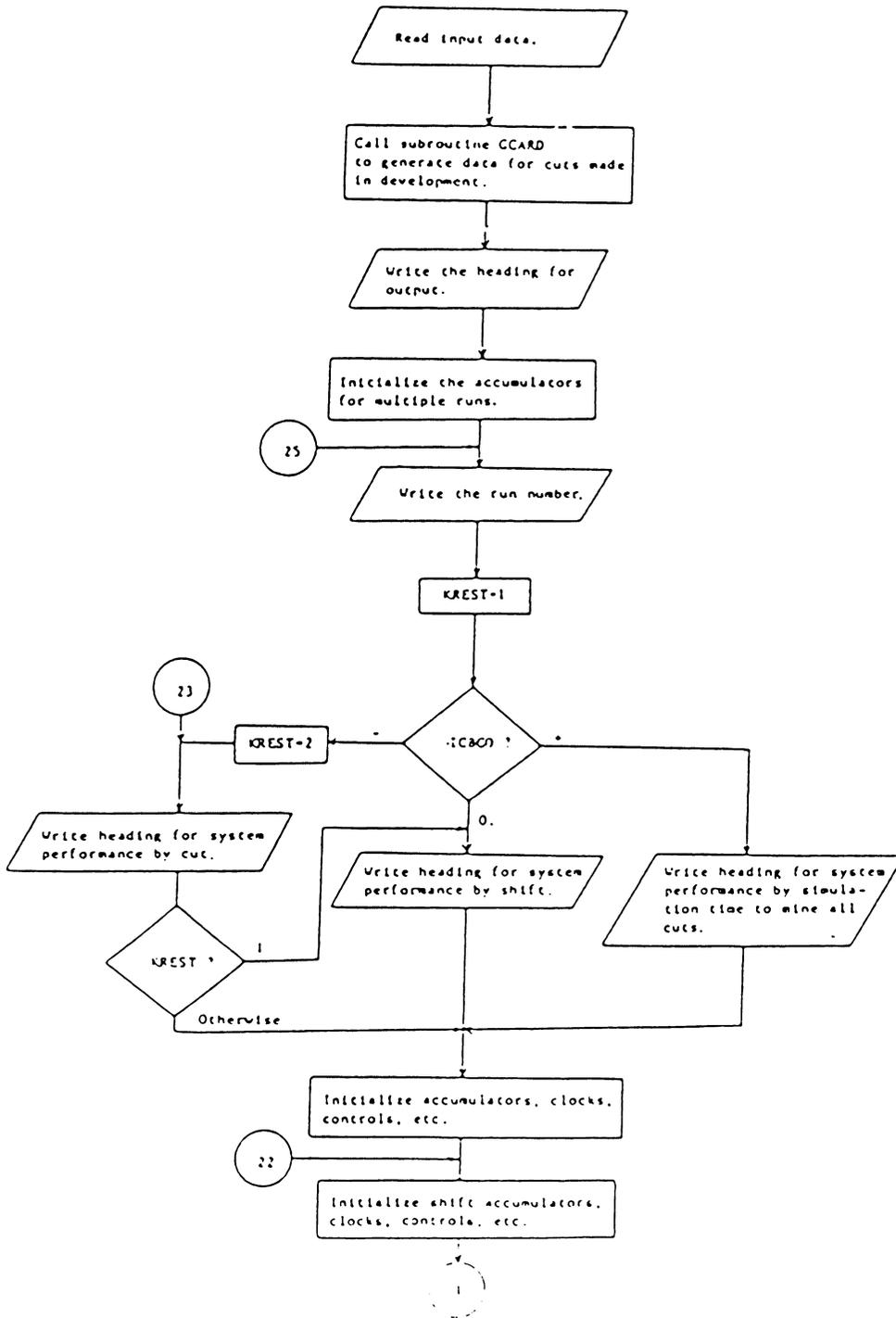
KK1 Number of single cuts to be made before
 another cut in the same breakthrough.

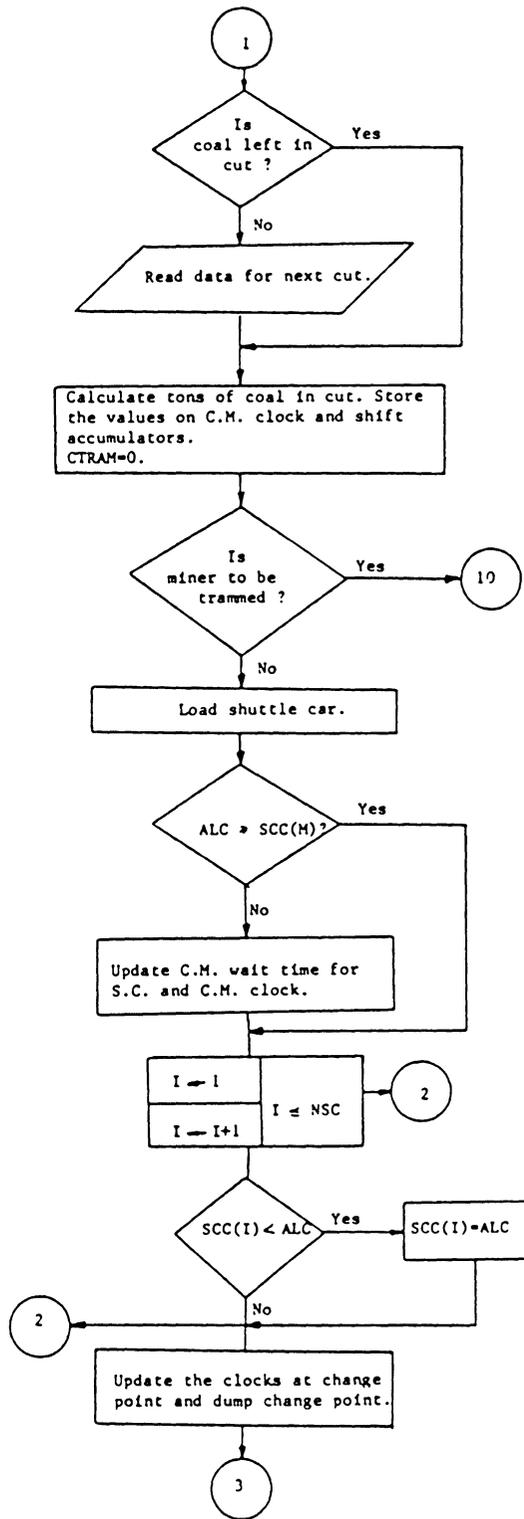
CLAST Width of the last cut in a breakthrough.

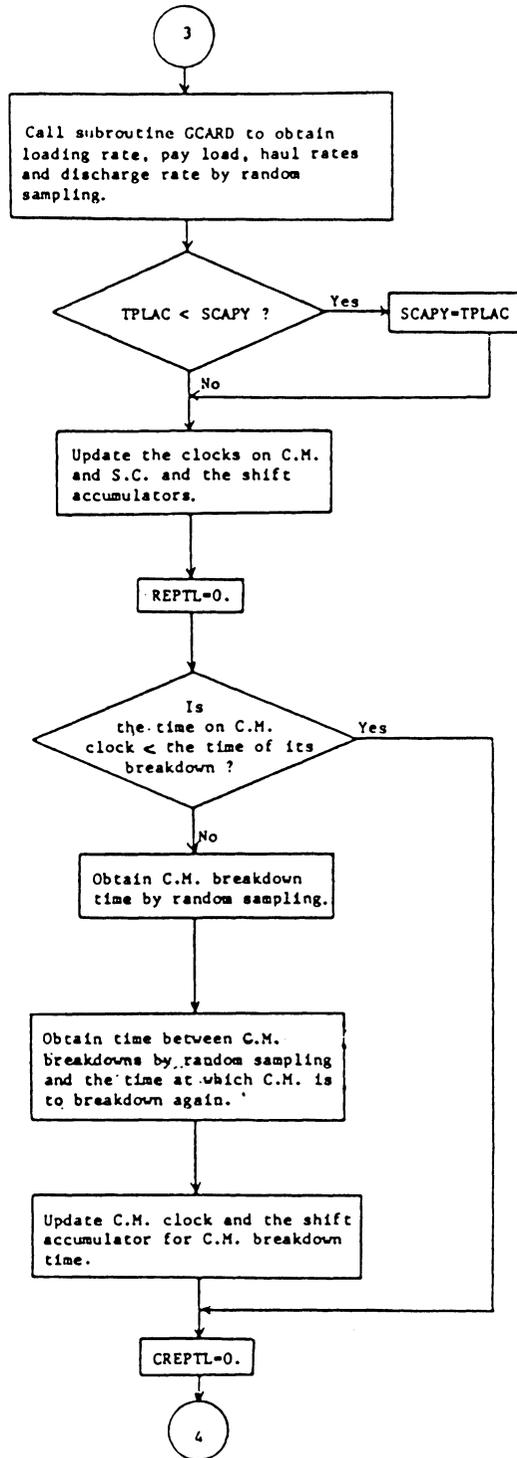
KK2 Same as KK1, but when multiple cuts are
 made.

