

**APPENDIX A**

**SAMPLE CALCULATIONS**

Following are sample calculations detailing the entire process for calculating the various values reported. This example is entirely for the exterior girder, EGL, from the Haunched Girder specimen.

**Load Capacity:**

Determine Moment Capacity:

$$M_y = A_{BC} * F_{yBC} * d_{eBC} + 0.25 * A_{TC} * F_{yTC} * d_{eTC}$$

$$a = \frac{A_{BC} F_{yBC} + 0.25 A_{TC} F_{yTC}}{0.85 * f_c' * b_1}$$

$$d_{eBC} = H - y_{BC} - a/2$$

$$d_{eTC} = h + y_{TC} - a/2$$

$$M_d = 0.6 * M_y$$

For EGL, with nominal material properties:

$$A_{BC} = 5.7188 \text{ in.}^2$$

$$A_{TC} = 2.875 \text{ in.}^2$$

$$F_y = 50.0 \text{ ksi}$$

$$f_c' = 4.0 \text{ ksi}$$

$$b_1 = 47.5 \text{ in.}$$

$$A_{BC} F_{yBC} + A_{TC} F_{yTC} = 5.7188 * 50 + 0.25 * 2.875 * 50 = 321.88 \text{ kips}$$

$$a = \frac{321.88}{0.85 * 4.0 * 47.5} = 1.9931 \text{ in.} \quad a/2 = 0.9965 \text{ in.}$$

$$d_{eBC} = 35.0 - 1.138 - 0.9965 = 32.8655 \text{ in.}$$

$$d_{eTC} = 10.0 + 0.842 - 0.9965 = 9.8455 \text{ in.}$$

$$\begin{aligned} M_{yn} &= A_{BC} * F_y * d_{eBC} + 0.25 * A_{TC} * F_y * d_{eTC} \\ &= 5.7188 * 50 * 32.8655 + 0.25 * 2.875 * 50 * 9.8455 \\ &= 9751.4 \text{ k-in.} = \underline{\underline{812.6 \text{ k-ft}}} \end{aligned}$$

$$M_{dn} = 0.6 * M_{yn} = \underline{\underline{487.6 \text{ k-ft}}}$$

Determine Load Capacity:

$$M_{CL} = R_L(15) - R_{sj}(5) - 15(15/2)w_g - P(5)$$

$$R_L = R_{sj} + 15w_g + P$$

For EGL,

$$w_g = 0.220 \text{ klf}$$

$$R_{sj} = 1.464 \text{ kips}$$

$$R_L = 1.464 + 15 * 0.220 + P = 4.764 + P$$

$$\begin{aligned} M_{CL} &= 4.764 * 15 + 15P - 1.464 * 5 - (15^2/2) * 0.220 - 5P \\ &= 39.39 + 10P \end{aligned}$$

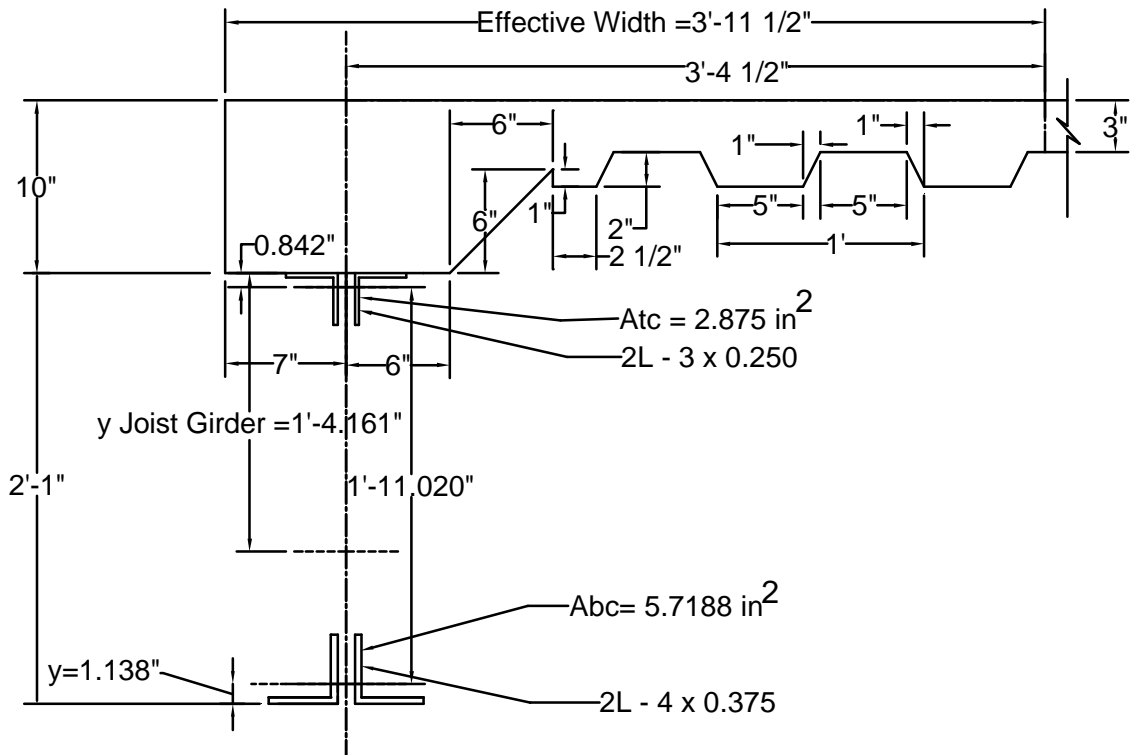
Solve for P using  $M_{CL} = M_{yn}$

$$10P = M_{yn} - 39.39$$

For  $M_{yn} = 812.6 \text{ k-ft}$ ,  $P = 77.3 \text{ kips}$

$$\begin{aligned} TL_{yn} &= 2 * (P + R_{sj}) + 30w_g = 2(77.3 + 1.464) + 30 * 0.220 \\ &= \underline{\underline{164.1 \text{ kips}}} = \text{Total Load on EGL} \end{aligned}$$

Moment of Inertia: (Provided by D. Samuelson, Nucor Research and Development.)



**Detail No. 1**

Calculate Joist-Girder Noncomposite Moment of Inertia

$$y_{Joist\ Girder} = \frac{A_{TC} y_{TC} + A_{BC} (d_{Joist\ Girder} - y_{BC})}{A_{TC} + A_{BC}} = \frac{2.875 (0.842) + 5.7188 (25 - 1.138)}{2.875 + 5.7188} = 16.161 \text{ in}$$

$$I_{Joist\ Girder\ Noncomposite} = I_{TC} + I_{BC} + \frac{A_{TC} A_{BC} d_e^2}{A_{TC} + A_{BC}}$$

Where:

$$d_{Joist\ Girder} = \text{Depth of steel joist girder} = 25 \text{ in}$$

$$I_{TC} = \text{Moment of Inertia for both top chord angles} = 1.244 \text{ in}^4 \times 2 \text{ angles} = 2.488 \text{ in}^4$$

$$I_{BC} = \text{Moment of Inertia for both bottom chord angles} = 4.359 \text{ in}^4 \times 2 \text{ angles} = 8.718 \text{ in}^4$$

$$y_{TC} = \text{Location for centroid of top chord} = 0.842 \text{ in}$$

$$y_{BC} = \text{Location for centroid of bottom chord} = 1.138 \text{ in}$$

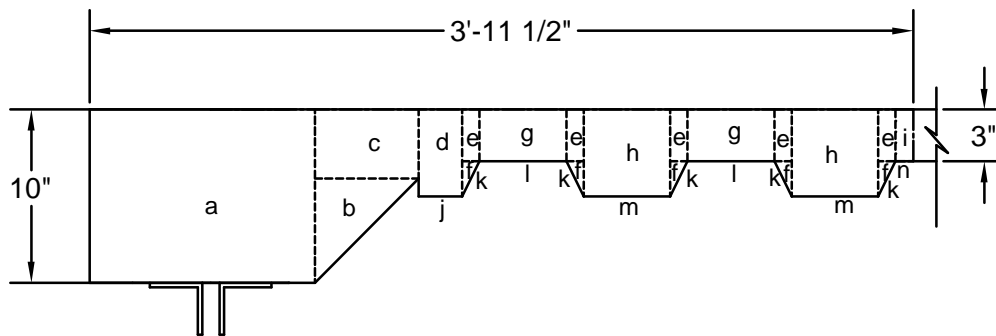
$$d_e = \text{Joist girder effective depth} = 25 \text{ in} - 0.842 \text{ in} - 1.138 \text{ in} = 23.020 \text{ in}$$

$$A_{TC} = \text{Area of both top chord angles} = 1.438 \text{ in}^2 \times 2 \text{ angles} = 2.875 \text{ in}^2$$

$$A_{BC} = \text{Area of both bottom chord angles} = 2.859 \text{ in}^2 \times 2 \text{ angles} = 5.718 \text{ in}^2$$

$$I_{\text{Joist Girder Noncomposite}} = 2.488 \text{ in}^4 + 8.718 \text{ in}^4 + \frac{(2.875 \text{ in}^2)(5.718 \text{ in}^2)(23.020 \text{ in})^2}{(2.875 \text{ in}^2 + 5.718 \text{ in}^2)} = 1,025 \text{ in}^4$$

Calculate Transformed Moment of Inertia for Concrete Slab



**Detail No. 2**

$$n = \frac{E_s}{E_c}$$

$$E_c = 33w_c^{1.5} \sqrt{f'_c} = 33(145 \text{ pcf})^{1.5} \sqrt{4530} = 3,878.1 \text{ ksi}$$

$$n = \frac{29,000 \text{ ksi}}{3,878.1 \text{ ksi}} = 7.4779$$

2VL 18 Ga. deck, deck thickness = 0.0474 in

1 layer 6 x 6 – W1.4 x W1.4 welded wire fabric

**Table No. 1**

	Element Area (in <sup>2</sup> )	Element Area/ n (in <sup>2</sup> )	<sup>1</sup> No. Pieces	Area (in <sup>2</sup> )	Area Transformed (in <sup>2</sup> )	y to top slab (in)	A <sub>trans</sub> x y (in <sup>3</sup> )	h (in)	A <sub>trans</sub> x h <sup>2</sup> (in <sup>4</sup> )	I <sub>o</sub> (in <sup>4</sup> )
a	130.00	17.384	1	130.0	17.3844	5.00	86.9221	-1.3253	30.5346	144.87
b	18.00	2.4071	1	18.00	2.4071	6.000	14.4424	-2.3253	13.0152	4.8141
c	24.00	3.2094	1	24.00	3.2094	2.00	6.4189	1.6747	9.0012	4.2792
d	12.50	1.6716	1	12.50	1.6716	2.500	4.1789	1.1747	2.3066	3.4825
e	3.00	.4012	5	15.00	2.0059	1.500	3.0088	2.1747	9.4865	1.5044
f	1.00	.1337	5	5.00	.6686	3.666	2.4517	.0080	0.0000	.1486
g	15.00	2.0059	2	30.0	4.0118	1.500	6.0177	2.1747	18.9730	3.0088
h	25.00	3.3432	2	50.00	6.6863	2.500	16.7158	1.1747	9.2265	13.93
i	3.00	.4012	1	3.000	.4012	1.500	.6018	2.1747	1.8973	.3009
j	.1185	.1185	1	.1185	.1185	5.000	.5925	-1.3253	.2081	0.0000
k	.1060	.1060	5	.5299	.5299	4.000	2.1198	-.3253	.0561	.1767
l	.2370	.2370	2	.4740	.4740	3.000	1.4220	.6747	.2158	.0001
m	.2370	.2370	2	.4740	.4740	5.000	2.3700	-1.3253	.8325	.0001
n	.0474	.0474	1	.0474	.0474	3.000	.1422	.6747	.0216	0.0000
mesh	0.1116	0.1116	1	0.112	0.1116	2.909	.3248	.7654	.0654	.0001
Totals	232.3575	31.8152		289.2555	40.2018		147.7294		95.8404	76.5157

Haunch flashing metal was ignored in the above calculation.

$$y_{transformed} = \frac{\sum A_{trans} \cdot y}{\sum A_{trans}} = \frac{147.7294}{40.2018} = 3.6747 \text{ in to top of slab}$$

$$I_{transformed} = \sum A_{trans} h^2 + \sum I_o = 95.8404 + 176.5157 = 272.3561 \text{ in}^4$$

Calculate Combined Transformed Moment of Inertia for Concrete Slab & Girder

Area of top and bottom chord = 2.875 in<sup>2</sup> + 5.7188 in<sup>2</sup> = 8.5938 in<sup>2</sup>

Distance from centroid of joist to top of slab = y = y<sub>joist</sub> + 10 = 16.161 + 10 = 26.161 in

**Table No. 2**

Element	<sup>1</sup> Element Area (in <sup>2</sup> )	Y to top of slab (in)	Area *y (in <sup>3</sup> )	h (in)	Area x h <sup>2</sup> (in <sup>4</sup> )	I <sub>o</sub> (in <sup>4</sup> )
Joist Girder	8.5938	26.161	224.82	18.5261	2,949.5	1,025
Slab	40.2018	3.6747	147.7295	3.9602	630.492	272
Total	48.7956		372.5496		3,580.0	1,297.4

<sup>1</sup>Element area shown for slab has been transformed into equivalent area of steel . See Table No. 1

$$y_{centroid} = \frac{\sum A y}{\sum A} = \frac{372.5496}{48.7956} = 7.6349" \text{ from top of slab}$$

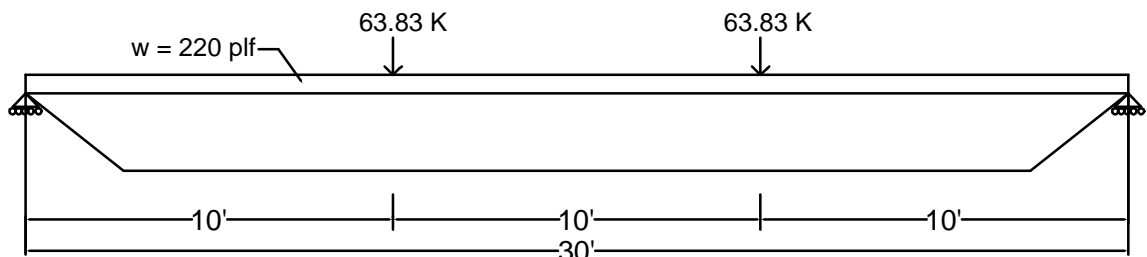
$$I_{composite} = \sum A h^2 + \sum I_O = 3,580 + 1,297.4 = 4,877.4 \text{ in}^4$$

### Adjustment to $I_{composite}$ for Shear Stud Slippage

Adjusting for slippage between the shear studs and the concrete, a shear stud slip factor of 1.05 was assumed.

$$I_{non-adjusted \text{ for span / depth}} = \frac{I_{composite}}{1.05} = \frac{4,877.4}{1.05} = 4,645 \text{ in}^4$$

### Adjusting for Web Shortening Effects



**Detail No. 3**

$$\Delta_{centerline \text{ for uniform load on noncomposite joist girder}} = \frac{5w_g l^4}{384EI_{noncomposite}}$$

$$\Delta_{centerline \text{ for uniform load on noncomposite joist girder}} = \frac{5(220 \text{ plf})(30 \text{ ft})^4 (12 \text{ in/ft})^3}{384(29 \times 10^6 \text{ psi})(1,025 \text{ in}^4)} = 0.1349"$$

$$\Delta_{centerline \text{ for concentrated loads}} = \frac{Pa(3l^2 - 4a^2)}{24EI} = \frac{63,830 \text{ lb} (120 \text{ in}) [3(360 \text{ in})^2 - 4(120 \text{ in})^2]}{24(29 \times 10^6 \text{ psi})(1,025 \text{ in}^4)} = 3.556 \text{ in}$$

$$\Delta_{Total \text{ Noncomposite}} = \Delta_{Uniform \text{ Load Noncomposite}} + \Delta_{Concentrated \text{ Load}} = 0.1349 \text{ in} + 3.556 \text{ in} = 3.6909 \text{ in}$$

Using the Vulcraft Joist Design Program, the deflection of the noncomposite joist under the loading shown in Detail No. 3 was calculated to be 3.97". The Vulcraft joist program assumes that: 1) The top chord is a continuous member and 2) That the webs and chords are connected to the top and bottom chords by pinned joints.