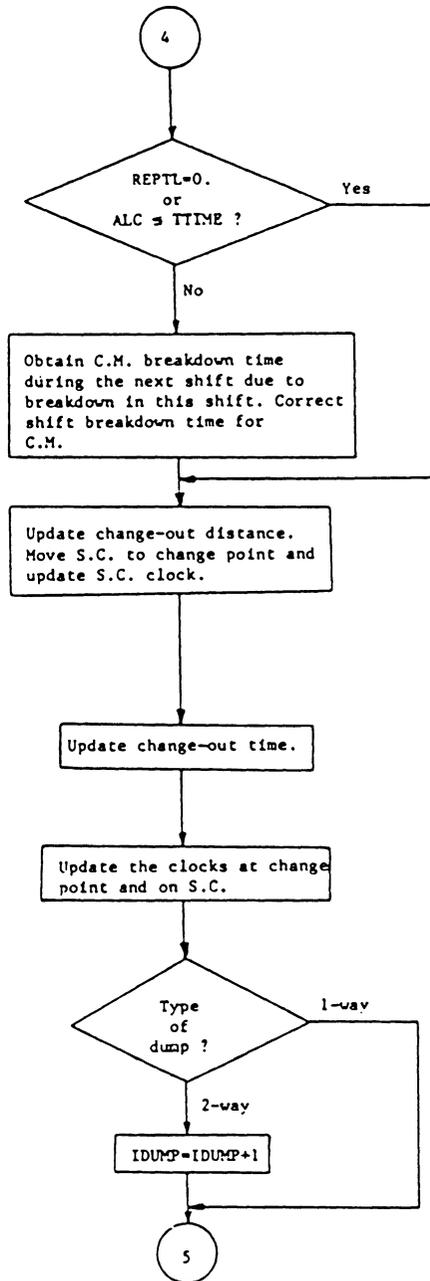
APPENDIX B
FLOWCHART FOR CONSIM

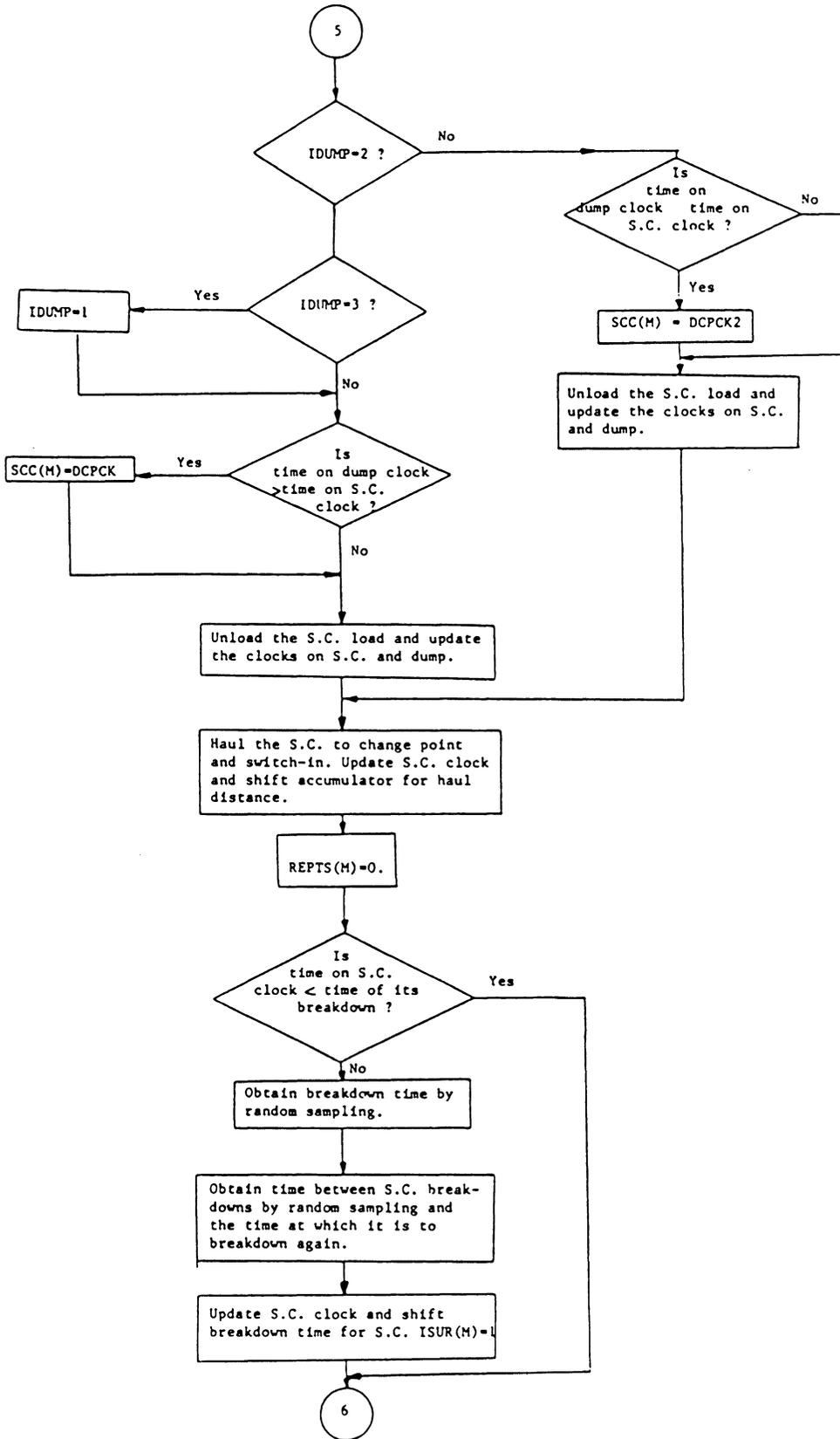
(1) Flowchart for Main Program

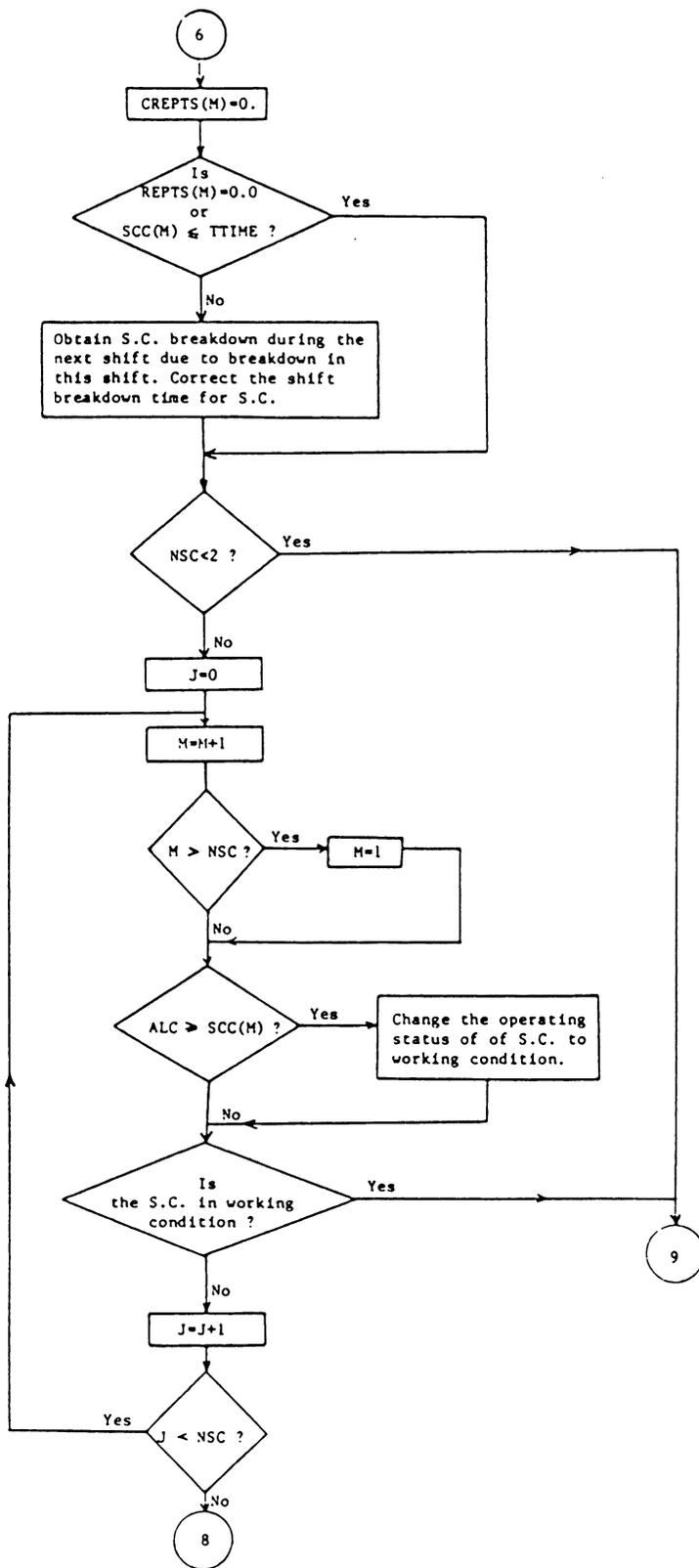


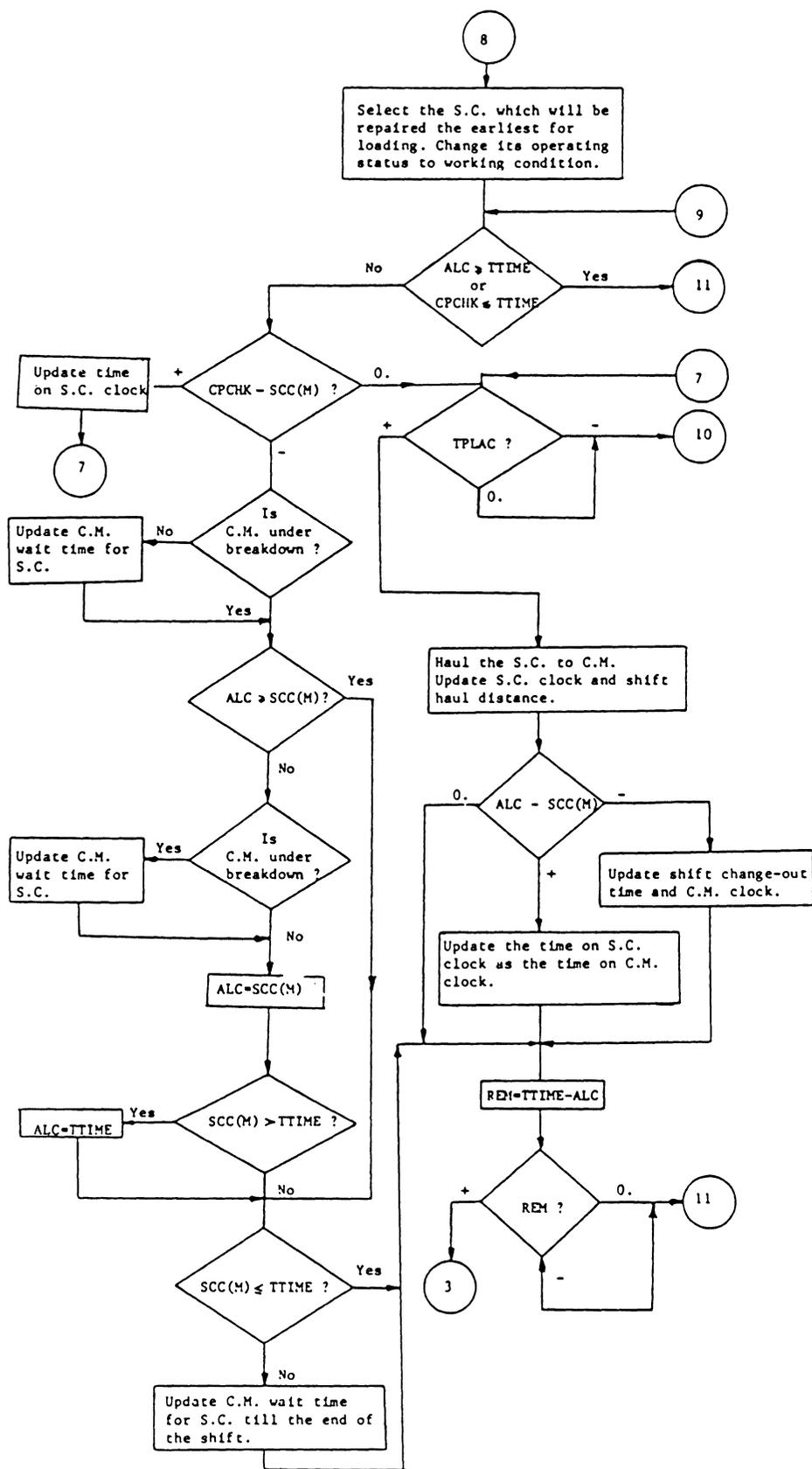


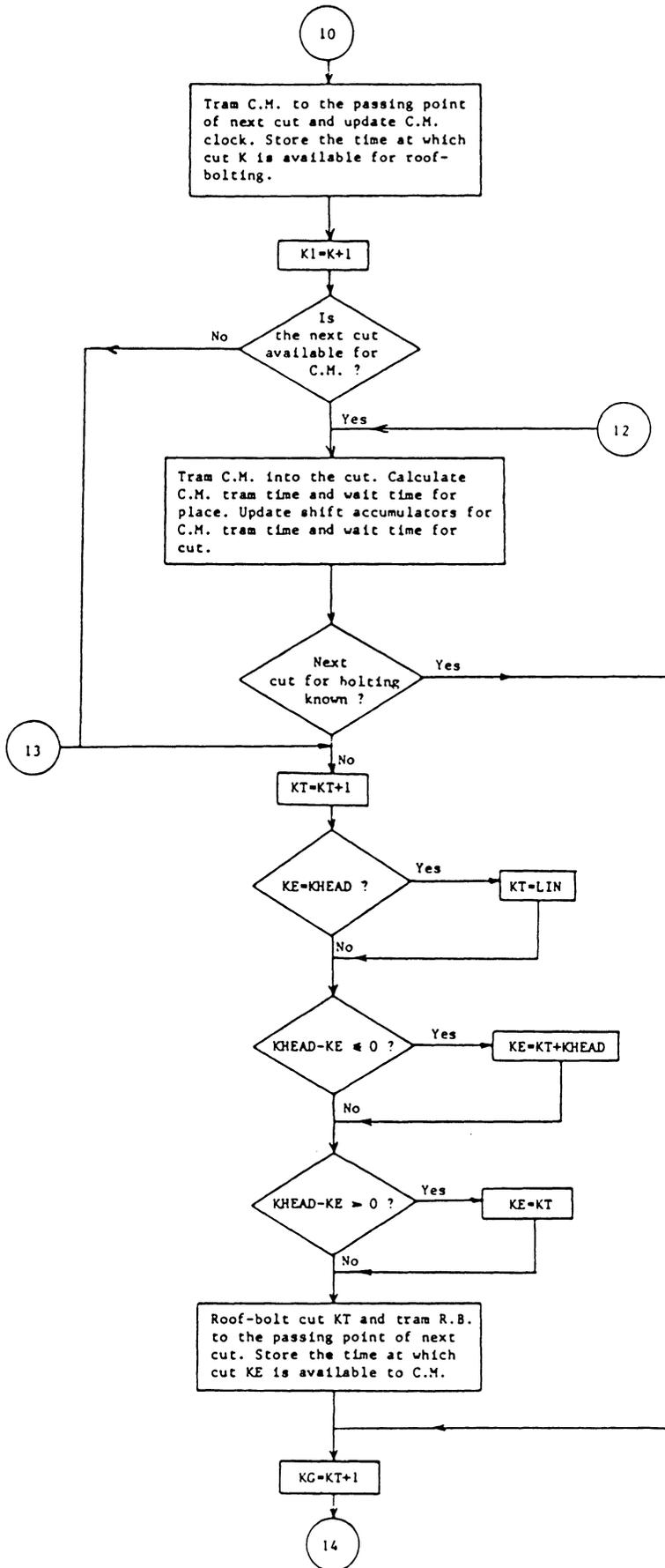


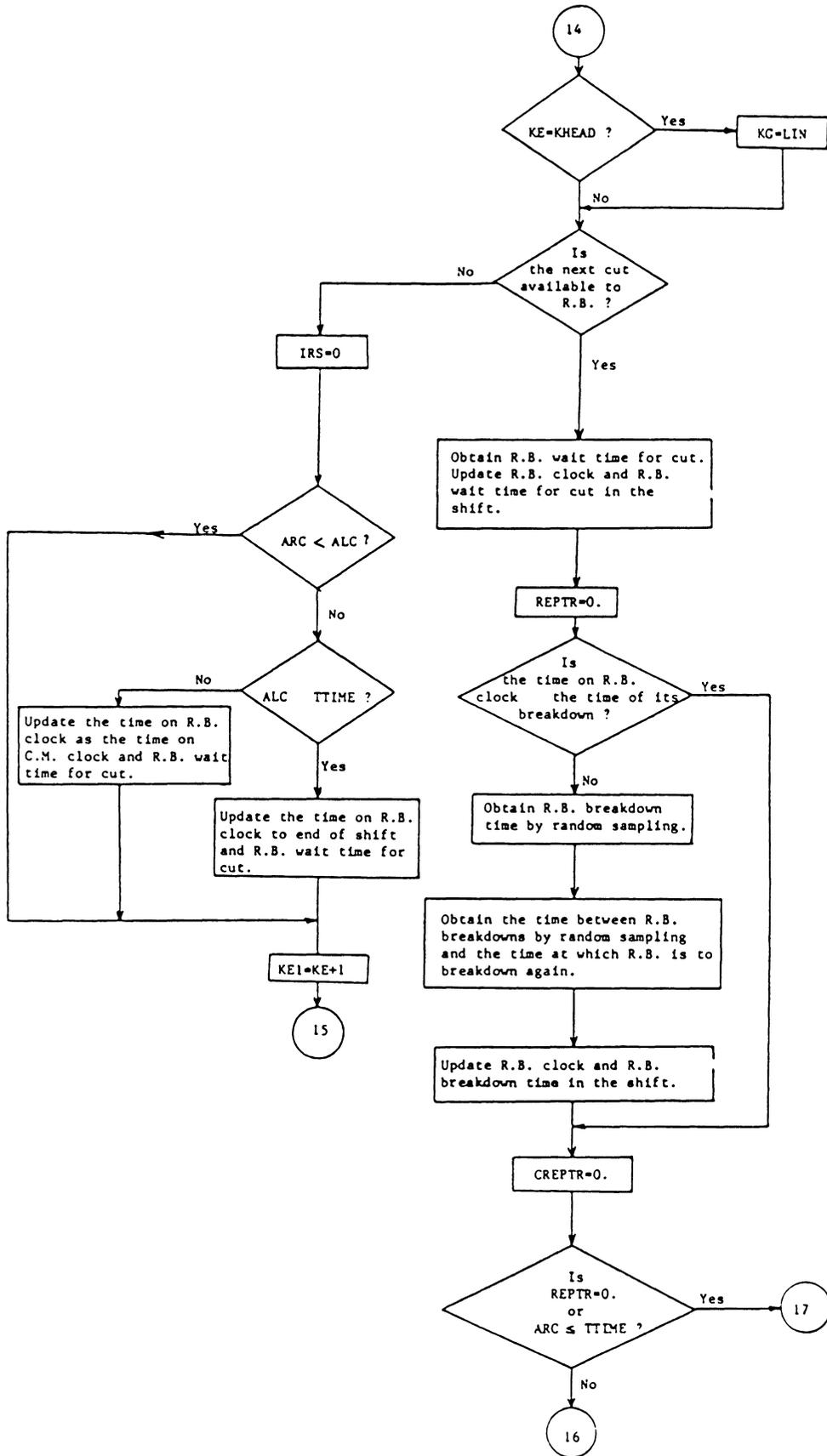


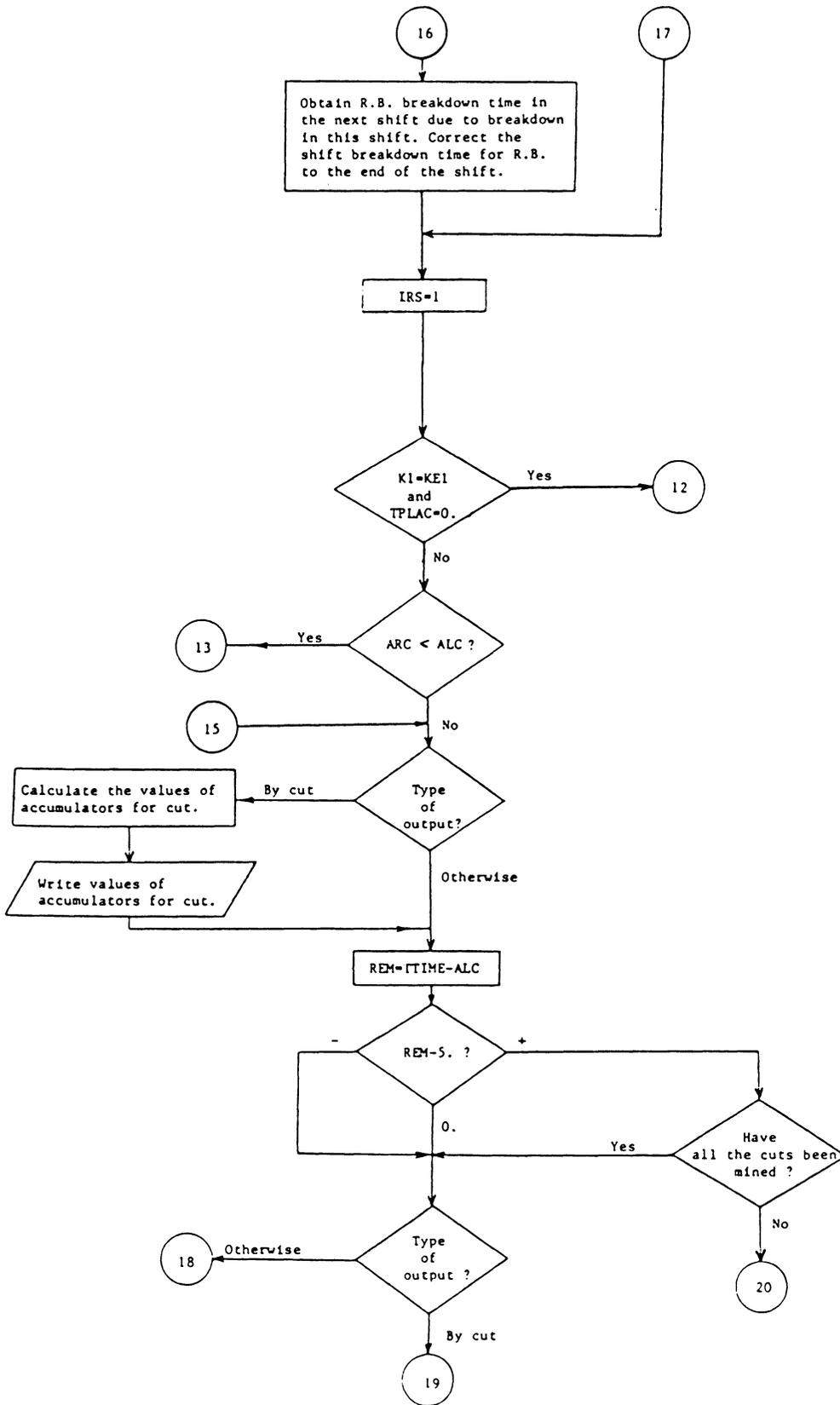


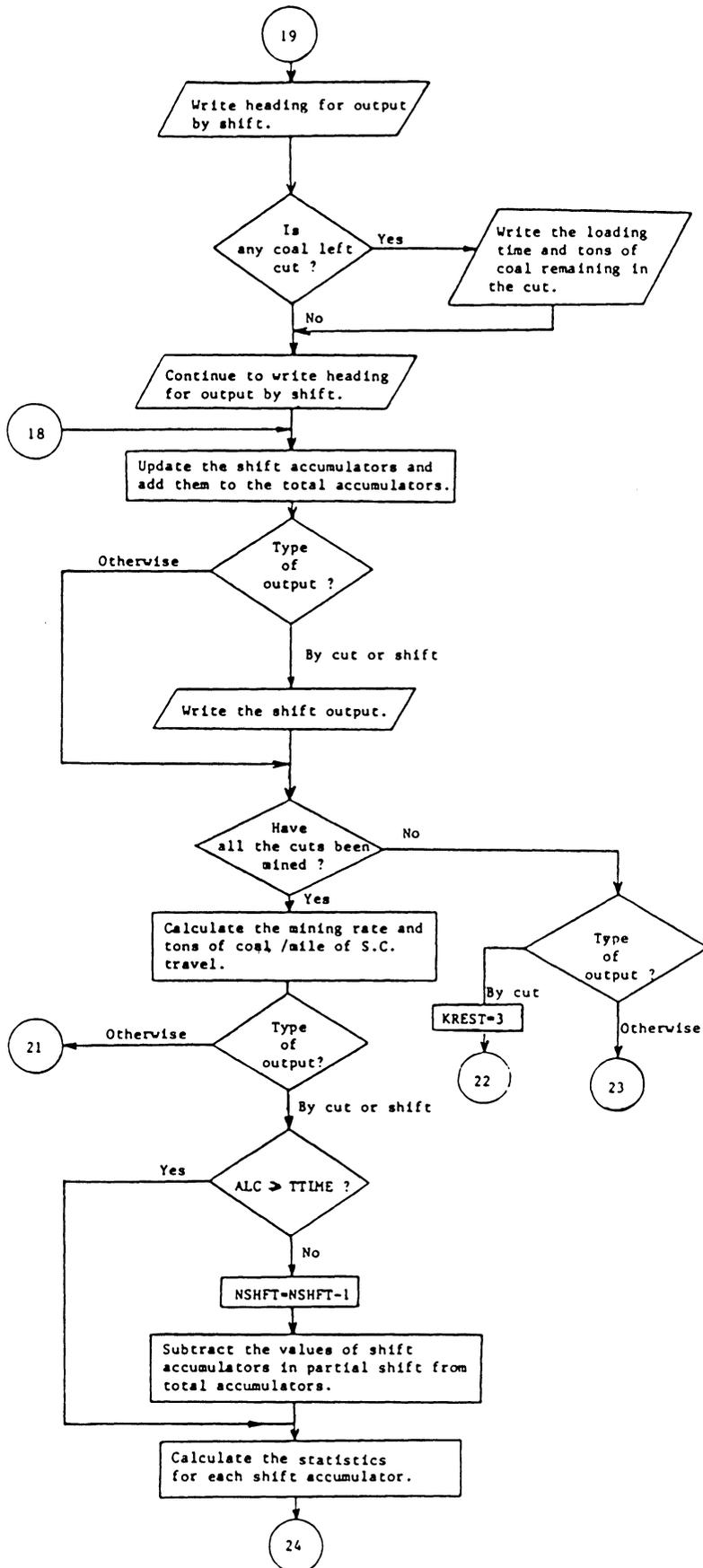


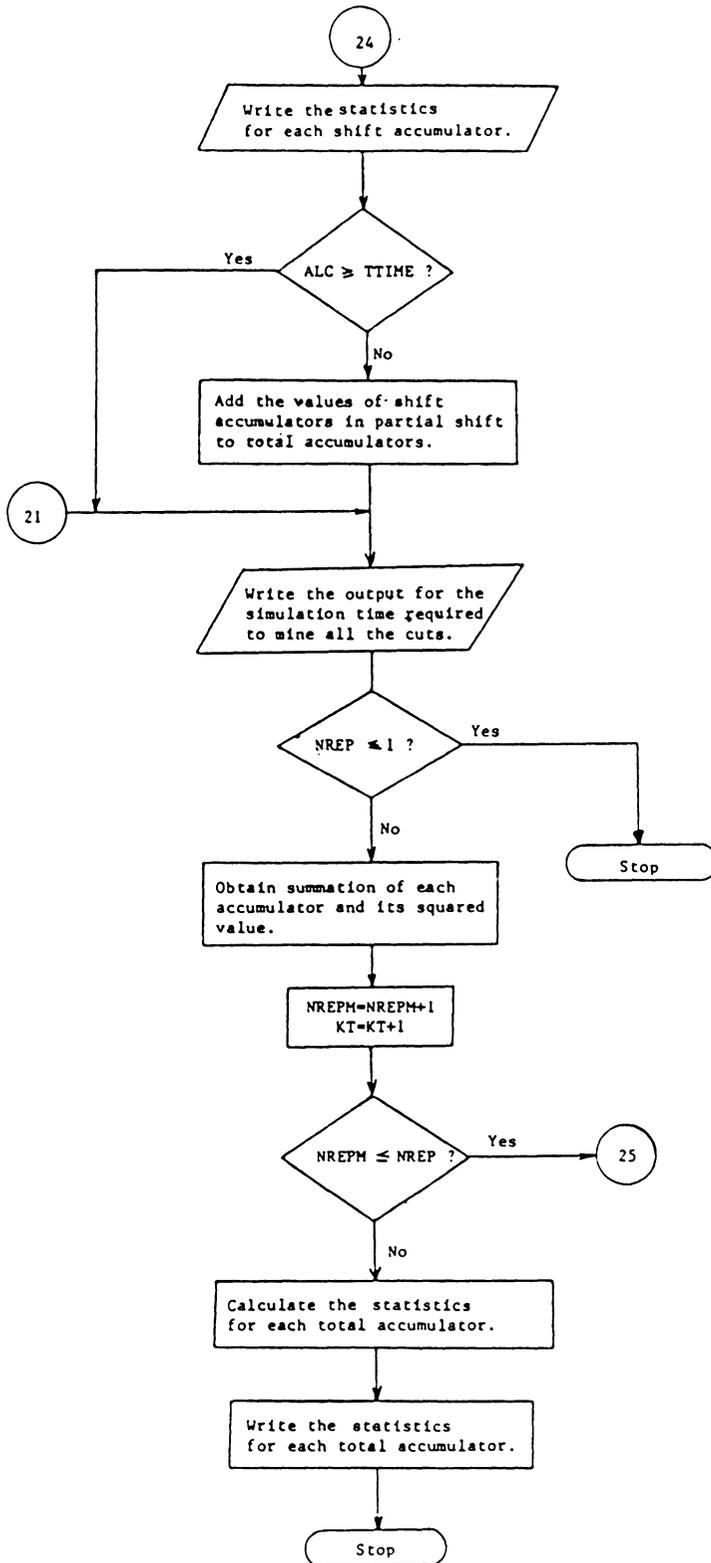




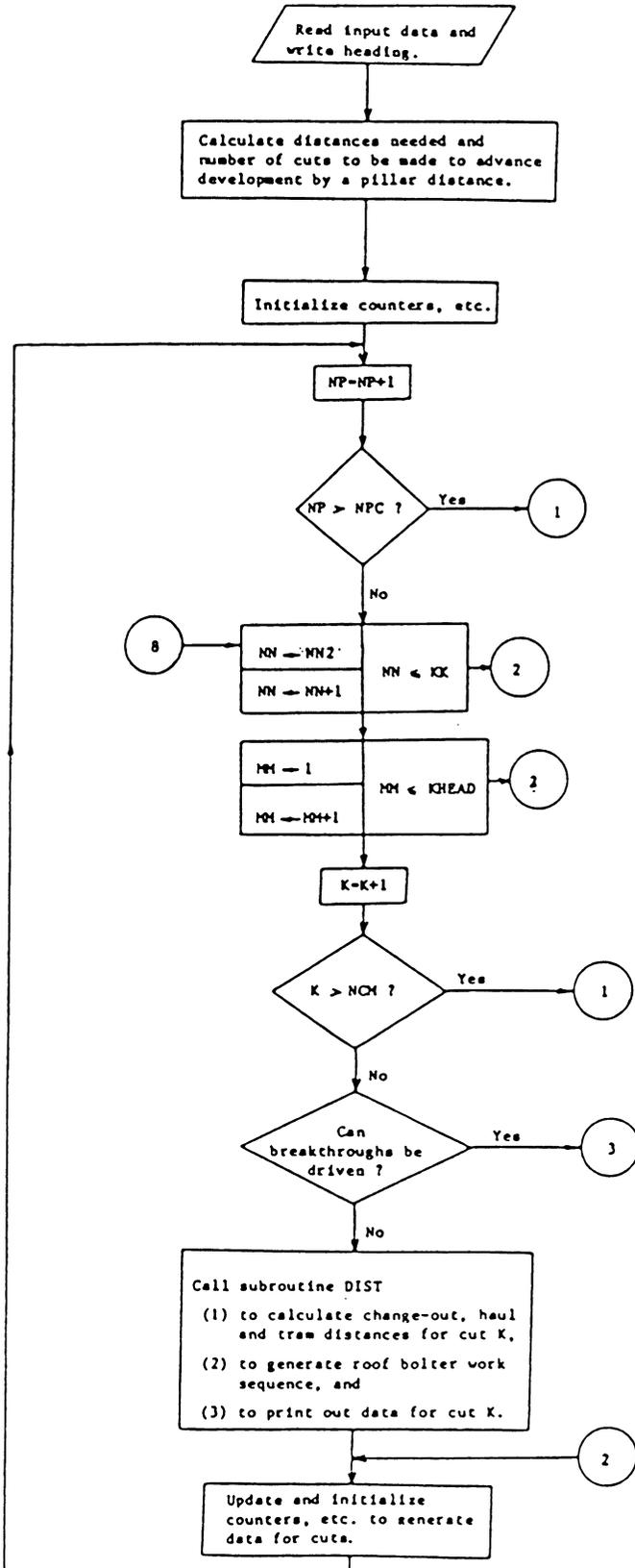


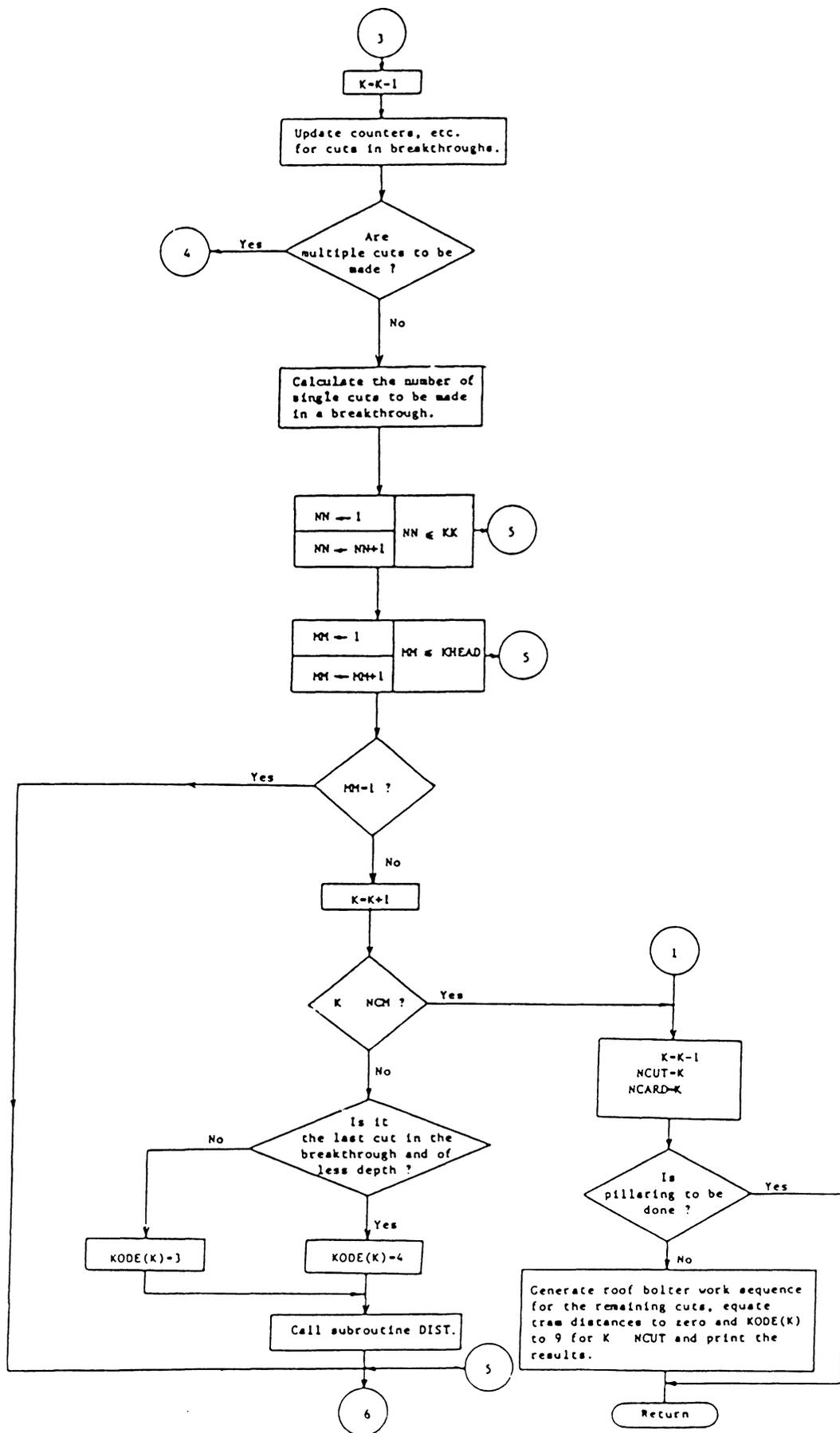


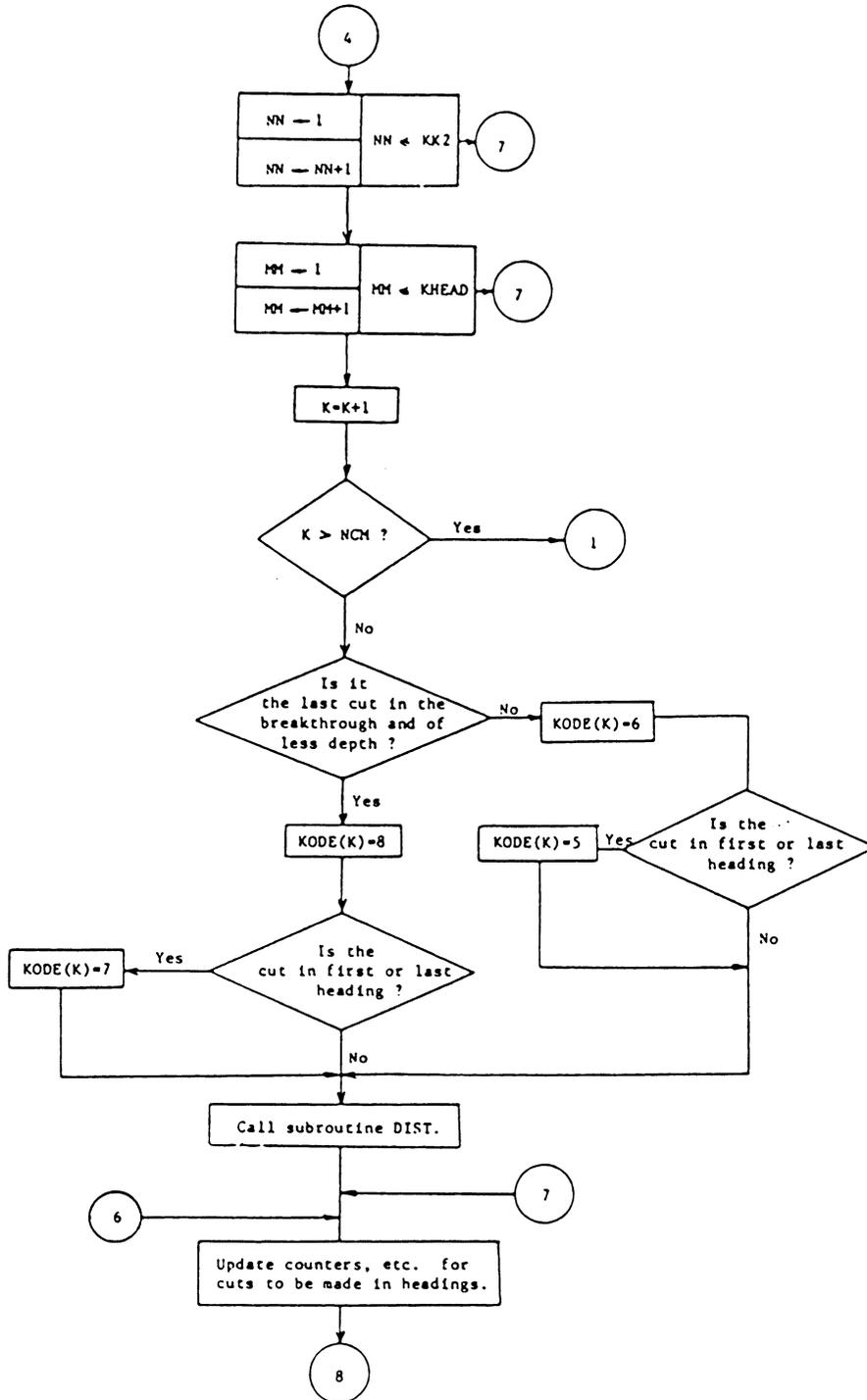




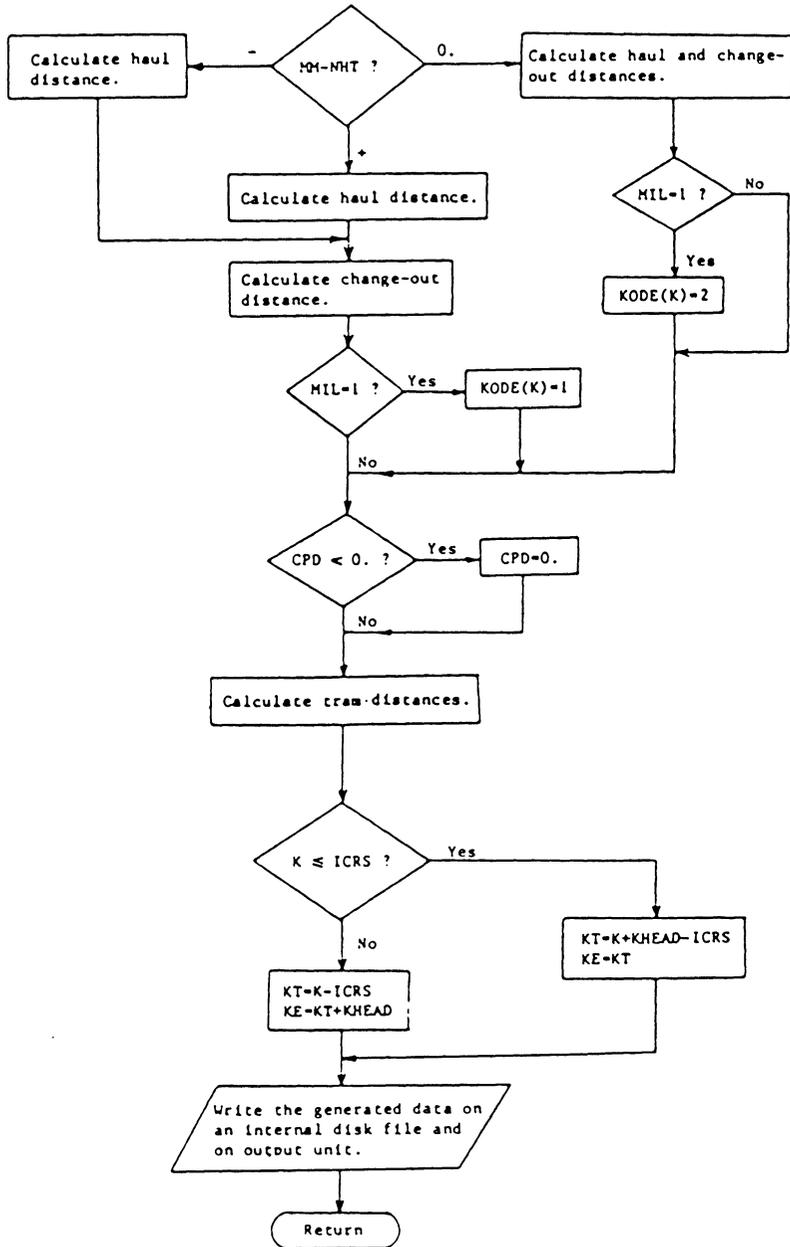
(2) Flowchart for Subroutine GCARD







(3) Flowchart for Subroutine DIST



APPENDIX C
LISTING OF CONSIM

C
C
C

CONSIM, A SIMULATOR FOR CONTINUOUS MINING SYSTEMS.

COMMON DCPD, NCUT, KHEAD, LT1(400), LT2(400), KODE(400)
COMMON/RAND/IX, IY, IZ