The difference between the theoretical centerline deflection and the deflection from the Vulcraft Program is due to web effects. Correcting the moment of inertia for web effects:

$$I_{\text{adjusted for web effects}} = 4,645 \text{ in}^4 \left( \frac{3.6909 \text{ in}}{3.97 \text{ in}} \right) = 4,645 \text{ in}^4 (0.9297) = 4,318 \text{ in}^4$$

### Correcting Composite Moment of Inertia for Span / Depth Effects

Using results of 18 prior full-scale composite joist tests, an empirical equation to adjust for Span / Depth joist ratios was derived. This additional adjustment was required after taking into account shear stud slip and web shorting effects so that the measured deflections would more closely match predicted deflections.

The equation selected for adjusting for the span \ depth effects is of the form  $y = a + \frac{b}{x^2}$

$$\text{where } y = \frac{I_{\text{non-adjusted for span / depth}}}{I_{\text{adjusted for span / depth}}}$$

$$a = 0.91775$$

$$b = 79.1692$$

$$x = \frac{\text{Joist Span}}{\text{Joist Depth}} = \frac{30 \text{ ft} \times 12 \text{ in/ft}}{25 \text{ in}} = 14.4$$

$$\text{Adjustment factor for Span / Depth} = a + \frac{b}{x^2} = 0.91775 + \frac{79.1692}{14.4^2} = 1.2995$$

$$I_{\text{adjusted for span / depth}} = \frac{I_{\text{non-adjusted for span / depth}}}{\text{Adjustment factor for Span / Depth}} = \frac{4,318 \text{ in}^4}{1.2995} = 3,323 \text{ in}^4$$

The calculated value for  $I_{\text{composite}}$  for IG after adjusting for shear stud slip, web effects, and span / depth ratio is  $= 3,323 \text{ in}^4$

$$\underline{I_{\text{calc}} = 3,323 \text{ in}^4 \text{ for EGL}}$$

## **APPENDIX B**

### **COMPOSITE JOIST-GIRDER TEST RESULTS**

Following are plots of the data obtained from the various composite joist-girder specimens. The data is plotted as total load on the girder versus the measured displacement or force (vertical deflection, chord member strain, web member strain, concrete strain, slip, etc.) The test data is organized according to girder for each specimen. Each section begins with a summary of the girder configuration and related information. Total load refers to the combined loading of the structure self-weight plus the applied load introduced through the hydraulic rams.

The first load point of each data set establishes a zero position. The second data point within each set accounts for the self-weight of the steel in the specimen. The third point indicates effect of the placement of concrete. All subsequent data points refer to the effects of the cycles of live load applied during testing.

# COMPOSITE FLUSH FRAMED JOIST-GIRDER TEST SUMMARY SHEET

GIRDER DESIGNATION: EGL(EG3)

TEST DATES: 28-30 November 1995

TEST DESCRIPTION				
<b>Joist-Girder:</b>	Span:	<u>30'-0"</u>	Weight:	<u>48.9 plf</u>
	Depth:	<u>30 in.</u>	Spacing:	<u>7 ft</u>
	Top Chord:	<u>2L-3.00x3.00x0.250</u>	Yield Stress:	<u>58.0 ksi</u>
	Bottom Chord:	<u>2L-4.00x4.00x0.375</u>	Yield Stress:	<u>60.2 ksi</u>
	Deck:	Type: <u>2 VL</u>	Gage:	<u>18 ga</u>
<b>Slab:</b>	Total Depth:	<u>5 in.</u>	Compressive Strength:	<u>4900 psi</u>
<b>Shear Connector:</b>	Type:	<u>3/4 in. x 4 1/2 in. Welded Headed Shear Studs</u>		
	Quantity:	<u>15 per half-span, 30 total</u>		

THEORETICAL CALCULATIONS	
Theoretical Max. Total Load per Joist-Girder:	<u>189.5 kips</u>
Theoretical Moment of Inertia:	<u>2705 in.<sup>4</sup></u>

TEST RESULTS	
Total Load on Joist-Girder at Failure:	<u>160.8 kips</u>
Maximum Total Load on Joist-Girder:	<u>174.3 kips</u>
Midspan Deflection at Failure:	<u>2.74 in.</u>
Experimental Moment of Inertia:	<u>2965 in.<sup>4</sup></u>
Mode of Failure:	<u>Compression buckling of web member W3R</u>

COMPARISON OF ACTUAL TO THEORETICAL	
Maximum Total Load on Joist-Girder	= 0.92
Theoretical Max. Total Load on Joist-Girder	

### LOCATION OF INSTRUMENTATION ON JOIST-GIRDER

WEST EAST

Location of Strain Gages on EGL Braces:

SOUTH NORTH

EGL Joist

Strain Gages:

1-4 BC	21-24 TC5	E1 SLIP E1
5-8 TC1	25-28 TC6	E2 SLIP E2
9-12 TC2	29-32 V3	W1 SLIP W1
13-16 TC3	33-36 V6	W2 SLIP W2
17-20 TC4	CONC CONCRETE	

Slips:

E1 SLIP E1
E2 SLIP E2
W1 SLIP W1
W2 SLIP W2

Strain Gages on EGL Braces:

▽ BR E1   ▽ BR E2   ▽ BR W1   ▽ BR W2

Vertical Defl.:

- △ EQ BOTTOM
- △ CL BOTTOM
- △ CL TOP
- △ WQ BOTTOM

Lateral Defl.:

- ① LAT E\*
- ② LAT W\*
- ③ LAT M\*\*

\* Measured on EGL & EGR  
\*\* Measured on IG

Location of Strain Gages on Cross-Section:

West East

North South

TC BC

V3 V6

TOP VIEW CROSS-SECTION

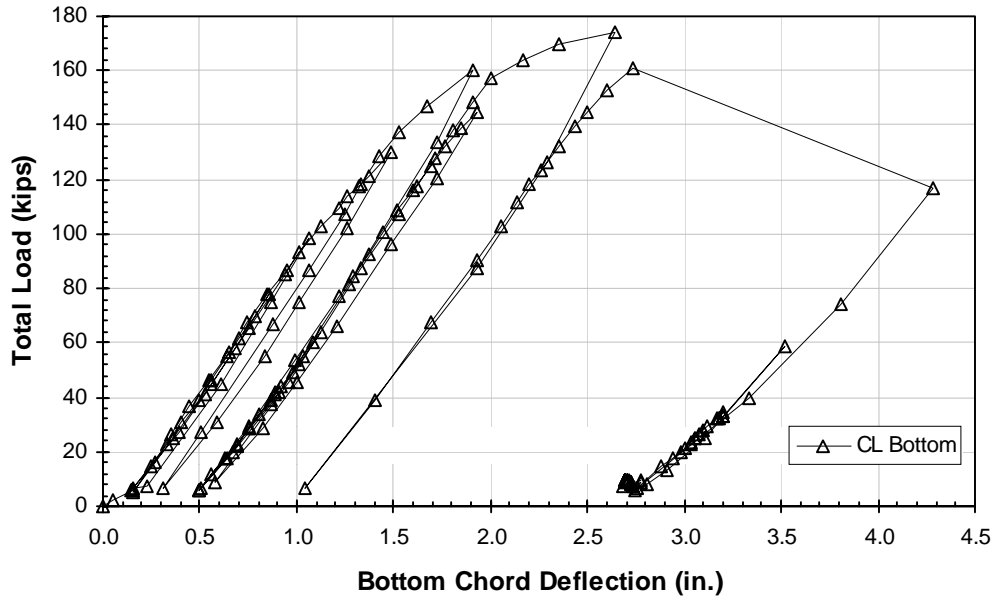


Figure B.1.1 Total Load vs. Bottom Chord Midspan Deflection of EGL

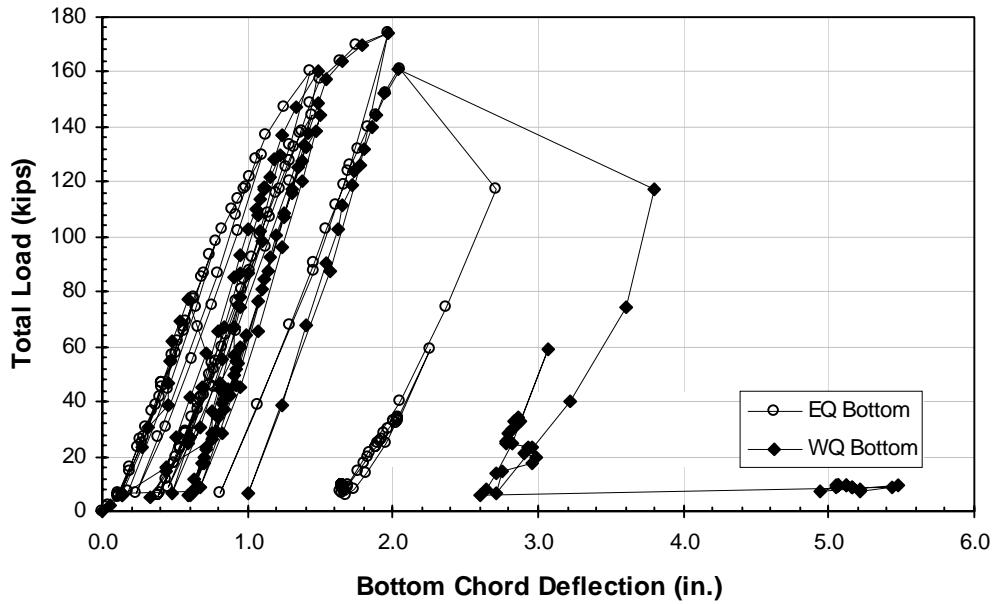
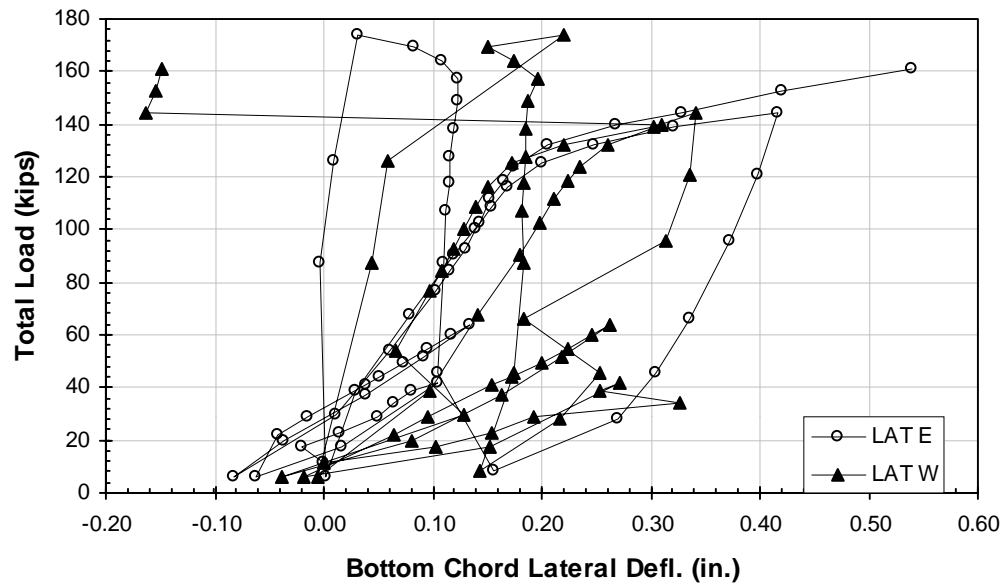
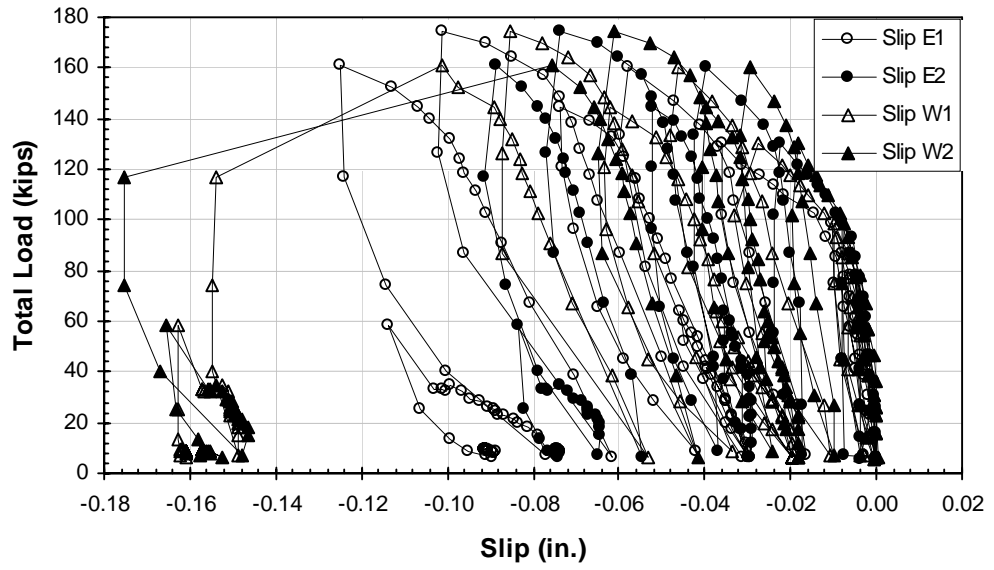


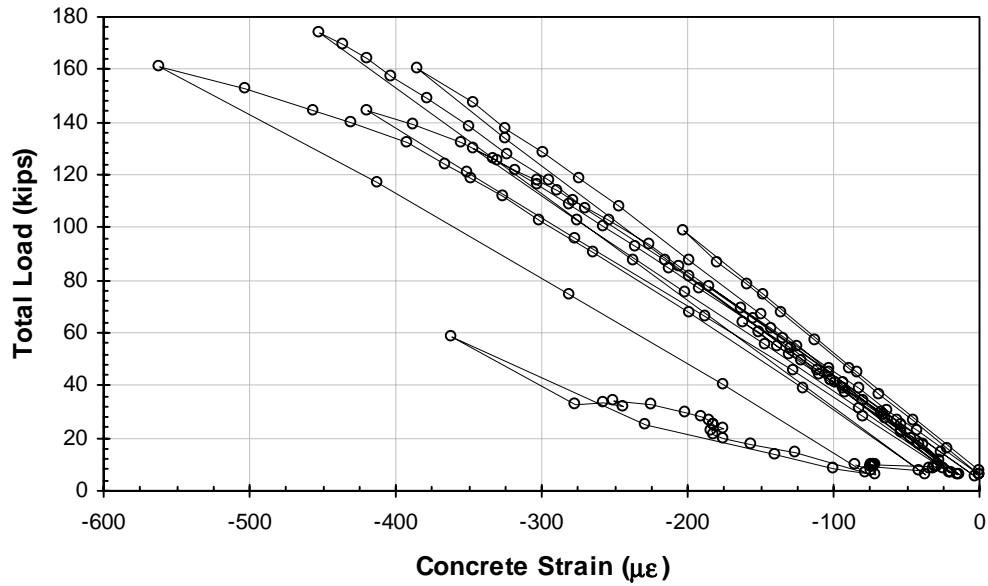
Figure B.1.2 Total Load vs. Bottom Chord Quarter Deflections of EGL