COMMON/GEN1/ RLA(25), RA(25), RLB(25), RB(25), RLC(25), RC(25), RLD(25),
+RD(25), RLF(25), RE(25), RLG(25), RG(25), RLH(25), RH(25), VL1, VL2, VE1,
+VF2, DISCH, SCAPY, ALOAD, NA, L
DIMENSION PLACE(400), RNRSUP(30), RMRSUP(30), HT(30), W(30), DTH(30),
+SCC(9), ISUR(9), FALTS(9), SFALTS(9), SREPTS(9), TREPTS(9), CREPTS(9),
+REPTS(9), SP(16), TSP(16), TTSP(16), SST(16), SS(16), SP1(16),
+XM2(9), XM5(9)
EQUIVALENCE(TLOAD, TSP(1)), (TCOT, TSP(2)), (TWL, TSP(3)), (TWP, TSP(4)),
+(TTON, TSP(5)), (TTPM, TSP(6)), (TWRS, TSP(7)), (TREP TL, TSP(8)), (TREP TR,
+TSP(9)), (THD, TSP(10)), (TCYCLE, TSP(11)), (RATE, TSP(14)), (TPMIL, TSP(1
+5)), (SLOAD, SP(1)), (SICOT, SP(2)), (SWL, SP(3)), (SWP, SP(4)), (STON, SP(5
+)), (STPM, SP(6)), (SWRS, SP(7)), (SREPTL, SP(8)), (SREP TR, SP(9)), (SHD, SP
+(10))
REWIND 1

C
C
C

READ CARD TYPE A

READ(5, 708)KT, NTSC, NSC, NDUMP, ICBCO, NA, NB, NREP

C
C
C

READ CARD TYPE B