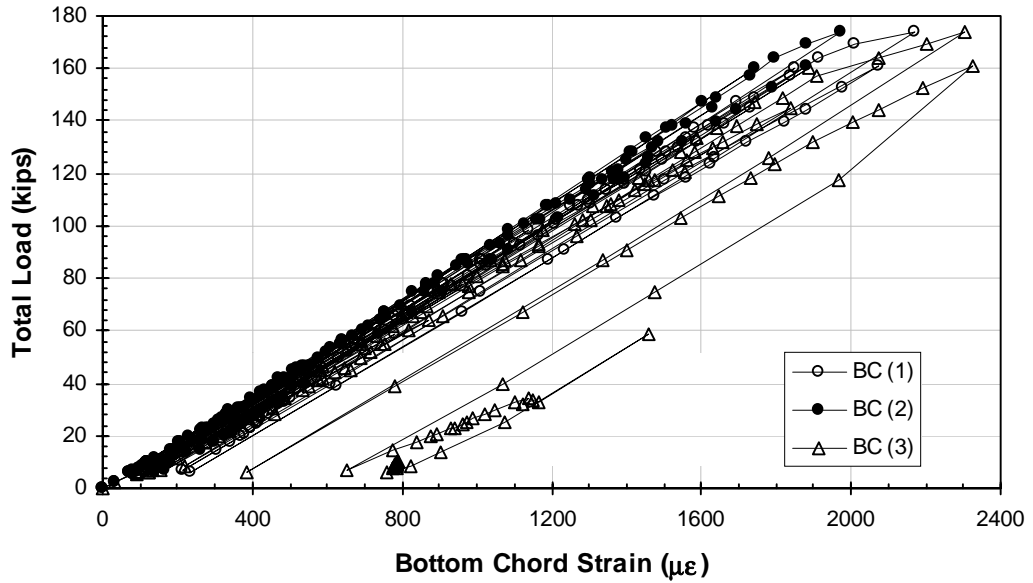
**Figure B.1.3 Total Load vs. Bottom Chord Lateral Deflections of EGL**



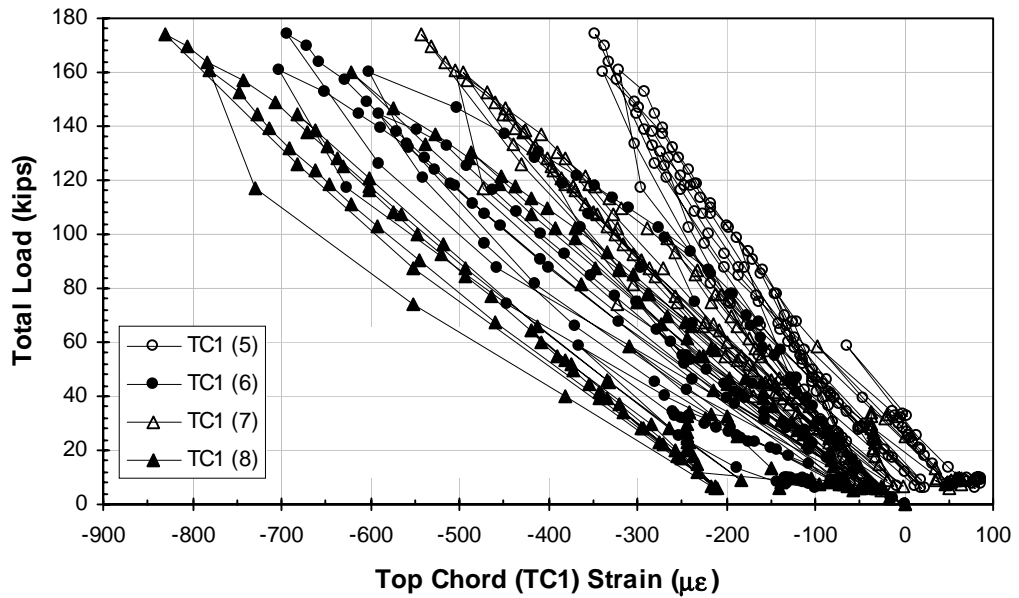
**Figure B.1.4 Total Load vs. Slip of EGL**



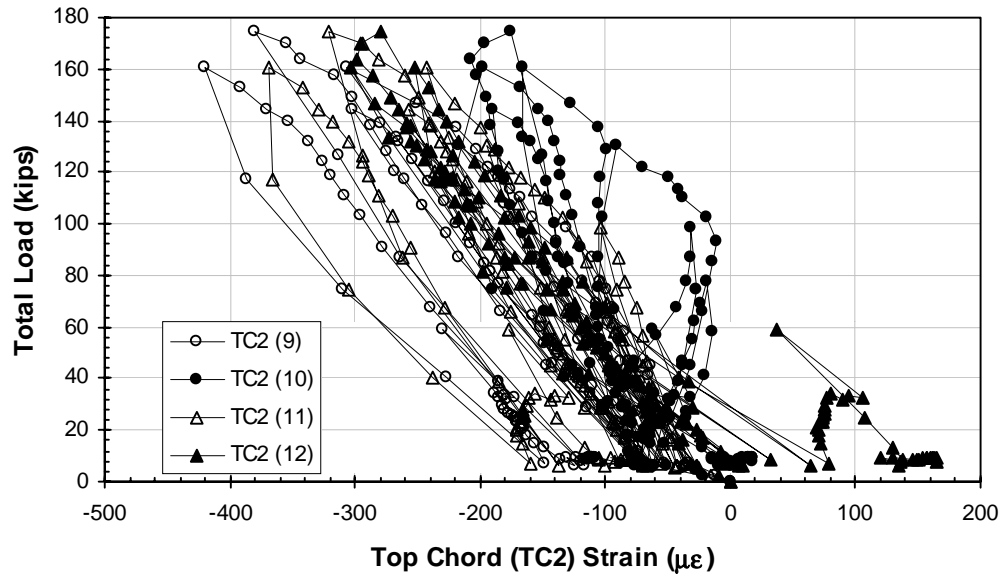
**Figure B.1.5 Total Load vs. Concrete Strain of EGL**



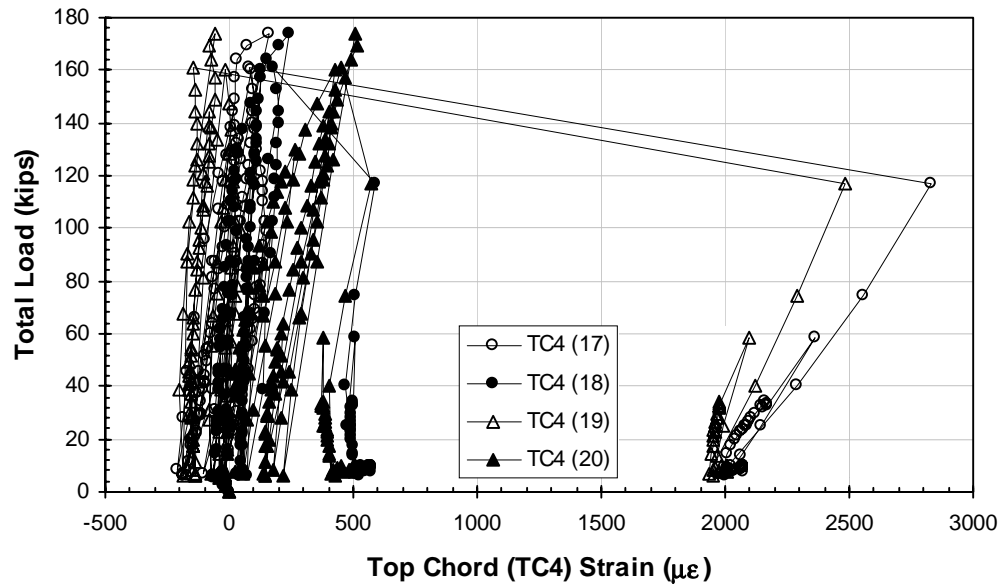
**Figure B.1.6 Total Load vs. Bottom Chord Strain of EGL**



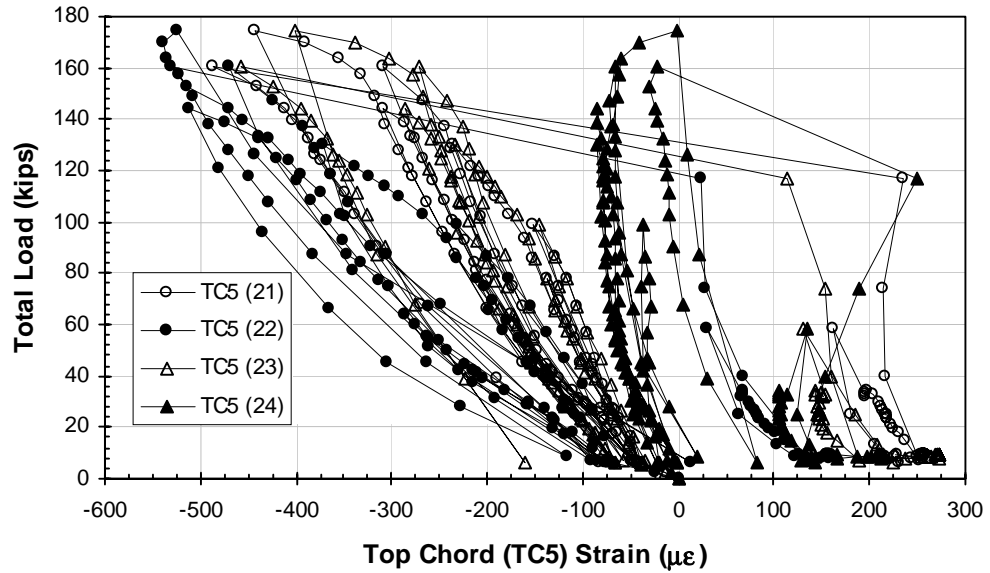
**Figure B.1.7 Total Load vs. Top Chord (TC1) Strain of EGL**



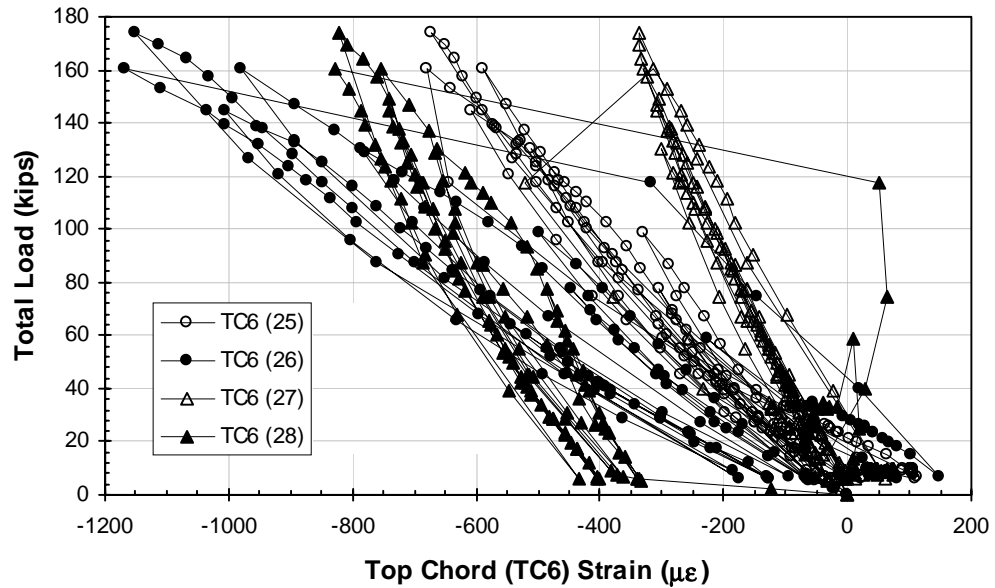
**Figure B.1.8 Total Load vs. Top Chord (TC2) Strain of EGL**



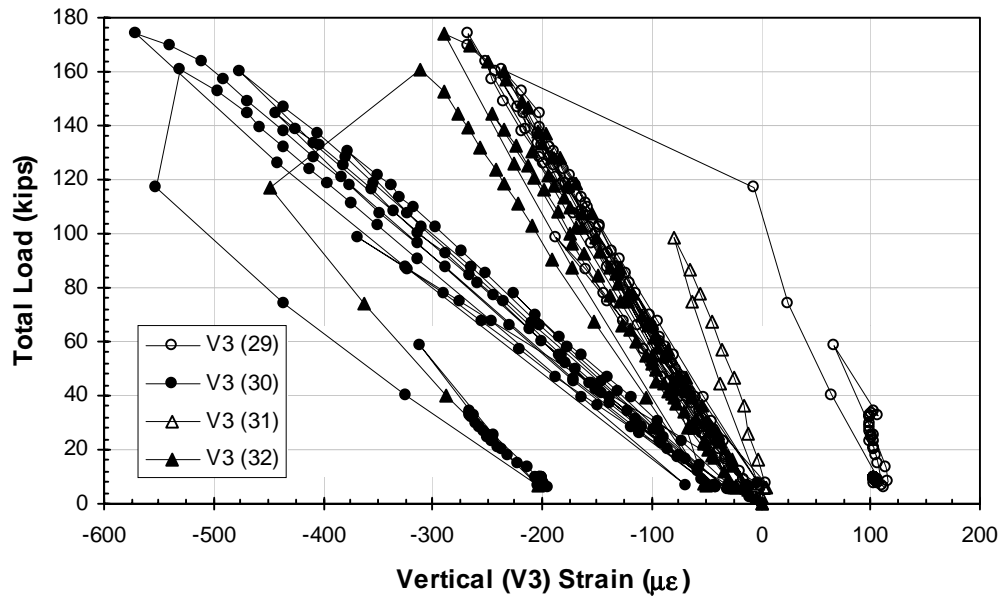
**Figure B.1.9 Total Load vs. Top Chord (TC4) Strain of EGL**



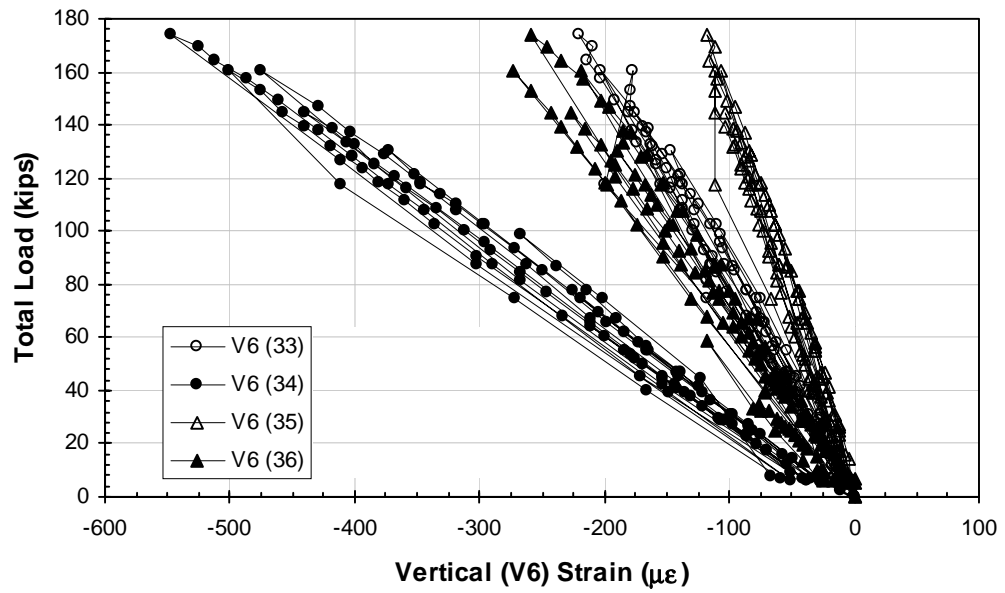
**Figure B.1.10 Total Load vs. Top Chord (TC5) Strain of EGL**



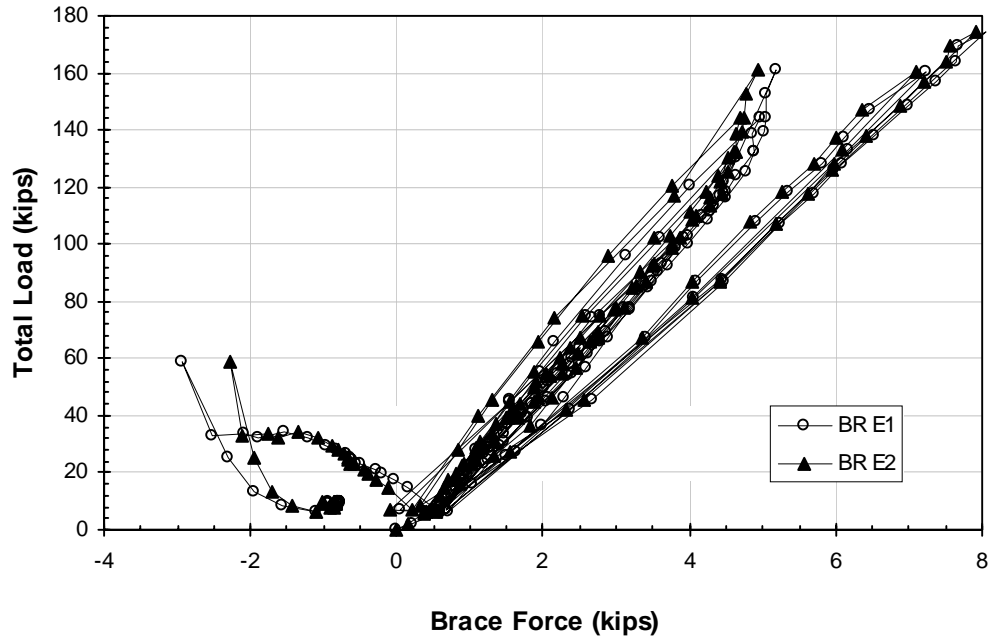
**Figure B.1.11 Total Load vs. Top Chord (TC6) Strain of EGL**