READ(5, 710)SHFT, DENS, TL, TR, SW1, SWO, CL1, CR1

C
C
C

READ CARD TYPE C

READ(5, 738)XM1, XM3, XM4, XM6

C
C
C

READ CARD TYPE D

READ(5, 739)(XM2(1), XM5(1), I=1, NTSC)

C
C
C

READ CARD TYPE E

READ(5, 737)I, IX, IY, IZ

C
C
C

CALL SUBROUTINE GCARD TO GENERATE DATA FOR CUTS MADE
IN DEVELOPMENT

```

C
C      CALL GCARD
C
C      READ CARD TYPE H (IN NA NUMBER OF CARDS) TO DEFINE EMPIRICAL
C      DISTRIBUTIONS FOR LOADING RATE, PAYLOAD, HAUL RATES AND
C      DISCHARGE TIME
C
      DO 30 N=1,NA
30  READ(5,701)RLA(N),RLB(N),RLC(N),RLD(N),RLE(N),RLG(N),RLH(N),
      1RA(N),RB(N),RC(N),RD(N),RE(N),RG(N),RH(N)
C
C      READ CARD TYPE I (IN NB NUMBER OF CARDS) -- ROOF BOLTER
C      CYCLE TIMES AND TRAM FUNCTIONS AND CUT DIMENSIONS
C
      DO 40 N=1,NB
40  READ(5,705)RNRSUP(N),RMRSUP(N),HT(N),W(N),DTH(N)
C
C      INITIALIZE CLOCKS, ACCUMULATORS, ETC. WRITE HEADING
C
      WRITE(6,1)
      NREPM=1
      DO 904 I=1,16