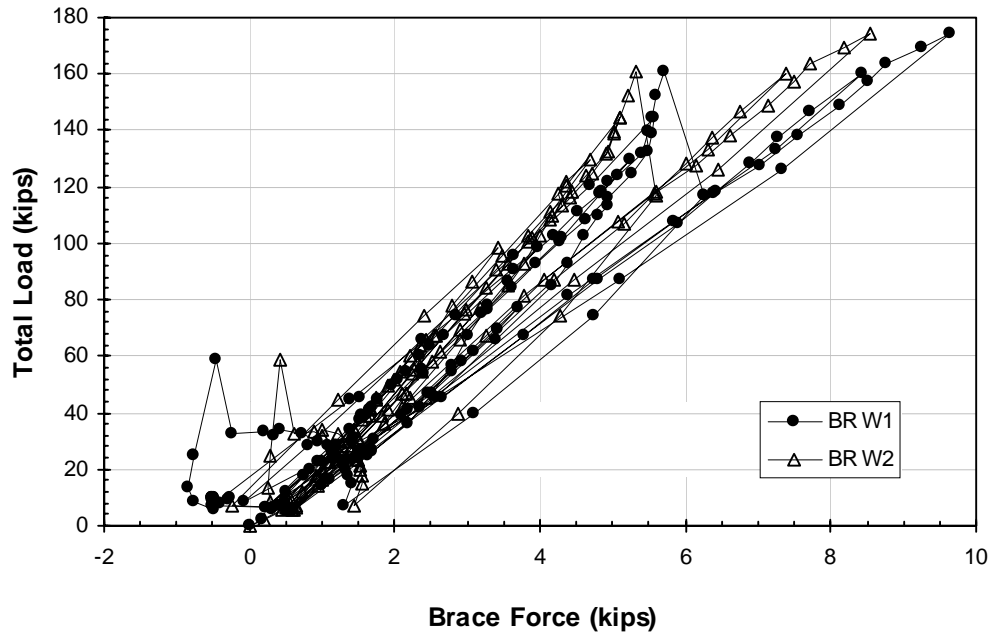
**Figure B.1.12 Total Load vs. Vertical (V3) Strain of EGL**



**Figure B.1.13 Total Load vs. Vertical (V6) Strain of EGL**



**Figure B.1.14 Total Load vs. Brace Force of EGL (East Braces)**



**Figure B.1.15 Total Load vs. Brace Force of EGL (West Braces)**

# COMPOSITE FLUSH FRAMED JOIST-GIRDER TEST SUMMARY SHEET

GIRDER DESIGNATION: IG

TEST DATES: 28-30 November 1995

TEST DESCRIPTION				
<b>Joist-Girder:</b>	Span:	<u>30'-0"</u>	Weight:	<u>91.3 plf</u>
	Depth:	<u>30 in.</u>	Spacing:	<u>7 ft</u>
	Top Chord:	<u>2L-4.00x4.00x0.375</u>	Yield Stress:	<u>58.7 ksi</u>
	Bottom Chord:	<u>2L-5.00x5.00x0.625</u>	Yield Stress:	<u>55.0 ksi</u>
	Type:	<u>2 VL</u>	Gage:	<u>18 ga</u>
<b>Deck:</b>	Total Depth:	<u>5 in.</u>	Compressive Strength:	<u>4900 psi</u>
<b>Slab:</b>	Type:	<u>3/4 in. x 4 1/2 in. Welded Headed Shear Studs</u>		
<b>Shear Connector:</b>	Quantity:	<u>28 per half-span, 56 total</u>		

THEORETICAL CALCULATIONS	
Theoretical Max. Total Load on Joist-Girder:	<u>350.9 kips</u>
Transformed Moment of Inertia:	<u>5324 in.<sup>4</sup></u>

TEST RESULTS	
Total Load on Joist-Girder at Failure:	<u>329 kips</u>
Maximum Total Load on Joist-Girder:	<u>341.4 kips</u>
Midspan Deflection at Failure:	<u>7.2 in.</u>
Experimental Moment of Inertia:	<u>5541 in.<sup>4</sup></u>
Mode of Failure:	<u>Failure of filler welds; Web buckling</u>

COMPARISON OF ACTUAL TO THEORETICAL	
Maximum Total Load on Joist-Girder	= 0.97
Theoretical Max. Total Load on Joist-Girder	

### LOCATION OF INSTRUMENTATION ON JOIST-GIRDER

WEST EAST

Location of Strain Gages on EGL Braces:

SOUTH NORTH

EGL Joist

Strain Gages:

1-4	BC	21-24	TC5
5-8	TC1	25-28	TC6
9-12	TC2	29-32	V3
13-16	TC3	33-36	V6
17-20	TC4	CONC	CONCRETE

Slips:

E1	SLIP E1
E2	SLIP E2
W1	SLIP W1
W2	SLIP W2

Strain Gages on EGL Braces:

▽ BR E1   ▽ BR E2   ▽ BR W1   ▽ BR W2

Vertical Defl.:

- △ EQ BOTTOM
- △ CL BOTTOM
- △ CL TOP
- △ WQ BOTTOM

Lateral Defl.:

- ① LAT E\*
- ② LAT W\*
- ③ LAT M\*\*

\* Measured on EGL & EGR  
\*\* Measured on IG

West East

V3   V6

TOP VIEW

North South

TC   BC

CROSS-SECTION

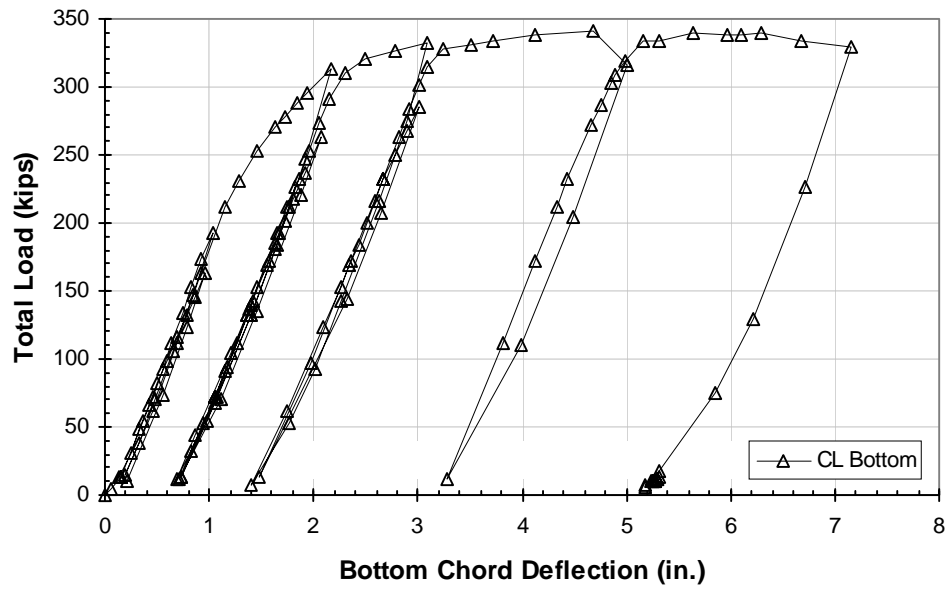


Figure B.2.1 Total Load vs. Bottom Chord Midspan Deflection of IG

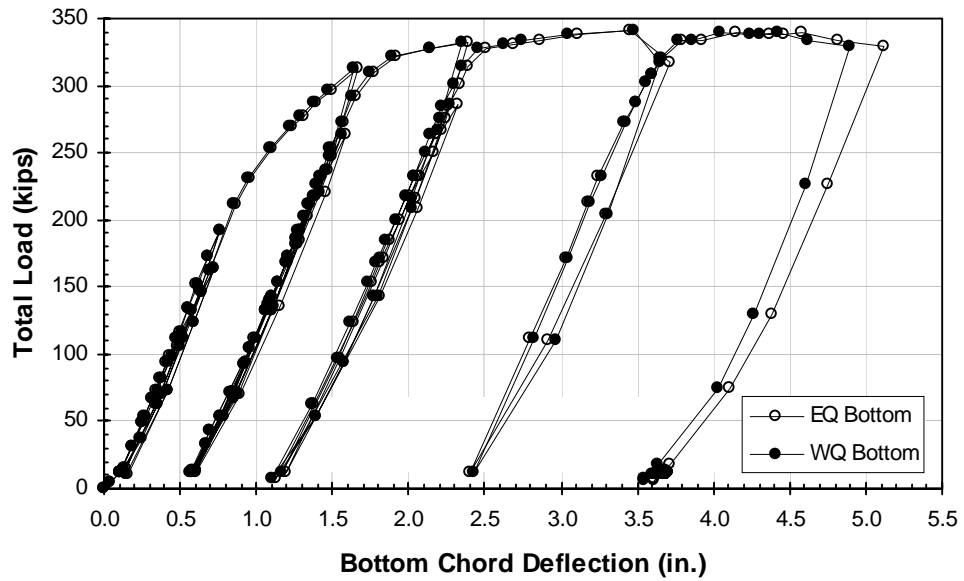
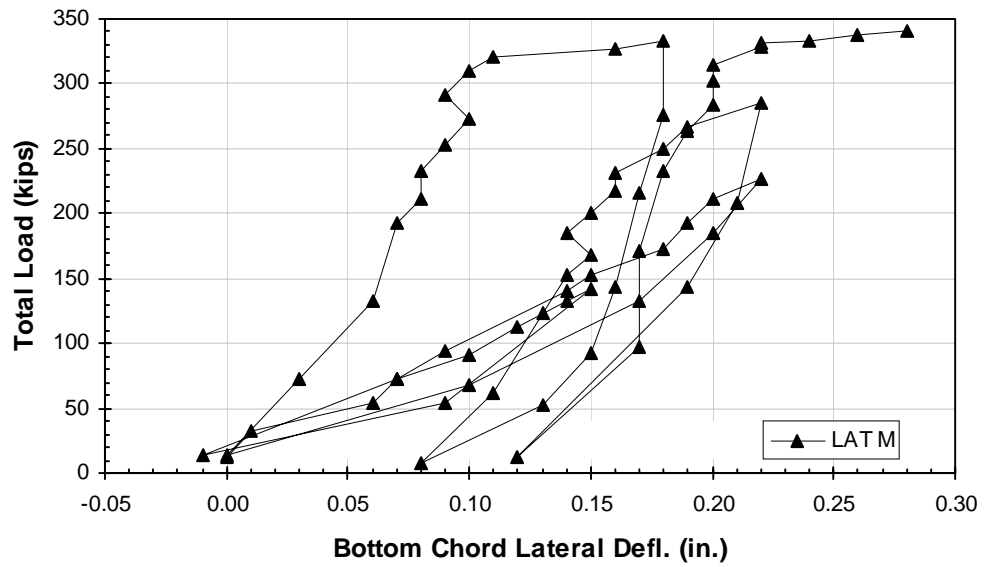
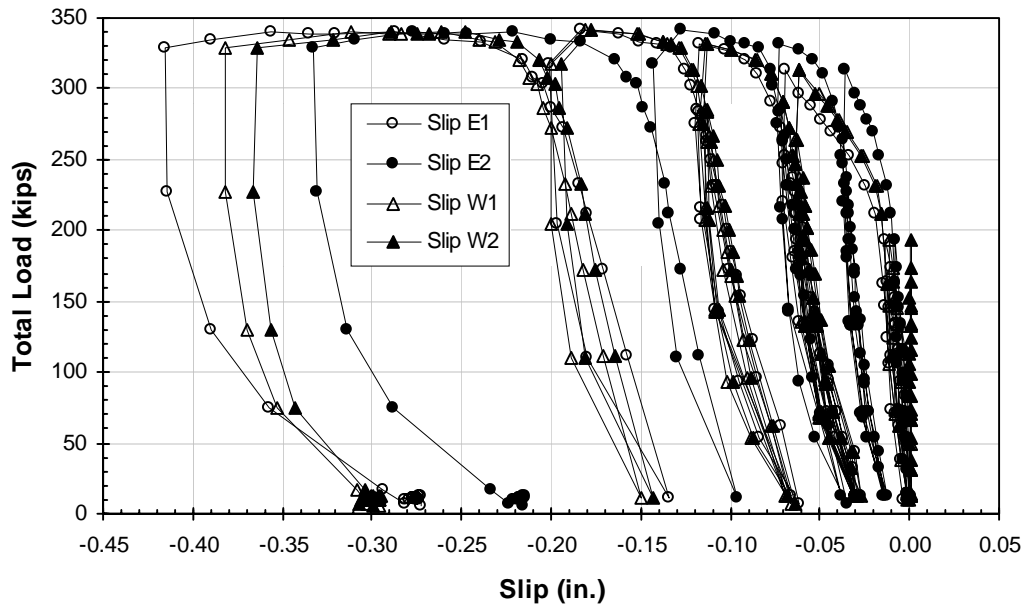


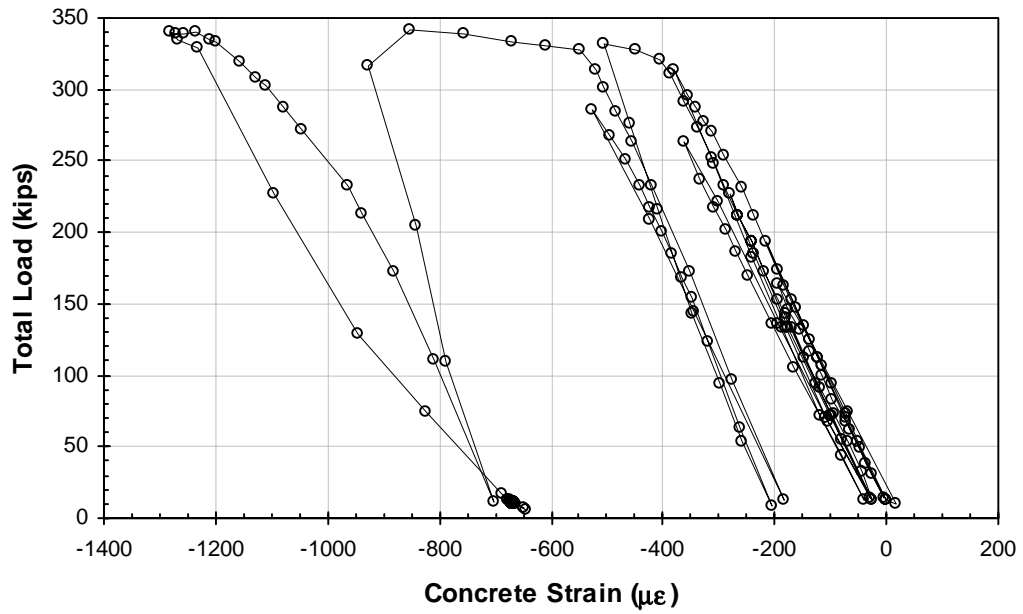
Figure B.2.2 Total Load vs. Bottom Chord Quarter Deflections of IG



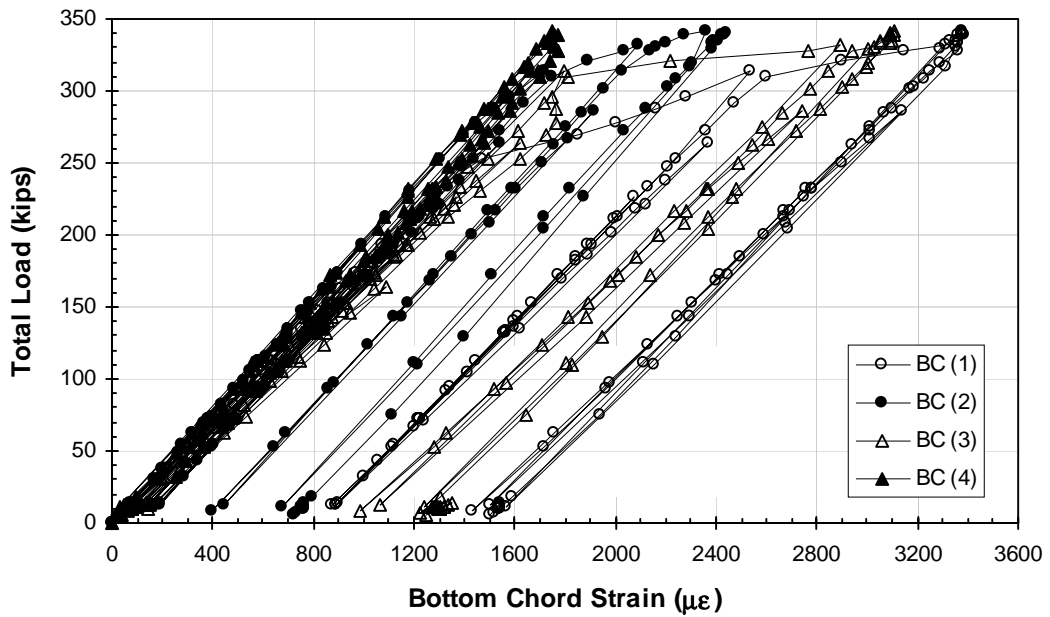
**Figure B.2.3 Total Load vs. Bottom Chord Lateral Deflections of IG**



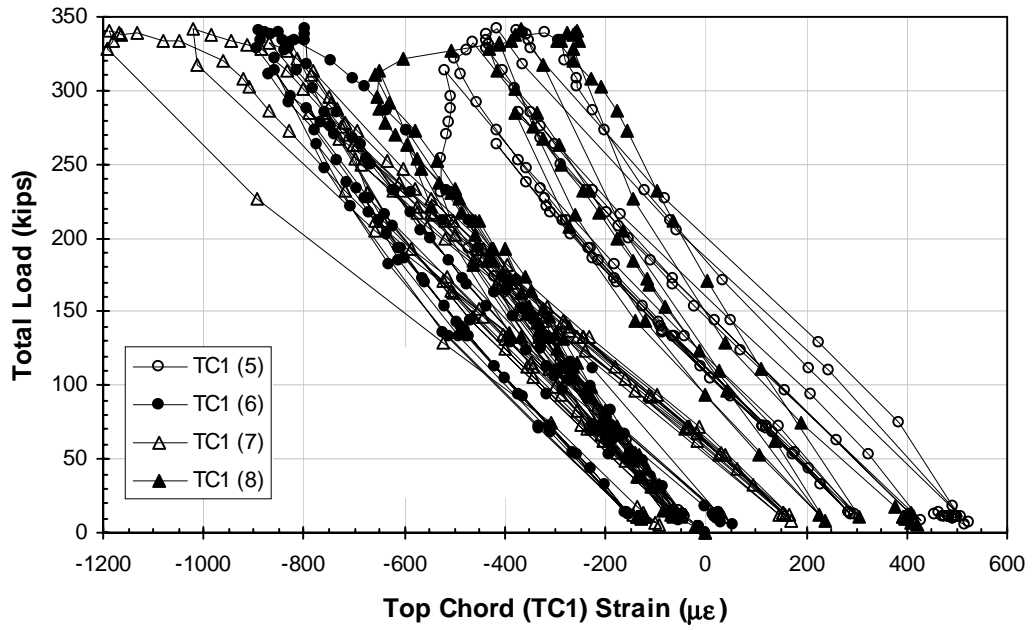
**Figure B.2.4 Total Load vs. Slip of IG**



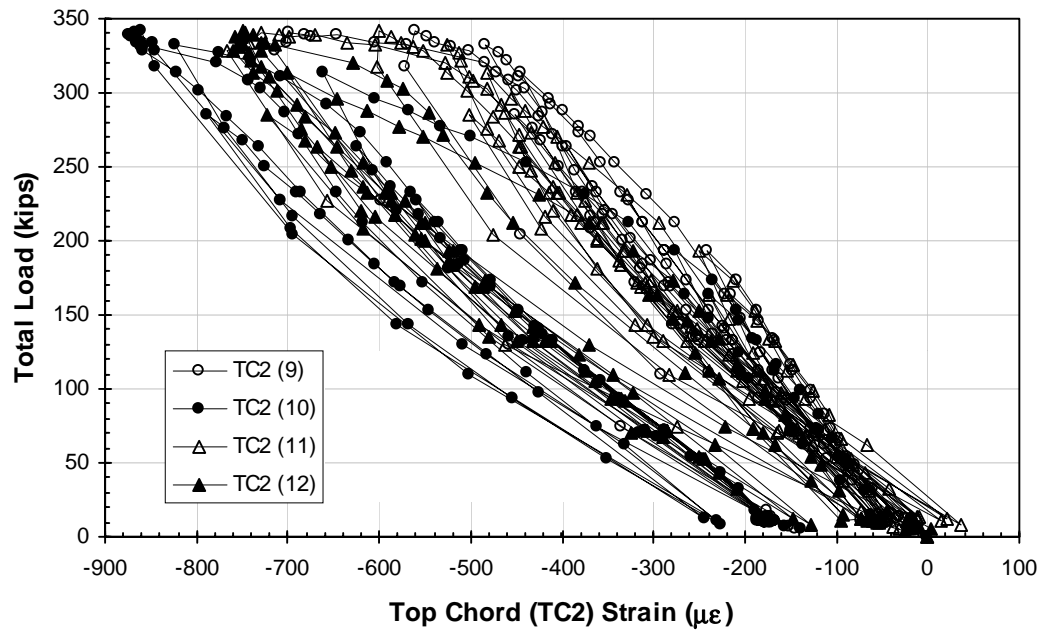
**Figure B.2.5 Total Load vs. Concrete Strain of IG**



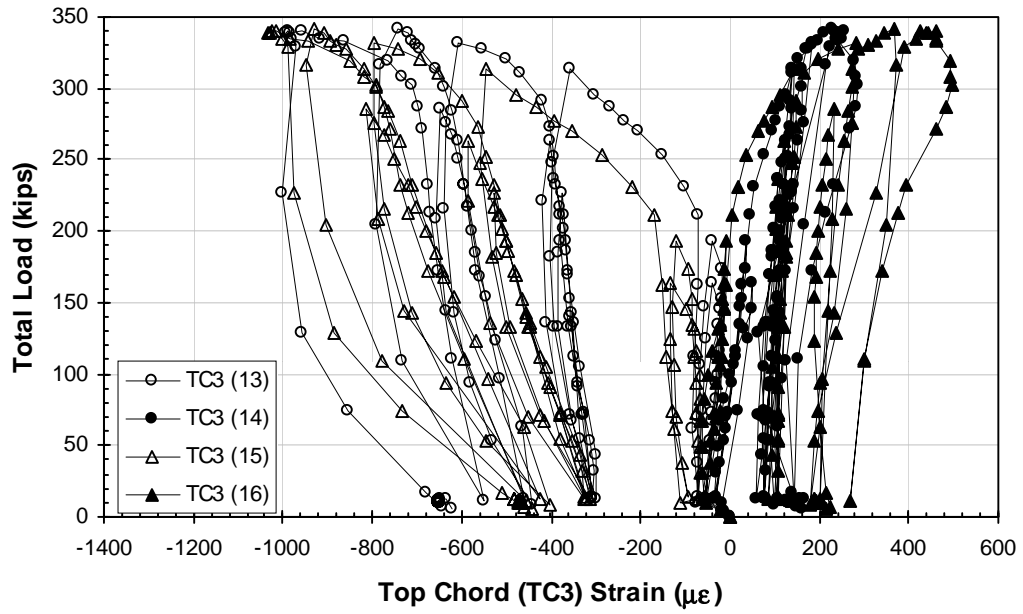
**Figure B.2.6 Total Load vs. Bottom Chord Strain of IG**



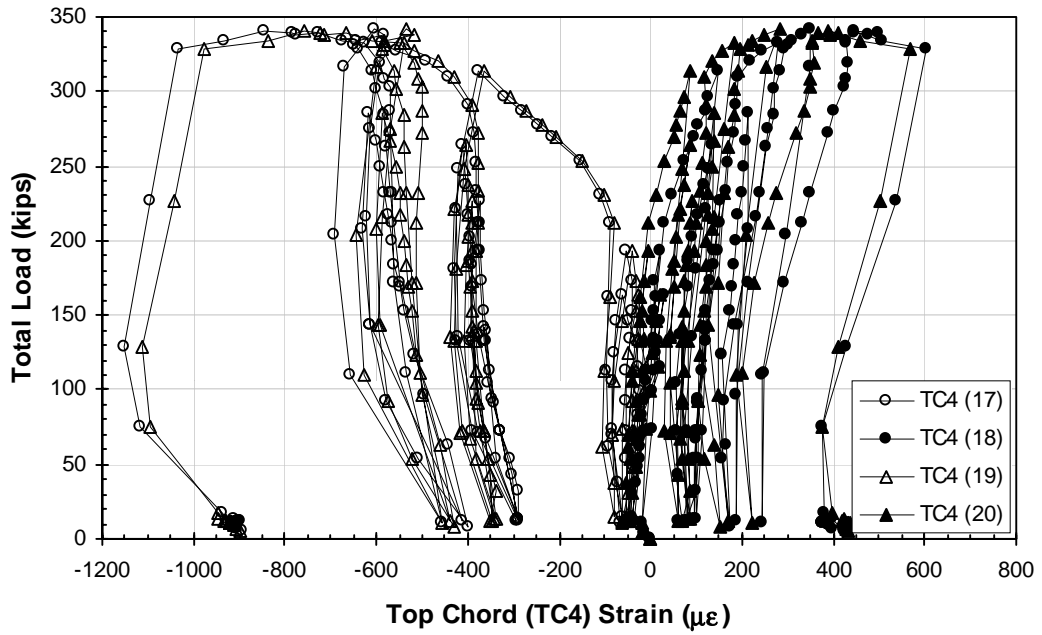
**Figure B.2.7 Total Load vs. Top Chord (TC1) Strain of IG**



**Figure B.2.8 Total Load vs. Top Chord (TC2) Strain of IG**



**Figure B.2.9 Total Load vs. Top Chord (TC3) Strain of IG**



**Figure B.2.10 Total Load vs. Top Chord (TC4) Strain of IG**

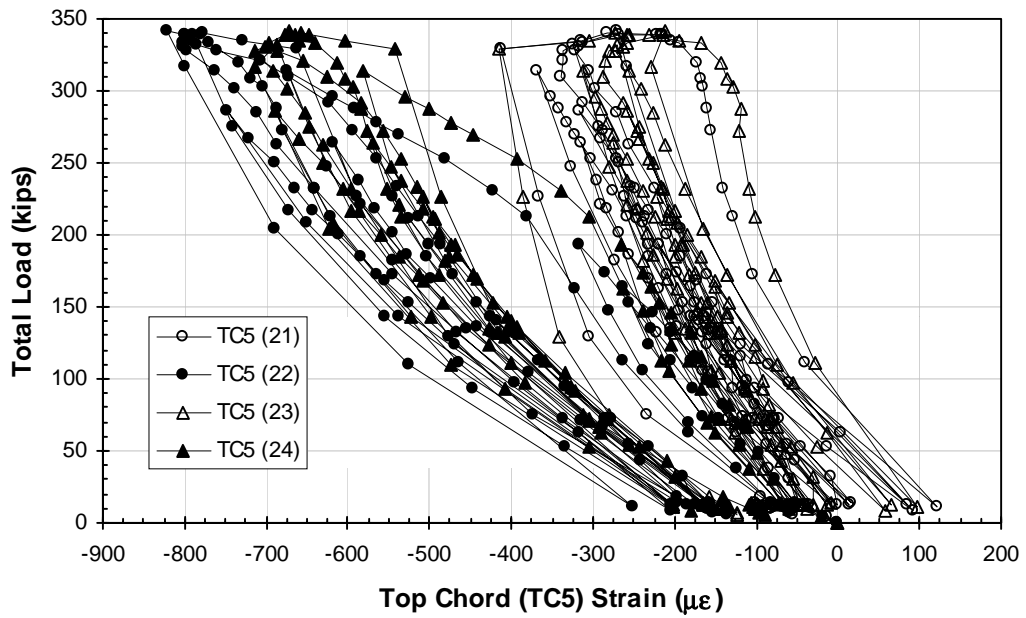


Figure B.2.11 Total Load vs. Top Chord (TC5) Strain of IG

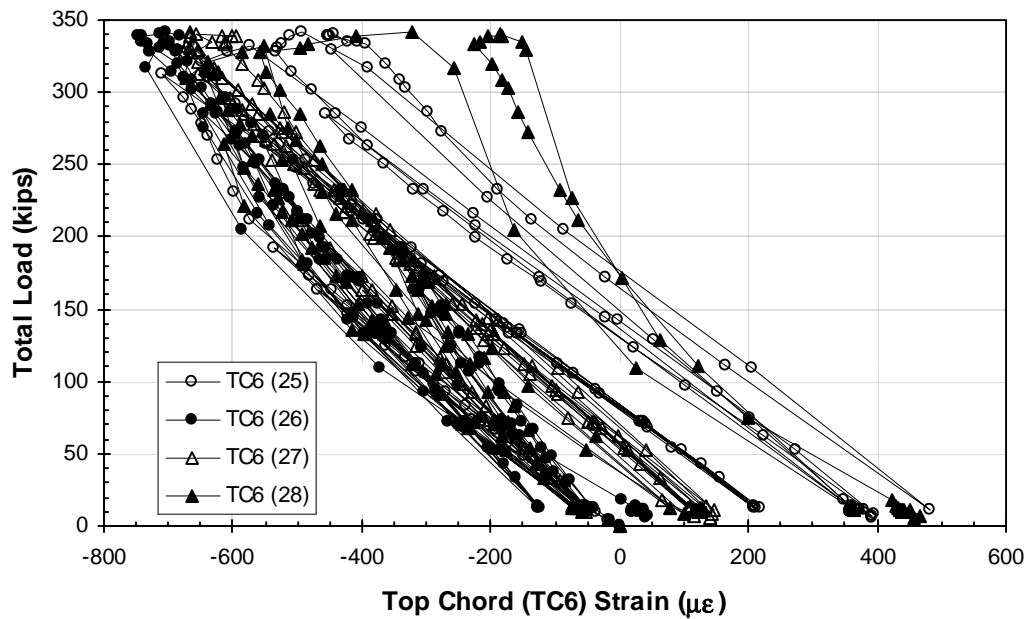
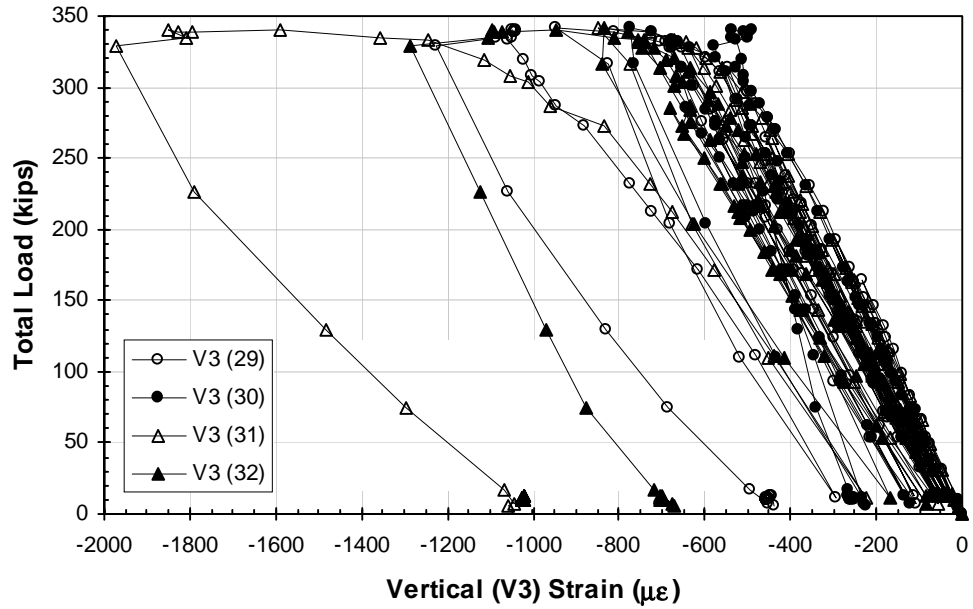
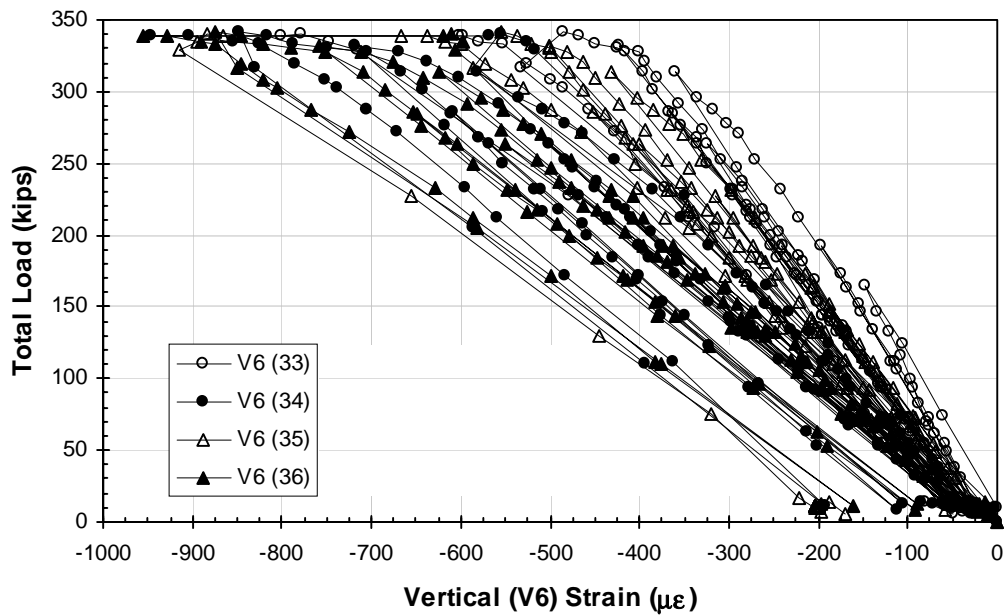