      SSI(I)=0.
904  TISP(I)=0.
1098 WRITE(6,605) NREPM,NREP
      REWIND 1
      KREST=1
      IF(1CBCO)146,151,148
146  KREST=2
153  WRITE(6,3)
      WRITE(6,4)
      GO TO(151,147,125),KREST
151  WRITE(6,6)
      WRITE(6,7)
      GO TO 147
148  WRITE(6,17)
147  DO 45 N=1,400
      45  PLACE(N)=0.
      DO 905 I=1,16
      SS(I)=0.
905  TSP(I)=0.
      IDUMP=1

```

```

K=0
L=1
LIN=1
M=1
KT1=KT
KE1=KT
KT=KT-1
KE=KT
ARC=0.0
ALC=0.0
FALTL=EXPON(XM1)
DO 800 I=1,NSC
SCC(I)=0.
TREPIS(I)=0.
ISUR(I)=0
CREPTS(I)=0.
IF(NTSC.NE.1) GO TO 800
XM2(I)=XM2(I)
XM5(I)=XM5(I)
800 FALIS(I)=EXPON(XM2(M))
FALIR=EXPON(XM3)
IRS=1
NSHIFT=0
TTIME=0.
TTRAM=0.
TPLAC=0.
REM=0.
CREPTL=0.
CREPIR=0.
CIRAM1=0.
WPI=0.
WRS1=0.
TARC=0.

C
C      INITIALIZE SHIFT ACCUMULATORS, ETC.
C
125 SLC=ALC
IF(CREPTL.GT.0) SLC=TTIME
IF(ARC.LT.TTIME) ARC=TTIME
IF(TARC.GT.0) ARC=ARC+TARC
DO 810 I=1,NSC
IF(SCC(I).LT.TTIME) SCC(I)=TTIME