Figure B.2.12 Total Load vs. Top Chord (TC6) Strain of IG



**Figure B.2.13 Total Load vs. Vertical (V3) Strain of IG**



**Figure B.2.14 Total Load vs. Vertical (V6) Strain of IG**

## COMPOSITE FLUSH FRAMED JOIST-GIRDER TEST SUMMARY SHEET

GIRDER DESIGNATION: EGR(EG4)

TEST DATES: 28-30 November 1995

TEST DESCRIPTION				
<b>Joist-Girder:</b>	Span:	<u>30'-0"</u>	Weight:	<u>48.9 plf</u>
	Depth:	<u>30 in.</u>	Spacing:	<u>7 ft</u>
	Top Chord:	<u>2L-3.00x3.00x0.250</u>	Yield Stress:	<u>59.5 ksi</u>
	Bottom Chord:	<u>2L-4.00x4.00x0.375</u>	Yield Stress:	<u>60.0 ksi</u>
	<b>Deck:</b>	Type:	<u>2 VL</u>	Gage:
<b>Slab:</b>	Total Depth:	<u>5 in.</u>	Compressive Strength:	<u>4900 psi</u>
<b>Shear Connector:</b>	Type:	<u>3/4 in. x 4 1/2 in. Welded Headed Shear Studs</u>		
	Quantity:	<u>15 per half-span, 30 total</u>		

THEORETICAL CALCULATIONS	
Theoretical Max. Total Load on Joist-Girder:	<u>189.0 kips</u>
Theoretical Moment of Inertia:	<u>2705 in.<sup>4</sup></u>

TEST RESULTS	
Total Load on Joist-Girder at Failure:	<u>165.9 kips</u>
Maximum Total Load on Joist-Girder:	<u>172.9 kips</u>
Midspan Deflection at Failure:	<u>3.1 in.</u>
Experimental Moment of Inertia:	<u>2944 in.<sup>4</sup></u>
Mode of Failure:	<u>Compression buckling of web member W3R</u>

COMPARISON OF ACTUAL TO THEORETICAL	
<u>Maximum Total Load on Joist-Girder</u>	= 0.91
<u>Theoretical Max. Total Load on Joist-Girder</u>	

### LOCATION OF INSTRUMENTATION ON JOIST-GIRDER

WEST EAST

Location of Strain Gages on EGL Braces:

SOUTH NORTH

EGL Joist

**Strain Gages:**

①-4 BC	②1-24 TC5	E1 SLIP E1
⑤-8 TC1	②5-28 TC6	E2 SLIP E2
⑨-12 TC2	②9-32 V3	W1 SLIP W1
⑬-16 TC3	③3-36 V6	W2 SLIP W2
⑰-20 TC4	CONC CONCRETE	

**Slips:**

① LAT E\*  
② LAT W\*  
③ LAT M\*\*

\* Measured on EGL & EGR  
\*\* Measured on IG

Strain Gages on EGL Braces:

▽ BR E1   ▽ BR E2   ▽ BR W1   ▽ BR W2

Location of Strain Gages on Cross-Section:

West East North TC South

V3   V6   BC

TOP VIEW CROSS-SECTION

**Vertical Defl.:**

△ EQ BOTTOM  
△ CL BOTTOM  
△ CL TOP  
△ WQ BOTTOM

**Lateral Defl.:**

① LAT E\*  
② LAT W\*  
③ LAT M\*\*

\* Measured on EGL & EGR  
\*\* Measured on IG

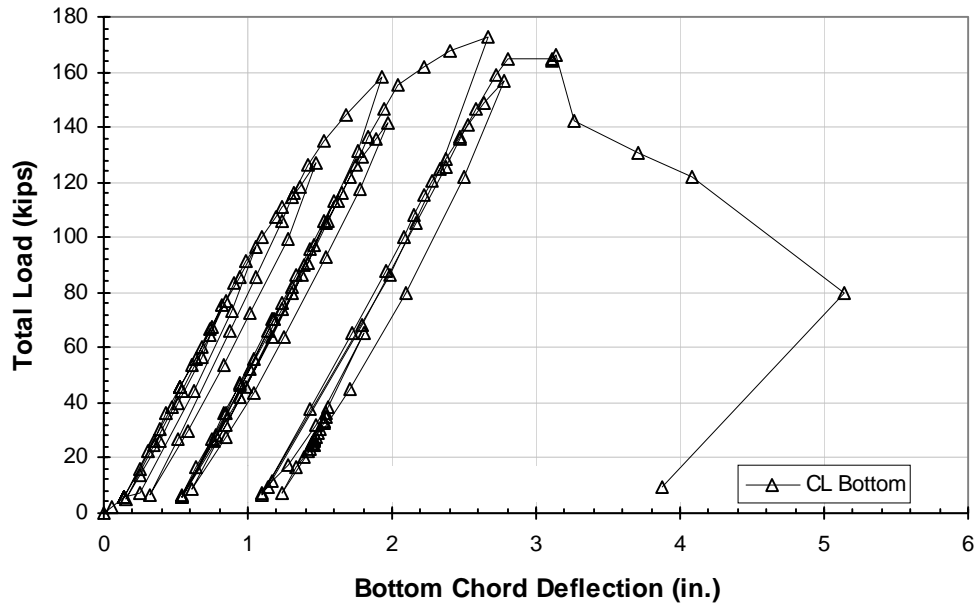


Figure B.3.1 Total Load vs. Bottom Chord Midspan Deflection of EGR

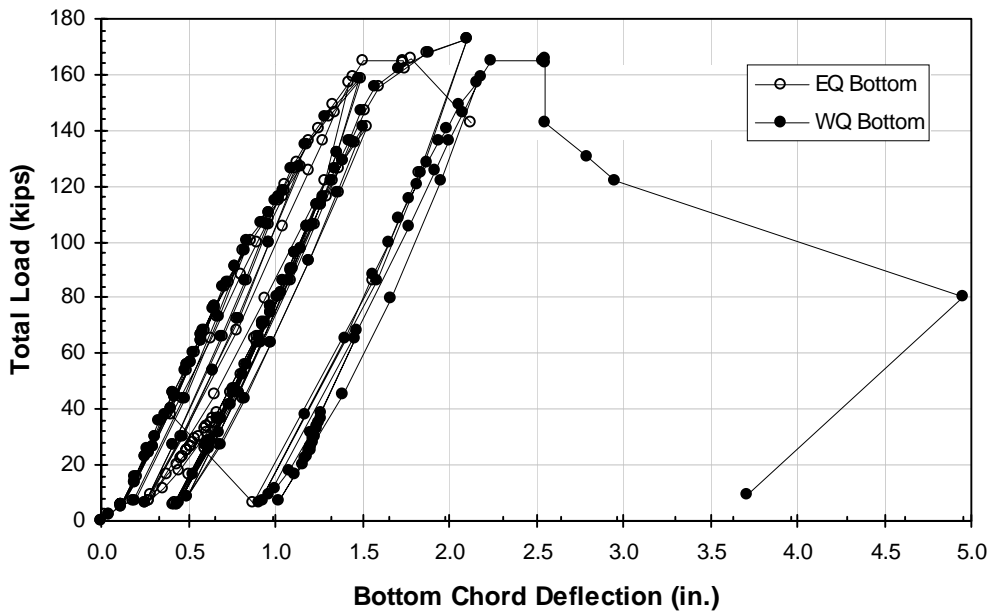
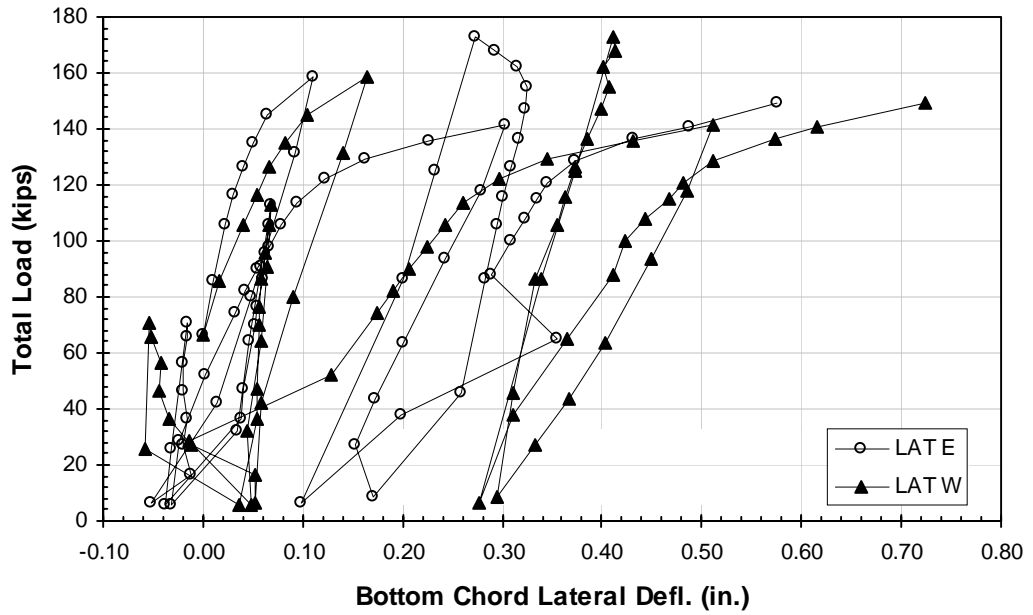
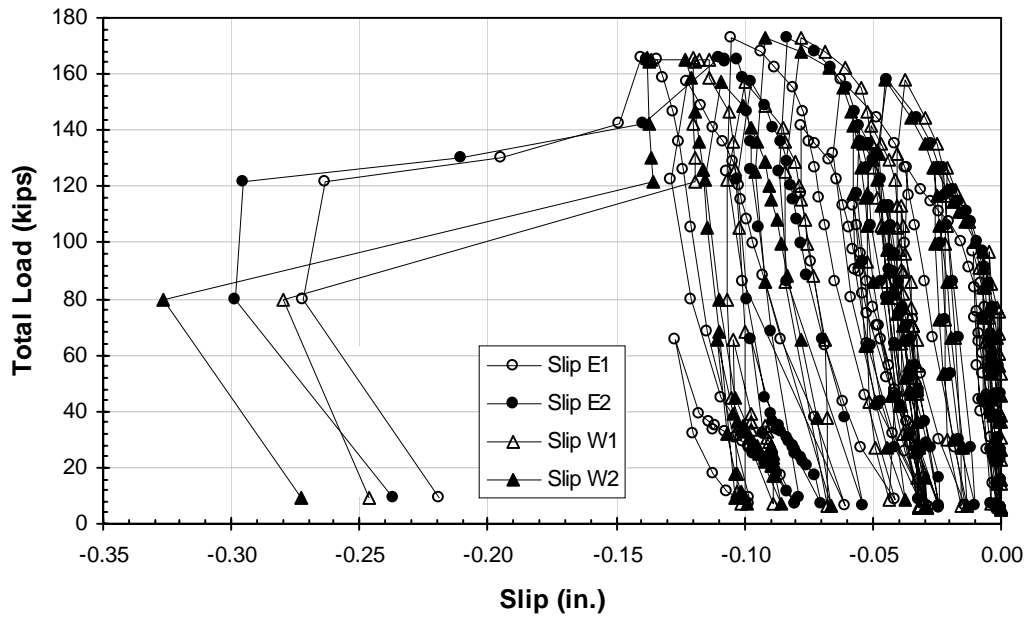


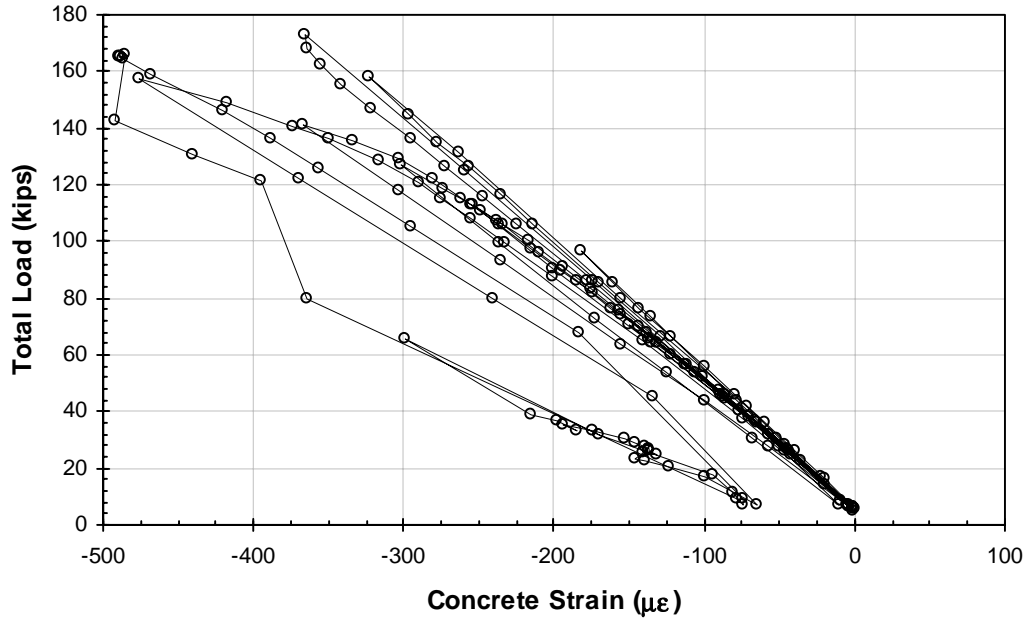
Figure B.3.2 Total Load vs. Bottom Chord Quarter Deflections of EGR



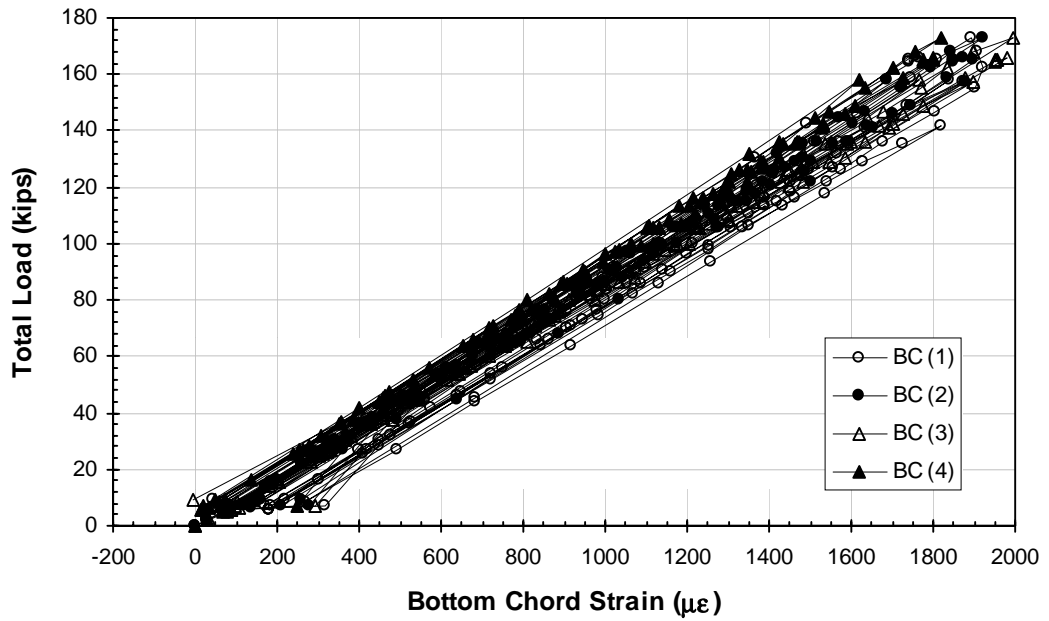
**Figure B.3.3 Total Load vs. Bottom Chord Lateral Deflections of EGR**



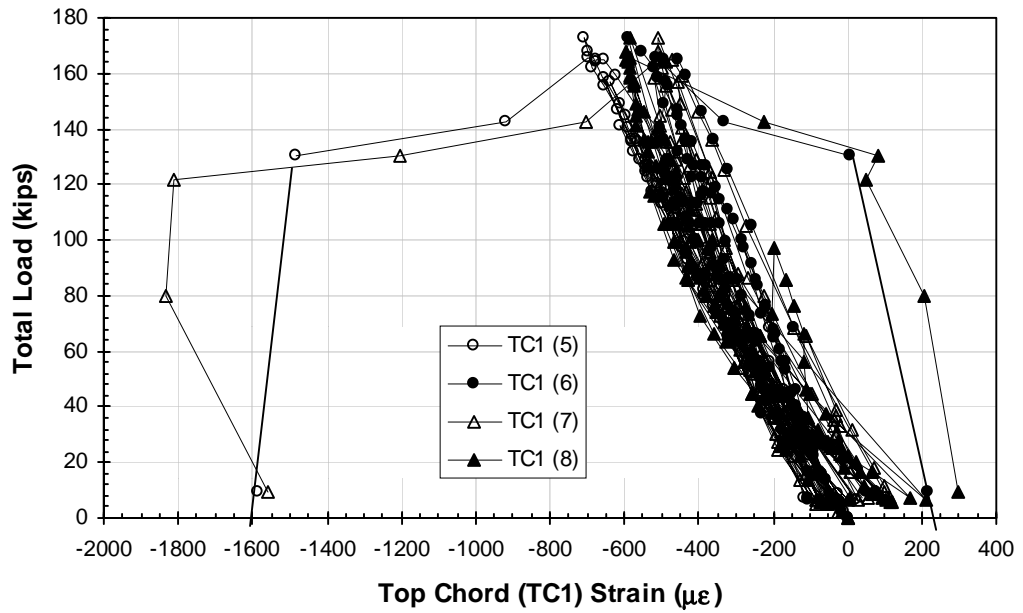
**Figure B.3.4 Total Load vs. Slip of EGR**



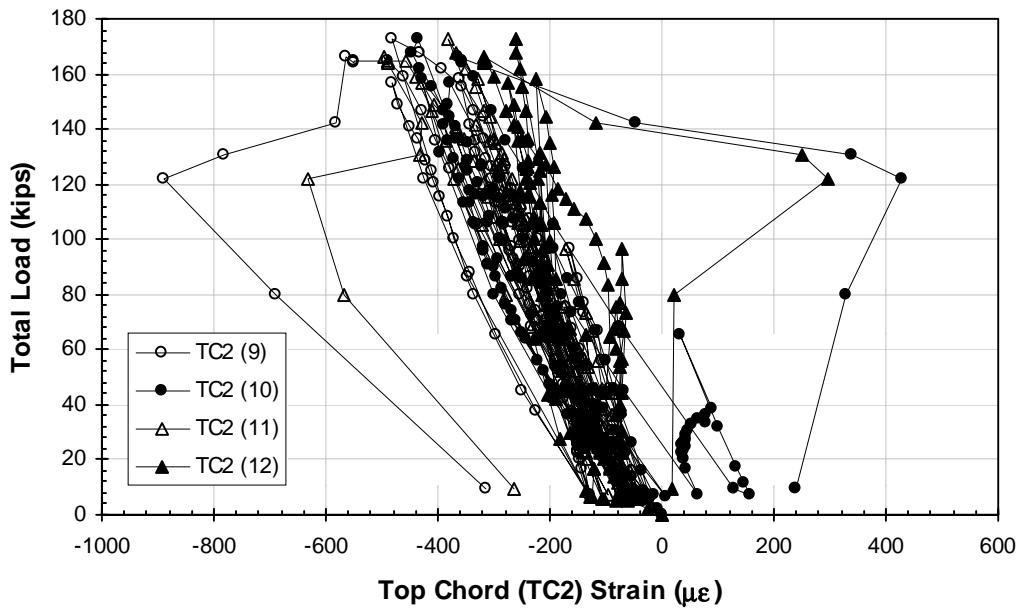
**Figure B.3.5 Total Load vs. Concrete Strain of EGR**



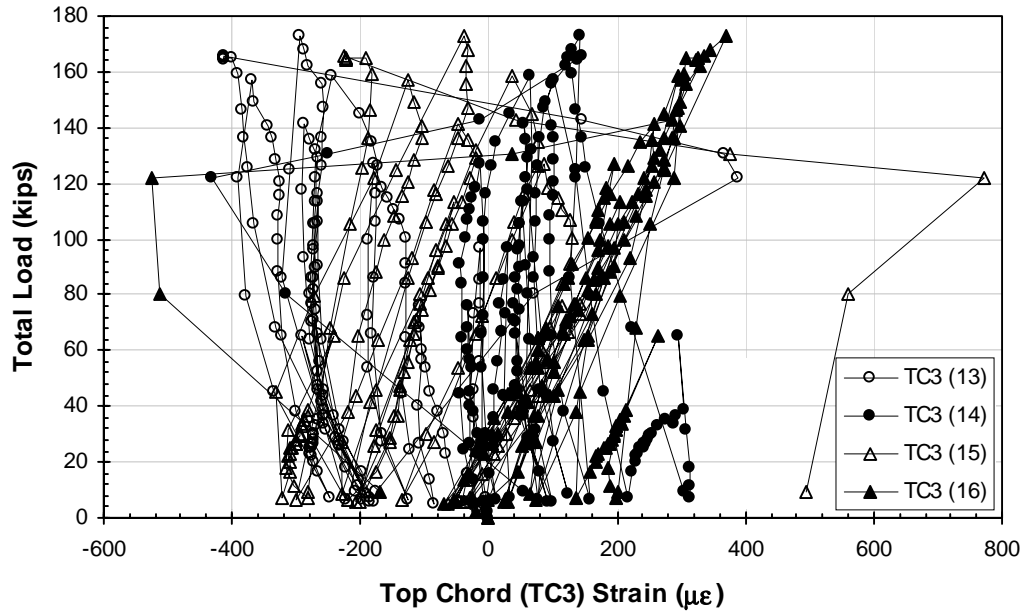
**Figure B.3.6 Total Load vs. Bottom Chord Strain of EGR**



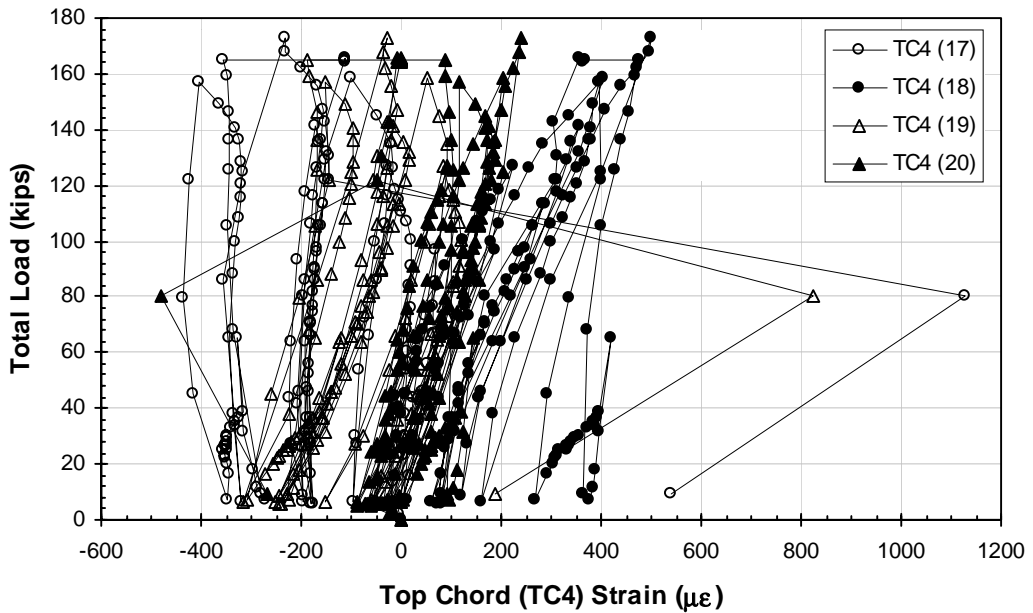
**Figure B.3.7 Total Load vs. Top Chord (TC1) Strain of EGR**



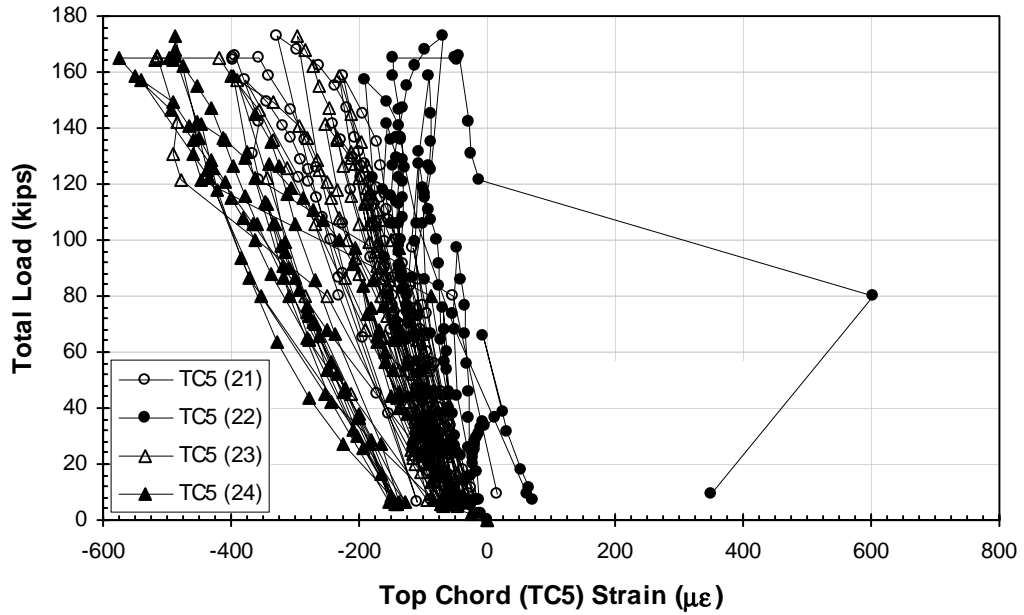
**Figure B.3.8 Total Load vs. Top Chord (TC2) Strain of EGR**



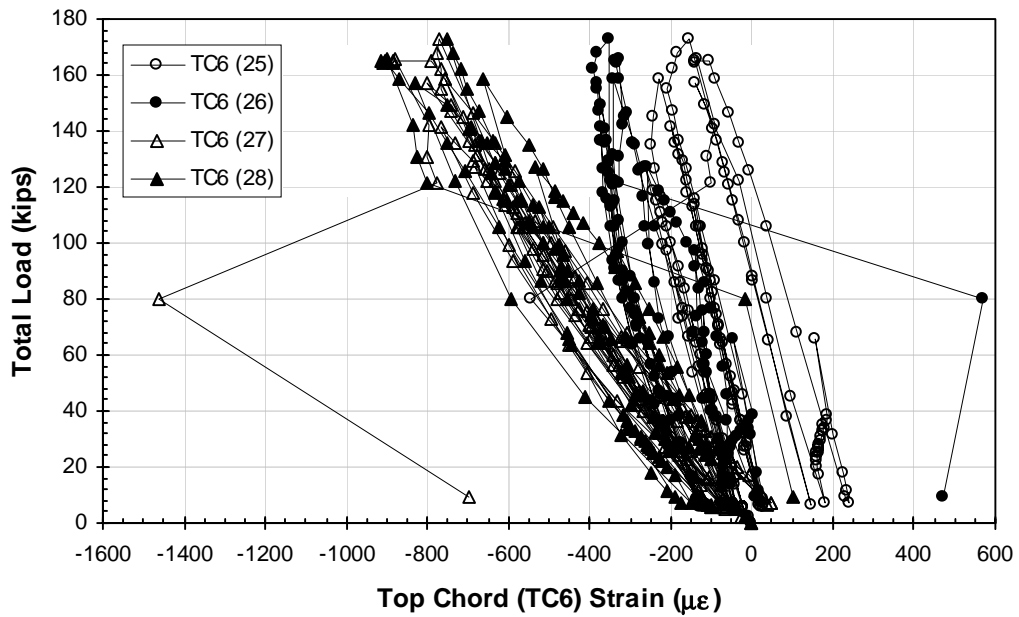
**Figure B.3.9 Total Load vs. Top Chord (TC3) Strain of EGR**



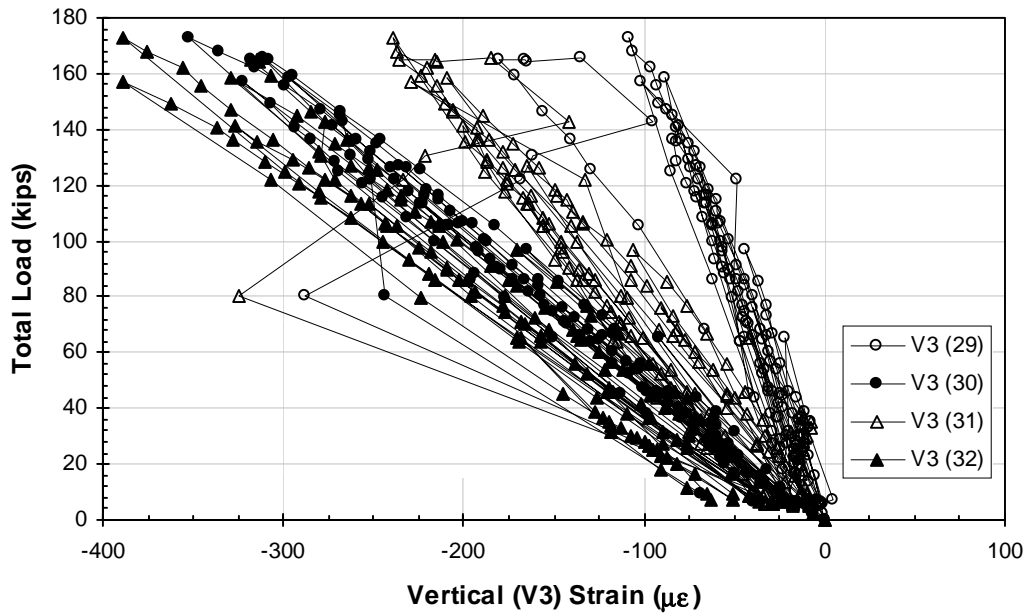
**Figure B.3.10 Total Load vs. Top Chord (TC4) Strain of EGR**