```

```

810 SREPTS(1)=CREPTS(1)
    TIME=TIME+SHFT
    STRAM=0.
    SWRS2=0.
    DO 910 I=1,10
910 SP(1)=0.
    IF(CIRAM1.GT.0.0) STRAM=STRAM+CTRAM1
    IF(WP1.GT.0.0) SWP=SWP+WP1
    IF(ALC.GT.TIME.AND.ALC.GT.ARC) SWRS=ALC-ARC
    IF(WRS1.GT.0.0) SWRS=SWRS+WRS1
    SREPTL=CREPTL
    SREPTR=CREPTR
    IIRS=0
    IF(IPLAC.GT.0.) GO TO 117
C
C     READ DATA FOR THE NEXT CUT -- HAUL, CHANGE-OUT AND
C     DISCHARGE CHANGE-OUT DISTANCES
C
120 READ(1,75)K,HD,CPD,DCPD
    PTON=HT(KODE(K))*W(KODE(K))*DTH(KODE(K))*DENS
    IPLAC=PTON
    IIRS=1.
C
C     CALCULATE TONS OF COAL IN CUT
C
C     INITIALIZE ACCUMULATORS, ETC. FOR CUT
C
117 SWL2=SWL
    SLOAD2=SLOAD
    STON2=STON
    SHD2=SHD
    SICOT2=SICOT
    ALC2=ALC
    CIRAM=0.
    WP=0.
    IF(IPLAC.EQ.1.E-10) GO TO 400
    IF(ALC.GE.SCC(M)) GO TO 900
    SWL=SWL+SCC(M)-ALC
    ALC=SCC(M)
900 DO 855 I=1,NSC
    IF(SCC(I).LT.ALC) SCC(I)=ALC
855 CONTINUE

```

```

      CPCJK=ALC
      DCPCK=ALC
C
C      LOAD SHUTTLE CAR
C
200 CALL RANDG
   IF (TPLAC.LI.SCAPY) SCAPY=TPLAC
   SCC(M)=SCC(M)+ALOAD
   SLOAD=SLOAD+ALOAD
   STON=STON+SCAPY
   TPLAC=TPLAC-SCAPY
   ALC=ALC+ALOAD
   RFM=TTIME-ALC
C
C      SIMULATE BREAKDOWN OF MINER
C
      REPTL=0.
      IF (ALC.LI.FALIL) GO TO 2060
      REPTL=EXPON(XM4)
      FALIL=FALIL+REPTL+EXPON(XM1)
      SREPTL=SREPTL+REPTL
      ALC=ALC+REPTL
2060 CREPTL=0.
      IF (REPTL.EQ.0.OR.ALC.LE.TTIME) GO TO 2061
      CREPTL=ALC-TTIME
      IF (ALC-REPTL.GT.TTIME) CREPTL=REPTL
      SREPTL=SREPTL-CREPTL.
C
C      HAUL SHUTTLE CAR TO CHANGE POINT
C
2061 CPD=CPD+(1.-TPLAC/PION)*DTH(KODE(K))
      SCC(M)=SCC(M)+VL1*CPD
      IF (REPTL.LI.VL1*CPD) STCOT=STCOT+VL1*CPD-REPTL
      CPCJK=SCC(M)
      IF (ALC.LI.CPCHK) ALC=CPCHK
C
C      HAUL SHUTTLE CAR TO DISCHARGE CHANGE POINT
C
      SCC(M)=SCC(M)+VL2*HD
      IF (NDUMP.EQ.1) GO TO 215
      IDUMP=IDUMP+1
      IF (IDUMP.EQ.2) GO TO 216

```

```

      IF (IDUMP.EQ.3) IDUMP=1
215  IF (DCPCK.GT.SCC(M)) SCC(M)=DCPCK
C
C      HAUL SHUTTLE CAR TO DUMP AND UNLOAD IT
C
      SCC(M)=SCC(M)+(VL2+VE1)*DCPD+DISCH
      DCPCK=SCC(M)
      GO TO 224
216  IF (DCPCK2.GT.SCC(M)) SCC(M)=DCPCK2
      SCC(M)=SCC(M)+(VL2+VE1)*DCPD+DISCH
      DCPCK2=SCC(M)
224  SCC(M)=SCC(M)+VE1*HD+SWI
      SHD=SHD+(HD+DCPD)*2+CPD
C
C      EMPTY CAR BACK AT CHANGE POINT
C      SIMULATE BREAKDOWN OF SHUTTLE CAR
C
      REPTS(M)=0.
      IF (SCC(M).LT.FALIS(M)) GO TO 2248
      REPTS(M)=EXPON(XM5(M))
      FALIS(M)=FALIS(M)+REPTS(M)+EXPON(XM2(M))
      SREPTS(M)=SREPTS(M)+REPTS(M)
      SCC(M)=SCC(M)+REPTS(M)
      ISUR(M)=1
2248  CREPTS(M)=0.
      IF (REPTS(M).EQ.0.OR.SCC(M).LE.TTIME) GO TO 2249
      CREPTS(M)=SCC(M)-TTIME
      IF (SCC(M)-REPTS(M).GT.TTIME) CREPTS(M)=REPTS(M)
      SREPTS(M)=SREPTS(M)-CREPTS(M)
C
C      SELECT THE NEXT SHUTTLE CAR TO BE LOADED.
C
2249  IF (NSC.LT.2) GO TO 228
      J=0
      820  M=M+1
          IF (M.GT.NSC) M=1
          IF (ALC.GE.SCC(M)) ISUR(M)=0
          IF (ISUR(M).EQ.0) GO TO 228
          J=J+1
          IF (J.LT.NSC) GO TO 820
          DMIN=1.E+10
          DO 830 I=1,NSC

```

```

      IF(SCC(I).GE.DMIN) GO TO 830
      DMIN=SCC(I)
      M=I
830  CONTINUE
      ISUR(M)=0
C
      UPDATE ACCUMULATORS, ETC.  CHECK FOR AVAILABLE SHIFT TIME
C
228  IF(ALC.GE.TTIME.OR.CPCHK.GE.TTIME) GO TO 4000
      IF(CPCHK-SCC(M))229,233,230
229  IF(REPTL.EQ.0.) SWL=SWL+SCC(M)-CPCHK
      IF(ALC.GE.SCC(M)) GO TO 231
      IF(REPIL.NE.0.) SWL=SWL+SCC(M)-ALC
      ALC=SCC(M)
      IF(SCC(M).GT.TTIME) ALC=TTIME
231  IF(SCC(M).LE.TTIME) GO TO 233
      SWL=SWL-SCC(M)+TTIME
      IF(TPLAC.EQ.0.0) TPLAC=1.E-10
      GO TO 237
230  SCC(M)=CPCHK
C
      HAUL EMPTY CAR TO MINER
C
233  IF(TPLAC) 400,400,2251
2251  SCC(M)=SCC(M)+VE2*CPD+SWO
      SHD=SHD+CPD
      IF(ALC-SCC(M)) 235,237,236
235  SICOT=SICOT+SCC(M)-ALC
      ALC=SCC(M)
      GO TO 237
236  SCC(M)=ALC
C
      CHECK FOR AVAILABLE SHIFT TIME
C
237  REM=TTIME-ALC
238  IF(REM)4000,4000,200
C
      TRAM THE MINER TO THE NEXT CUT
C
400  TPLAC=0.
      ALC=ALC+CL1+TL*(LT1(K)+LT2(K)+DTH(KODE(K)))
      PLACE(K)=ALC-TL*LT1(K)

```

```

      K1=K+1
      IF(K1.EQ.KE1) GO TO 4001
C
C      CALCULATE MINER WAIT TIME FOR PLACE
C
      850 WP=PLACE(K1)-ALC
        IF(PLACE(K1).LT.ALC) WP=0.
        WP1=0.0
        IF(ALC+WP.LE.TTIME) GO TO 851
        WP1=WP
        WP=0.
        IF(ALC.GF.TTIME) GO TO 851
        WP1=ALC+WP1-TTIME
        WP=TTIME-ALC
      851 ALC=ALC+WP+1L*LI2(K1)
        SWP=SWP+WP
        CTRAM=1L*(LT1(K)+LI2(K)+LT2(K1)+DTH(KODE(K)))+CL1
        CTRAM1=0.0
        IF(WP1.LE.0.0) GO TO 853
        CTRAM=CTRAM-1L*LT2(K1)
        ALC=ALC-1L*LI2(K1)
        CTRAM1=1L*LI2(K1)
      853 STRAM=STRAM+CTRAM
      4000 IF(1IRS.EQ.0) GO TO 841
        IF(IRS.EQ.0) GO TO 845
C
C      OBTAIN CUT TO BE ROOF-BOLTED AND CUT MADE AVAILABLE
C
      4001 KI=KT+1
        IF(KE.EQ.KHEAD) KI=LIN
        IF(KHEAD-KE.LE.0) KE=KT+KHEAD
        IF(KHEAD-KE.GT.0) KE=KI
      4209 KRS=KODF(KT)
C
C      ROOF-BOLT AND TRAM THE ROOF BOLTER TO NEXT CUT
C
        ARC=ARC+CR1+TR*(LT1(KT)+LT2(KT)+DTH(KODE(K)))+RNRSUP(KRS)+
        +RMRSUP(KRS)
C
C      CALCULATE ROOF BOLTER WAITING TIME FOR CUT
C
        PLACE(KE)=ARC-TR*LT1(KT)-RMRSUP(KRS)

```

```

4210 KG=KT+1
      IF(KE.EQ.KHEAD) KG=LIN
      IF(KG.EQ.K) GO TO 840
845  TRAR3=LT2(KG)
      WRS=0.0
      IF(PLACE(KG).GT.ARC) WRS=PLACE(KG)-ARC
      WRS1=0.0
      TARC=0.0
      IF(ARC+WRS.LE.TTIME) GO TO 854
      WRS1=WRS
      WRS=0.0
      IF(ARC.GE.TTIME) GO TO 856
      WRS1=ALC+WRS-TTIME
      WRS=TTIME-ARC
856  IF(WRS1.LE.0) GO TO 854
      TARC=TR*TRAR3
      ARC=ARC-TR*TRAR3
854  ARC=ARC+WRS+TR*TRAR3
      SWRS=SWRS+WRS
C
C      SIMULATE BREAKDOWN OF ROOF BOLTER
C
      REPTR=0.
      IF(ARC.LT.FALIR) GO TO 869
      REPTR=EXPON(XM6)
      FALIR=FALIR+REPTR+EXPON(XM3)
      SREPTR=SREPTR+REPTR
      ARC=ARC+REPTR
869  CREPTR=0.
      IF(REPTR.EQ.0.OR.ARC.LE.TTIME) GO TO 870
      CREPTR=ARC-TTIME
      IF(ARC-REPTR.GT.TTIME) CREPTR=REPTR
      SREPTR=SREPTR-CREPTR
870  IRS=1
      IF(K1.EQ.KE1.AND.1PLAC.EQ.0.0) GO TO 850
      GO TO 835
840  IRS=0
C
C      UPDATE ROOF BOLTER CLOCK
C
841  IF(ARC.GE.ALC) GO TO 4239
      IF(ALC.GT.TTIME) GO TO 4238

```

```

      SWRS=SWRS+ALC-ARC
      ARC=ALC
      GO TO 4239
4238 SWRS=SWRS+TTIME-ARC
      ARC=ALC
      GO TO 4239
      835 IF(ARC.LT.ALC) GO TO 4001
4239 KE1=KE+1
      IF(ICBCO)4240,154,154
C
C      CALCUIATE VALUES OF OUTPUT VARIABLES FOR CUT
C
4240 CYCLE=ALC-ALC2-CREPTL
      CLOAD=SLOAD-SLOAD2
      CCOT=STCOT1-STCOT2
      WL=SWL-SWL2
      CHD=(SHD-SHD2)/5280.
      CTON=STON-STON2
      CTPM=CTON/CYCLE
      CWRS=SWRS-SWRS2
      SWRS2=SWRS
C
C      WRITE OUTPUT FOR CUT
C
      WRITE(6,5) K,CYCLE,CLOAD,CCOT,WL,WP,CTRAM,CHD,ALC,CTON,CTPM,KE,PLA
      +CE(KE),KT,ARC
C
C      IF TIME IS AVAILABLE BEGIN MINING NEXT CUT
C
      154 REM=TTIME-ALC
      IF(REM-5.0)648,648,425
425 IF(K.GE.NCUT) GO TO 648
      GO TO 120
C
C      WRITE OUTPUT FOR A PARTIAL CUT
C
648 IF(ICBCO.GE.0) GO TO 650
      WRITE(6,6)
      IF(TPLAC.GT.0.) WRITE(6,9)CLOAD,TPLAC
C
C      UPDATE TOTAL ACCUMULATORS, ETC.
C
      WRITE SHIFT OUTPUT

```

```

C
WRITE(6,7)
650 SLC=ALC-SLC
C IF(CREPTL.GT.0.) SLC=SHFT
DO 860 I=1,NSC
860 TREPTS(I)=TREPTS(I)+SREPTS(I)
NSHFT=NSHFT+1
STPM=STON/SLC
SHD=SHD/5280.
DO 920 I=1,10
TSP(I)=TSP(I)+SP(I)
920 SS(I)=SS(I)+SP(I)**2
TTRAM=TTRAM+STRAM
IF(ICBCO.GT.0.) GO TO 6755
WRITE(6,8) NSHFT,SLC,SLOAD,STCOT,SWL,SWP,STRAM,SREPTL,SHD,STON,STP
IM,K,SWRS,SREPTR,KT
6755 IF(K.GE.NCUT.AND.TPLAC.EQ.0.0) GO TO 666
IF(ICBCO)665,125,125
665 KREST=3
GO TO 153

C
C WRITE THE OUTPUT OVER SIMULATION TIME, STATISTICS
C FOR SHIFT OUTPUT AND THE OUTPUT OVER SIMULATION TIME.
C
666 RATE=TION/ALC
TPMIL=TION/THD
IF(ICBCO.GT.0) GO TO 939
IF(ALC.GE.TTIME) GO TO 936
NSHFT=NSHFT-1
IF(NSHFT.EQ.1) GO TO 941
DO 937 I=1,10
SS(I)=SS(I)-SP(I)**2
937 TSP(I)=TSP(I)-SP(I)
936 DO 940 I=1,10
SS(I)=(SS(I)-ISP(I)**2/FLOAT(NSHFT))/FLOAT(NSHFT-1)
IF(SS(I).LT.0.0) SS(I)=0.
SS(I)=SQRT(SS(I))
940 SP1(I)=TSP(I)/FLOAT(NSHFT)
WRITE(6,14) (SP1(I),I=1,10)
WRITE(6,16) (SS(I),I=1,10)
IF(ALC.GE.TTIME) GO TO 941
DO 938 I=1,10

```

```

938 TSP(1)=TSP(1)+SP(1)
941 CONTINUE
    WRITE(6,17)
939 WRITE(6,18)ALC, ILOAD, TCOT, TWL, TWP, TTRAM, TREPTL, THD, TTON, RATE, TWRS,
    +TREPTR, ARC, TPMIL
    IF(NREP.LE.1) STOP
    TSP(16)=TTRAM
    TSP(13)=ALC
    TSP(12)=ARC
    DO 950 I=1,16
    SST(1)=SST(1)+TSP(1)**2
950 TTSP(1)=TTSP(1)+TSP(1)
    NREPM=NREPM+1
    KT=KT+1

C
C     CHECK IF MORE RUNS TO BE MADE
C
C     IF(NREPM.LE.NREP) GO TO 1098

C
C     CALCULATE AND WRITE STATISTICS FOR OUTPUT OVER SIMULATION
C     TIME
C
    DO 960 I=1,16
    SSI(1)=(SST(1)-TTSP(1)**2/FLOAT(NREP))/FLOAT(NREP-1)
    IF(SSI(1).LT.0.0) SSI(1)=0.
    SSI(1)=SQRT(SSI(1))
960 TTSP(1)=TTSP(1)/FLOAT(NREP)
    WRITE(6,19)TTSP(13), (TTSP(1), I=1,4), TTSP(16), TTSP(8), TTSP(10), TTSP
    +(5), TTSP(14), TTSP(7), TTSP(9), TTSP(12), TTSP(15)
    WRITE(6,20)SSI(13), (SSI(1), I=1,4), SSI(8), SSI(10), SSI(14), SSI(7),
    +SSI(9), SSI(12), SSI(15)

C
C     FORMAT STATEMENTS
C
701 FORMAT(2F5.2,4F5.4,F5.2,1X,7F5.3)
705 FORMAT(5I6.2)
708 FORMAT(8I5)
710 FORMAT(F5.1,F5.3,2F5.4,4F5.2)
737 FORMAT(4I10)
738 FORMAT(4(F10.2,2X))
739 FORMAT(2(F10.2,2X))
605 FORMAT(1H1,20X,'RUN ',I4,' OF ',I4,'////')

```

```

1 FORMAT(1H1,35X,'ANALYSIS OF CONTINUOUS MINING SYSTEM',/35X,' *****
+*****',///42X,'ALL TIMES IN MINUTES',/)
3 FORMAT(' SYSTEM PERFORMANCE BY CUT',/' *****')
4 FORMAT('/ CUT ', ' CYCLE ', ' LOAD', 3X, 'CHANGE', ' WAIT- ', ' WAIT- '
+ ' TRAM ', ' HAUL ', ' TIME', 4X, ' TONS', 3X, ' T/M', 2X, ' CUT MADE AVAIL '
+ ' RB', 2X, ' TIME', / ' NO. ', 15X, ' OUT', 4X, ' CAR', 4X, ' COAL', 9X, ' DIST', 3
+X, ' (CM)', 17X, ' NO. ', 5X, ' AT', 5X, ' AT', 2X, ' RB')
5 FORMAT(/14,5F7.1,F5.1,F7.1,F9.1,F7.1,F5.2,15,F9.1,15,F9.1)
6 FORMAT(///' SYSTEM PERFORMANCE BY SHIFT',/' *****
1*****',/)
7 FORMAT(' SHIFT ', ' TIME ', ' LOAD ', ' CHANGE ', ' WAIT- ', ' WAIT- ',
+ ' TRAM ', ' REPAIR', 3X, ' HAUL', 3X, ' TONS', 3X, ' T/M ', ' CM ', ' WAIT- '
+ ' REPAIR', ' RB', / ' NO. ', 15X, ' OUT', 5X, ' CAR', 4X, ' COAL', 9X, ' (CM)
+ ', 3X, ' DIST', 15X, ' AT', 4X, ' RB', 5X, ' RB', 6X, ' AT ', /)
8 FORMAT(/13,1X,F7.1,1X,F6.1,1X,F6.1,5F7.1,1X,F7.1,F5.2,14,2F8.1,15,
+ /)
9 FORMAT(' PARTIAL CUT',/' LOAD ', ' TONS REM.', /2F7.1, /)
14 FORMAT(///' OVERALL SYSTEM PERFORMANCE BY SHIFT',/' *****
+*****',/1X, ' LOAD', 4X, ' CHANGE OUT', 2X, ' WAIT-CAR', 3X
+ ' WAIT-COAL', 2X, ' TONS', 3X, ' TONS/MIN', 2X, ' WAIT(RB)', 2X, ' REPAIR(CM)'
+ , 2X, ' REPAIR(RB)', 2X, ' HAUL DIST', /5(F7.1,3X),F7.2
+ , 3X,4(F7.1,3X), /)
16 FORMAT(' SAMPLE STANDARD DEVIATION', /10(F9.1,1X), /)
17 FORMAT(///' SYSTEM PERFORMANCE OVER SIMULATION TIME',/' *****
+*****',/' TIME', 6X, ' LOAD', 4X, ' CHANGE', 4X, '
+ WAIT-', 3X, ' WAIT-', 3X, ' TRAM', 4X, ' REPAIR', 4X, ' HAUL', 5X, ' TONS', 5X, ' T/
+ M', 5X, ' WAIT-', 4X, ' REPAIR', 4X, ' TIME', 5X, ' TONS ', /19X, ' OUT', 7X, ' CAR
+ ', 5X, ' COAL', 12X, ' (CM)', 6X, ' DIST', 22X, ' RB', 7X, ' RB', 8X, ' RB ', 6X, ' /MI
+ LE', /)
18 FORMAT(7(F7.1,2X),F6.1,3X,F7.1,2X,F5.2,2X,4(F7.1,2X), /)
19 FORMAT(' SAMPLE MEAN', /7(F7.1,2X),F6.1,3X,F7.1,2X,F5.2,2X,3(F7.1,
+ 2X),F7.1, /)
20 FORMAT(' SAMPLE STANDARD DEVIATION', /4(F7.1,2X),F7.1,8X,2(F7.1,2
+ X),6X,F9.2,2X,4(1X,F8.1))
75 FORMAT(14,3F4.0)
STOP
END

```

```

C
C      SUBROUTINE TO OBTAIN RANDOM VARIATES FROM
C      EMPIRICAL DISTRIBUTIONS
C
SUBROUTINE RANDG

```

```

COMMON/GEN1/ RLA(25), RA(25), RLB(25), RB(25), RLC(25), RC(25), RLD(25),
+RD(25), RLE(25), RE(25), RLG(25), RG(25), RLH(25), RH(25), VL1, VL2, VE1,
+VF2, DISCH, SCAPY, ALOAD, NA, L
NVAR=1
518 U=RANDOM(L)
DO 516 N=2, NA
GO TO(501,503,505,507,509,511,513,517), NVAR
C
C      LOADING RATE
C
501 IF(RA(N)-U) 516,502,502
502 ALOAD=RLA(N-1)+(U-RA(N-1))*(RLA(N)-RLA(N-1))/(RA(N)-RA(N-1))
GO TO 515
C
C      PAYLOAD
C
503 IF(RB(N)-U) 516,504,504
504 SCAPY=RLB(N-1)+(U-RB(N-1))*(RLB(N)-RLB(N-1))/(RB(N)-RB(N-1))
GO TO 515
C
C      HAUL RATE -- MINER TO CHANGE POINT
C
505 IF(RC(N)-U) 516,506,506
506 VL1=RLC(N-1)+(U-RC(N-1))*(RLC(N)-RLC(N-1))/(RC(N)-RC(N-1))
GO TO 515
C
C      HAUL RATE -- CHANGE POINT TO DUMP
C
507 IF(RD(N)-U) 516,508,508
508 VL2=RLD(N-1)+(U-RD(N-1))*(RLD(N)-RLD(N-1))/(RD(N)-RD(N-1))
GO TO 515
C
C      HAUL RATE -- DUMP TO CHANGE POINT
C
509 IF(RE(N)-U) 516,510,510
510 VE1=RLE(N-1)+(U-RE(N-1))*(RLE(N)-RLE(N-1))/(RE(N)-RE(N-1))
GO TO 515
C
C      HAUL RATE -- CHANGE POINT TO MINER
C
511 IF(RG(N)-U) 516,512,512
512 VF2=RLG(N-1)+(U-RG(N-1))*(RLG(N)-RLG(N-1))/(RG(N)-RG(N-1))

```

```

      GO TO 515
C
C      DISCHARGE TIME
C
513 IF(RH(N)-U) 516,514,514
514 DISCH=RLH(N-1)+(U-RH(N-1))*(RLH(N)-RLH(N-1))/(RH(N)-RH(N-1))
515 NVAR=NVAR+1
      GO TO 518
516 CONTINUE
517 RETURN
      END
C
C      FUNCTION TO GENERATE EXPONENTIAL RANDOM VARIATES.
C
      FUNCTION EXPON(XM)
      EXPON=-XM*ALOG(RANDOM(L))
      RETURN
      END
C
C      FUNCTION TO GENERATE U(0,1) RANDOM NUMBER SEQUENCE.
C
      FUNCTION RANDOM(L)
      COMMON/RAND/IX,IY,IZ
      IX=171*MOD(IX,177)-2*(IX/177)
      IY=172*MOD(IY,176)-35*(IY/176)
      IZ=170*MOD(IZ,178)-63*(IZ/178)
      IF(IX.LT.0) IX=IX+30269
      IF(IY.LT.0) IY=IY+30307
      IF(IZ.LT.0) IZ=IZ+30323
      RANDOM=AMOD(FLOAT(IX) / 30269.0 + FLOAT(IY) / 30307.0 + FLOAT(IZ)
+ / 30323.0, 1.0)
      RETURN
      END
C
C      SUBROUTINE TO GENERATE DATA FOR CUTS MADE IN DEVELOPMENT.
C
      SUBROUTINE GCARD
      COMMON DCPD,NCUT,KHEAD,LT1(400),LT2(400),KODE(400)
      COMMON/GEN2/W(5),MULT1,NHT,WPI1,WHP1L,SCL,ALM,DTH,TLT2,TD1,SDIST,
+DIST1,DIST2,DIST3,KK2,KT,NPC,LPC,ICRS,K,J,KIL,NN,MM,MIL
C
C      READ CARD TYPE F

```

```

C      READ(5,10) (W(I),I=1,3),DTH,WHPIL,WPIL,ALM,SCL,SDIST,DCPD
C
C      READ CARD TYPE G
C
C      READ(5,19) NCM,MULTI,KHEAD,NIIT,KT,NPC,LPC
C
C      WRITE HEADING. INITIALIZE VARIABLES
C
C      WRITE(6,73)
C      WRITE(6,74)
C      ICRS=KHEAD-KI+1
C      KIL=0
C      K=0
C      NP=0
C      DIST1=WHPIL+W(3)
C      DIST2=DIST1-SCL
C      DIST3=WPIL+W(1)
C      KK=DIST1/DTH
C      RK=KK
C      IF(RK.LT.DIST1/DTH) KK=KK+1
56  J=0
C      NP=NP+1
C      I=1
C      IF(NP.GT.NPC) GO TO 55
C      IF(LPC.EQ.0.) I=NP
C      NN2=1
44  M11=1
C      LL12=0.
C      TD1=0.
C      KK2=0
C      DO 20 NN=NN2, KK
C      DO 20 MM=1, KHEAD
C
C      MAKE CUTS IN HEADINGS.
C
C      K=K+1
C      IF(K.GT.NCM) GO TO 55
C
C      CHECK IF CUTS CAN BE MADE IN BREAKTHROUGHS
C
C      IF(SDIST+(NN-1)*DTH-J*DIST1.GE.DIST1+W(3)/2.) GO TO 21

```

```

C
C      CALL SUBROUTINE DIST TO CALCULATE DISTANCES AND ROOF
C      BOLTER WORK SEQUENCE
C
      CALL DIST
20  CONTINUE
      IF(LPC.EQ.0) KIL=KIL+1
      SDIST=SDIST+KK*DTH-DIST1
      GO TO 56
21  SDIST2=SDIST
      NN2=NN
      SDISI=0.
      K=K-1
      TL12=DIST1
      ID1=DIST1+ALM
      IF(MULT1.GT.1) GO TO 41
C
C      MAKE SINGLE CUTS IN BREAKTHROUGHS.
C
      KK1=WPIL/DTH
      RK1=KK1
      IF(RK1.LT.WPIL/DTH) KK1=KK1+1
      M11=2
      DO 45 NN=1, KK1
      DO 45 MM=1, KHEAD
      IF(MM.EQ.1) GO TO 45
      K=K+1
      IF(K.GT.NCM) GO TO 55
      IF(NN.LT.KK1.AND.RK1.NE.FLOAT(KK1)) GO TO 50
C
C      CODE FOR LAST CUT OF SMALLER DEPTH
C
51  KODE(K)=4
      GO TO 46
50  KODE(K)=3
46  CALL DIST
45  CONTINUE
      GO TO 62
C
C      MAKE MULTIPLE CUTS IN BREAKTHROUGHS.
C
41  KK2=WPIL/(2.*DTH)

```

```

RK2=KK2
IF(RK2.LT.WPIL/(2.*DTH)) KK2=KK2+1
MIL=3
DO 61 NN=1, KK2
DO 61 MM=1, KHEAD
K=K+1
IF(K.GT.NCM) GO TO 55
IF(NN.LT.KK2.AND.RK2.NE.FLOAT(KK2)) GO TO 320
KODE(K)=8
C
C      CODE FOR CUT IN FIRST OR LAST HEADING
C
      IF(MM.EQ.1.OR.MM.EQ.KHEAD) KODE(K)=7
      GO TO 61
C
C      CODE FOR LAST CUT OF SMALLER DEPTH
C
320 KODE(K)=6
C
C      CODE FOR LAST CUT OF SMALLER DEPTH IN FIRST OR LAST HEADING
C
      IF(MM.EQ.1.OR.MM.EQ.KHEAD) KODE(K)=5
61 CALL DIST
C
C      UPDATE VARIABLES FOR CUTS IN HEADINGS
C
62 KIL=KIL+1
   IF(LPC.NE.0) KIL=0
   J=J+1
   IF(MULTI.GT.1) NN2=NN2+1
   SDIST=SDIST2
   GO TO 44
55 CONTINUE
   K=K-1
   NCUT=K
C
C      GENERATE ROOF BOLTER OPERATING SEQUENCE FOR THE REMAINING
C      CUTS.GENERATE DATA FOR DUMMY CUTS
C
      IICRS=0
86 IICRS=IICRS+1
   KI=KI+1

```

```

      KE=KT+KHEAD
      K=K+1
      LT1(K)=0
      LT2(K)=0
      KODE(K)=9
      WRITE(6,85)K,LT1(K),LT2(K),KODE(K),KT,KE
      IF(11CRS.LT.1CRS) GO TO 86
85  FORMAT(14,14X,316,4X,213)
10  FORMAT(10F5.1)
19  FORMAT(7I5)
73  FORMAT(1H1,42X,'DATA GENERATED BY SUBROUTINE GCARD',///)
74  FORMAT(3X,'K',2X,'HD ', ' CPD ', ' DCPD', ' LT1(K)', ' LT2(K) ',
+ 'KODE(K)', ' KT ', 'KE',//)
      RETURN
      END
C
C      SUBROUTINE TO GENERATE DISTANCES ROOF BOLTER WORK SEQUENCE
C
      SUBROUTINE DIST
      COMMON DCPD,NCUT,KHEAD,LT1(400),LT2(400),KODE(400)
      COMMON/GEN2/W(5),MULTI,NHT,WPII,WHPII,SCL,ALM,DTH,TLT2,TD1,SDIST,
+DIST1,DIST2,DIST3,KK2,KT,NPC,LPC,ICRS,K,J,KIL,NN,MM,MIL
      IF(MM-NHT) 22,23,24
C
C      CALCULATE HAUL AND CHANGE OUT DISTANCES.
C
22  HD=W(2)/2.+(NHT-MM)*DIST3-W(1)/2.+DIST2+KIL*DIST1
      GO TO 25
23  HD=KIL*DIST1+DIST2
      CPD=TD1+SDIST+(NN-1)*DTH-ALM
      IF(MIL.NE.1) CPD=CPD+W(2)/2.
      IF(NN.EQ.KK2) CPD=(3.*CPD-W(2)/2.-(KK2-1)*DTH)/3.
      IF(MIL.EQ.1) KODE(K)=2
      GO TO 26
24  HD=W(2)/2.+(MM-NHT)*DIST3-W(1)/2.+DIST2+KIL*DIST1
25  CPD=TD1+SDIST+(NN-1)*DTH-ALM
      IF(MIL.EQ.1) GO TO 90
      CPD=CPD+W(1)/2.
      IF(NN.NE.KK2) GO TO 26
      IF(MM.EQ.1.OR.MM.EQ.KHEAD) CPD=(2.*CPD+W(1)/2.-FLOAT(KK2-1)*DTH)/2
+
      IF(MM.NE.1.AND.MM.NE.KHEAD) CPD=(3.*CPD+W(1)-FLOAT(KK2-1)*DTH)/3.

```

```

          GO TO 26
90 KODE(K)=1
26 IF(CPD.LT.U.) CPD=0.
C
C      CALCULATE TRAM DISTANCES.
C
      LI2(K)=ILI2+SDIST+(NN-1)*DTH-J*DIST1
      IF(MII.EQ.1) GO TO 31
      LI2(K)=LT2(K)+W(1)/2.
      IF(MM.EQ.NII) LT2(K)=LT2(K)-W(1)/2.+W(2)/2.
31 LI1(K)=DIST3
      IF(MM.EQ.KHEAD) LT1(K)=LI1(K)*(KHEAD-1)
      IF(MII.FQ.2.AND.MM.EQ.KHEAD) LT1(K)=LI1(K)-INT(DIST3)
C
C      OBTAIN ROOF BOLTER WORK SEQUENCE
C
      IF(K.IE.ICRS) GO TO 32
      KI=K-ICRS
      KE=KI+KHEAD
      GO TO 36
32 KI=KHEAD+K-ICRS
      KE=KI
36 WRITE(1,75)K,HD,CPD,DCPD
      WRITE(6,76)K,HD,CPD,DCPD,LT1(K),LT2(K),KODE(K),KI,KE
75 FORMAT(14,3F4.0)
76 FORMAT(14,2X,3F4.0,3I6,4X,2I3)
      RETURN
      END

```

APPENDIX D
RANDOM NUMBER GENERATORS

```

FUNCTION TRIAG(A,B,C)
C
C   A AND B ARE THE LOWER AND UPPER ENDS OF THE DISTRIBUTION.
C   C IS THE MODE.
C
U=RANDOM(L)
IF(U.LE.(C-A)/(B-A)) GO TO 2
TRIAG=B-SQRT(1.0-U)*(B-C)*(B-A)
RETURN
2 TRIAG=A+SQRT((B-A)*(C-A)*U)
RETURN
END

```

FUNCTION TO GENERATE RANDOM VARIATES FROM TRIANGULAR DISTRIBUTION

```

FUNCTION WEIBL(ALPHA,BETA)
C
C   THE FOLLOWING STATEMENT CAN BE OMITTED, IF IT IS
C   EXTERNALLY INSURED THAT ALPHA AND BETA ARE
C   POSITIVE NUMBERS.
C
  IF(ALPHA.LE.0.0.OR.BETA.LE.0.0) GO TO 7
  U=RANDOM(L)
  WEIBL=(BETA/(-ALOG(U)))**(1./ALPHA)
  RETURN
7 WRITE(6,10)
10 FORMAT(' ALPHA OR BETA IS LESS THAN OR EQUAL TO ZERO')
  STOP
  END

```

FUNCTION TO GENERATE RANDOM VARIATES FROM WEIBULL DISTRIBUTION

```

FUNCTION BETA(ALPHA1, ALPHA2)
C
C   COMPUTE A, B AND C PRIOR TO EXECUTION OF THE PROGRAM
C   USING THE FOLLOWING EQUATIONS.
C   A=ALPHA1+ALPHA2
C   B=1.0/AMIN(ALPHA1,ALPHA2)
C   IF(AMIN(ALPHA1,ALPHA2).GT.0.) B=(A-2.)/SQRT(2.ALPHA1*
C   +ALPHA2-A)
C   D=-1.3862944
C   C=ALPHA1+1.0/B
C
C   THE FOLLOWING STATEMENT CAN BE OMITTED, IF IT IS
C   EXTERNALLY INSURED THAT ALPHA1, ALPHA2, A AND C
C   ARE POSITIVE NUMBERS.
C
C   IF(ALPHA1.LT.0.0.OR.ALPHA2.LT.0.0.OR.A.LT.0.0.OR.C.LT.0.0) GO TO 7
2  U1=RANDOM(L)
  U2=RANDOM(L)
  V=B*A*LOG(U1/(1.-U1))
  W=ALPHA1*EXP(V)
  IF(A*A*LOG(A/(ALPHA2+W))+C*V+D.GE.A*LOG(U1*U1*U2)) GO TO 2
  X=W/(B+W)
  RETURN
C
C   IF THE FIRST STATEMENT IS OMITTED, OMIT THE
C   FOLLOWING THREE STATEMENTS TOO.
C
7  WRITE(6,10)
10 FORMAT(' ALPHA1, ALPHA2, A OR B IS LESS THAN ZERO')
  STOP
  END

```

FUNCTION TO GENERATE RANDOM DEVIATES FROM BETA DISTRIBUTION

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