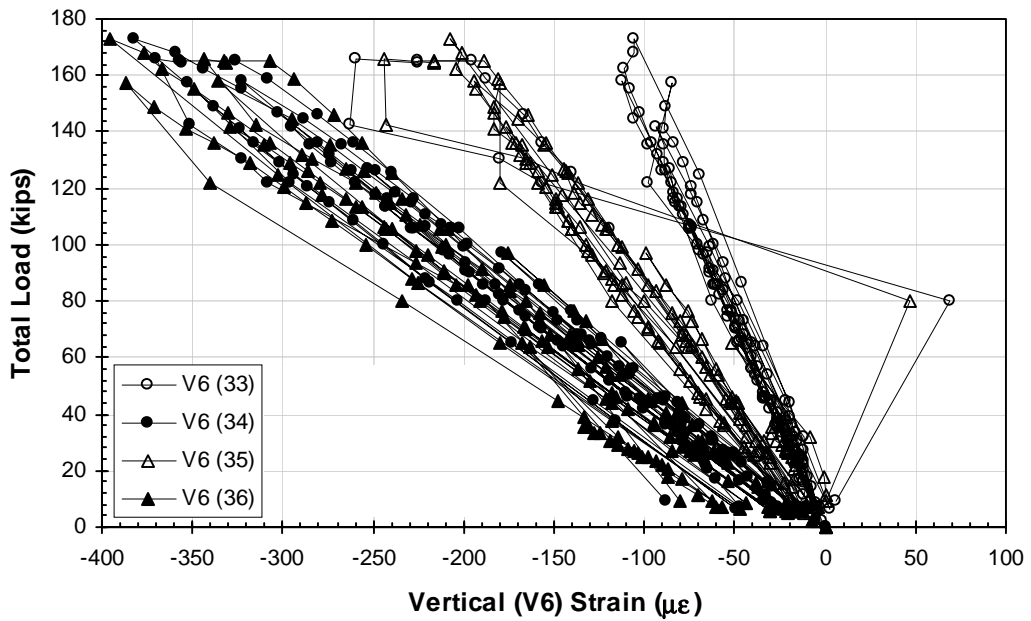
**Figure B.3.11 Total Load vs. Top Chord (TC5) Strain of EGR**



**Figure B.3.12 Total Load vs. Top Chord (TC6) Strain of EGR**



**Figure B.3.13 Total Load vs. Vertical (V3) Strain of EGR**



**Figure B.3.14 Total Load vs. Vertical (V6) Strain of EGR**

## COMPOSITE STUB JOIST-GIRDER TEST SUMMARY SHEET

GIRDER DESIGNATION: EGL

TEST DATES: 4-6 June 1996

TEST DESCRIPTION				
<b>Joist-Girder:</b>	Span:	<u>30'-0"</u>	Weight:	<u>52.8 plf</u>
	Depth:	<u>25 in.</u>	Spacing:	<u>7 ft</u>
	Top Chord:	<u>2L-3.00x3.00x0.250</u>	Yield Stress:	<u>50.1 ksi</u>
	Bottom Chord:	<u>2L-4.00x4.00x0.375</u>	Yield Stress:	<u>54.6 ksi</u>
	Stub:	<u>S5x10</u>	Yield Stress:	<u>49.0 ksi</u>
<b>Deck:</b>	Type:	<u>2 VL</u>	Gage:	<u>18 ga</u>
	Slab:	Total Depth: <u>5 in.</u>	Compressive Strength:	<u>3000 psi</u>
<b>Shear Connector:</b>	Type:	<u>3/4 in. x 4 1/2 in. Welded Headed Shear Studs</u>		
	Quantity:	<u>14 per half-span, 28 total</u>		

THEORETICAL CALCULATIONS	
Theoretical Max. Total Load per Joist-Girder:	<u>169.7 kips</u>
Theoretical Moment of Inertia:	<u>3077 in.<sup>4</sup></u>

TEST RESULTS	
Total Load per Joist-Girder at Failure:	<u>148.7 kips</u>
Maximum Total Load per Joist-Girder:	<u>148.7 kips</u>
Midspan Deflection at Failure:	<u>3.19 in.</u>
Experimental Moment of Inertia:	<u>3096 in.<sup>4</sup></u>
Mode of Failure:	<u>Loss of shear connection along east third of span</u>

COMPARISON OF ACTUAL TO THEORETICAL	
Maximum Total Load per Joist-Girder	= 0.88
Theoretical Max. Total Load per Joist-Girder	

### INSTRUMENTATION LOCATIONS

**Strain Gages:**

1-4 BC	25-28 TC6
5-8 TC1	
9-12 TC2	29-32 W5R
13-16 TC3	33-36 W5
17-20 TC4	
21-24 TC5	37-40 STUB

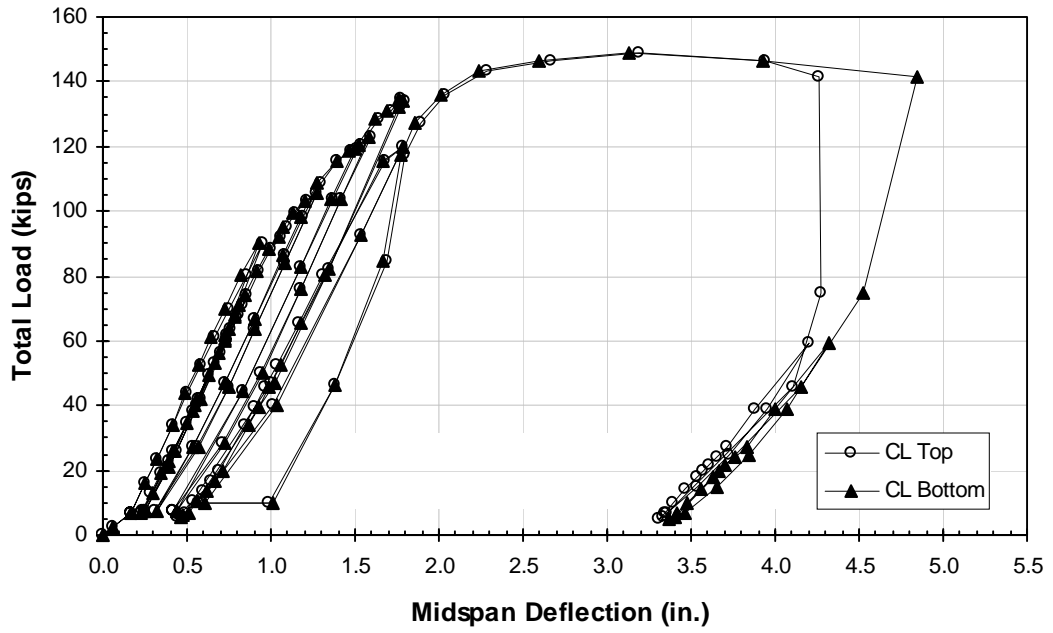
CL CONCRETE CL  
WT CONCRETE WT

Location of Strain Gages on Cross-Section:

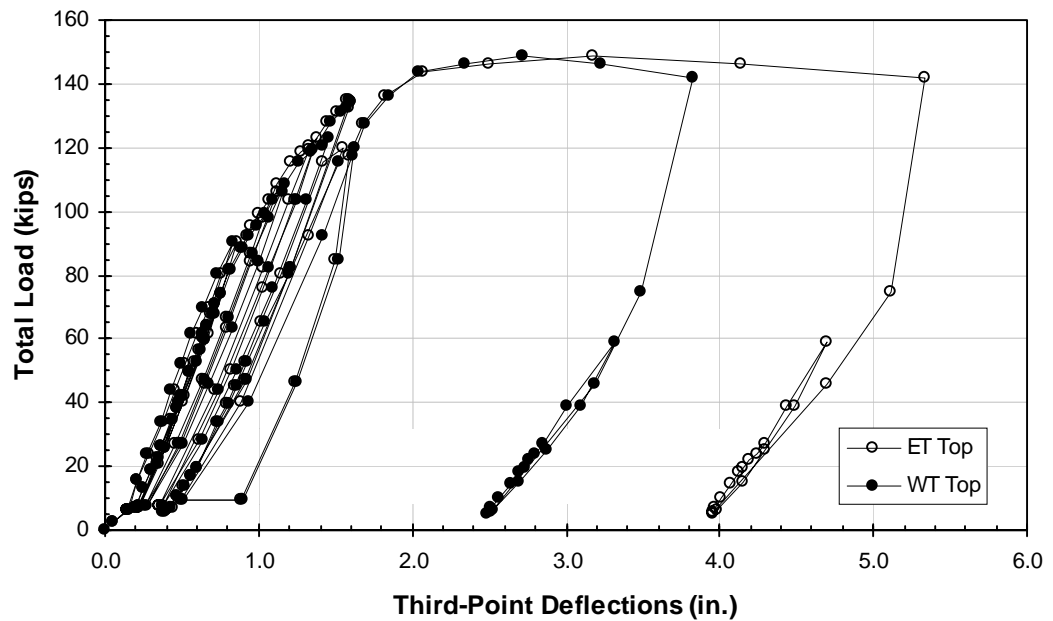
<p>STUB</p> <p>CROSS-SECTION</p>	<p>WEB</p> <p>CROSS-SECTION</p>	<p>TC &amp; BC</p> <p>CROSS-SECTION</p>
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**Slips:**      **Vert. Defl.:**

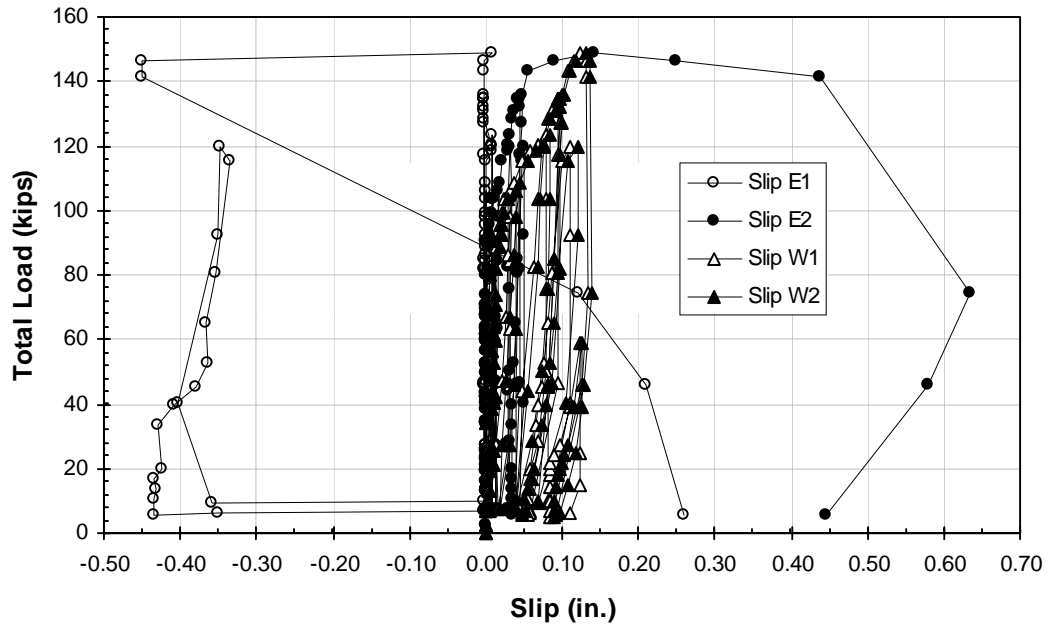
E1 SLIP-E1	△ ET TOP
E2 SLIP-E2	△ CL TOP
W1 SLIP-W1	△ CL BOTTOM
W2 SLIP-W2	△ WT TOP



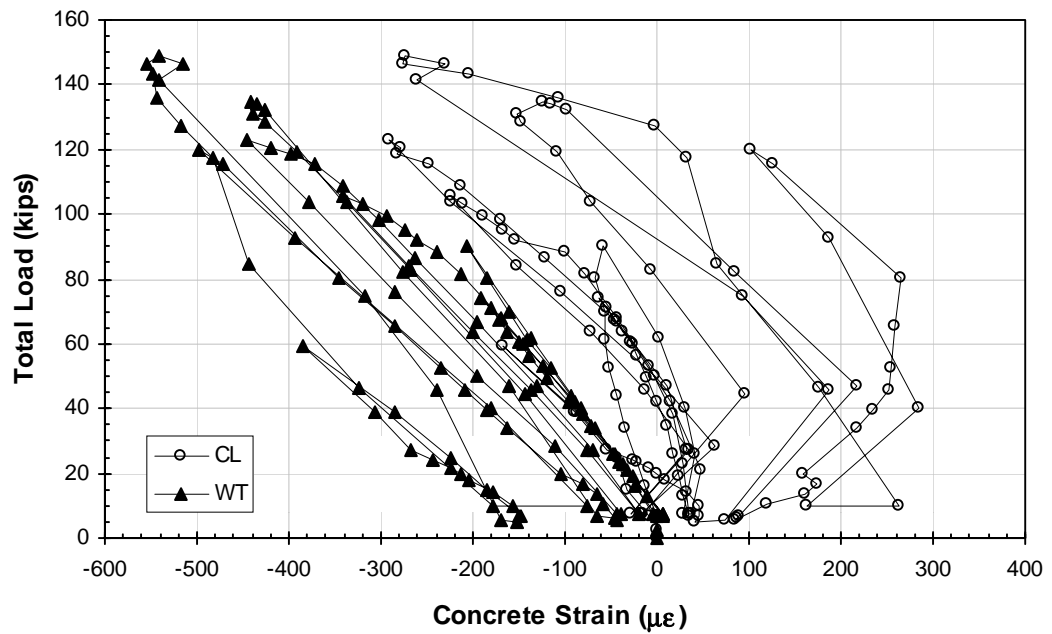
**Figure B.4.1 Total Load vs. Midspan Deflections of EGL**



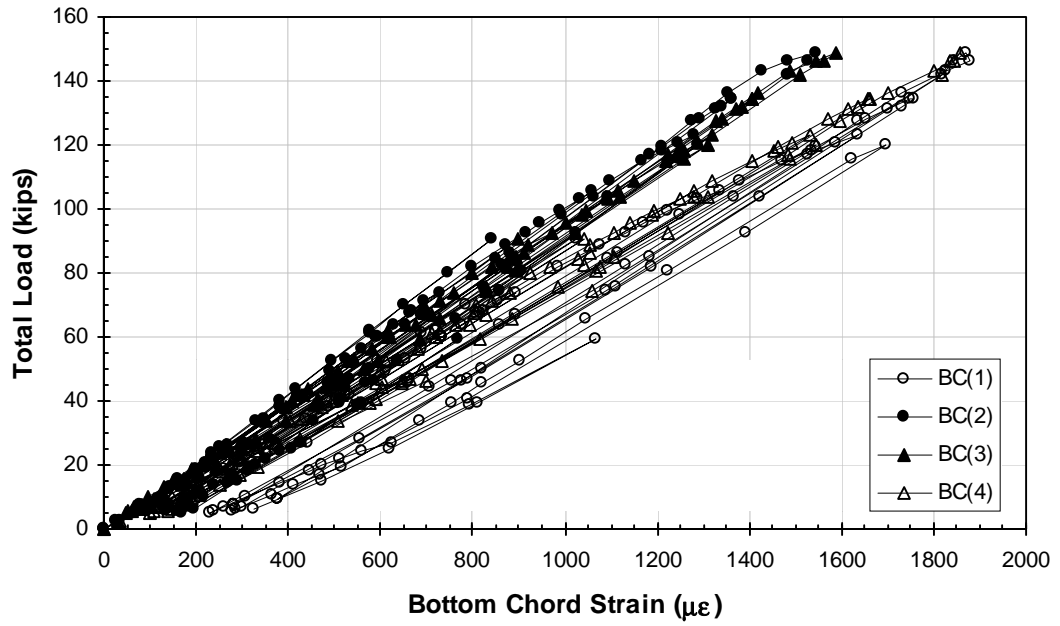
**Figure B.4.2 Total Load vs. Third-Point Deflections of EGL**



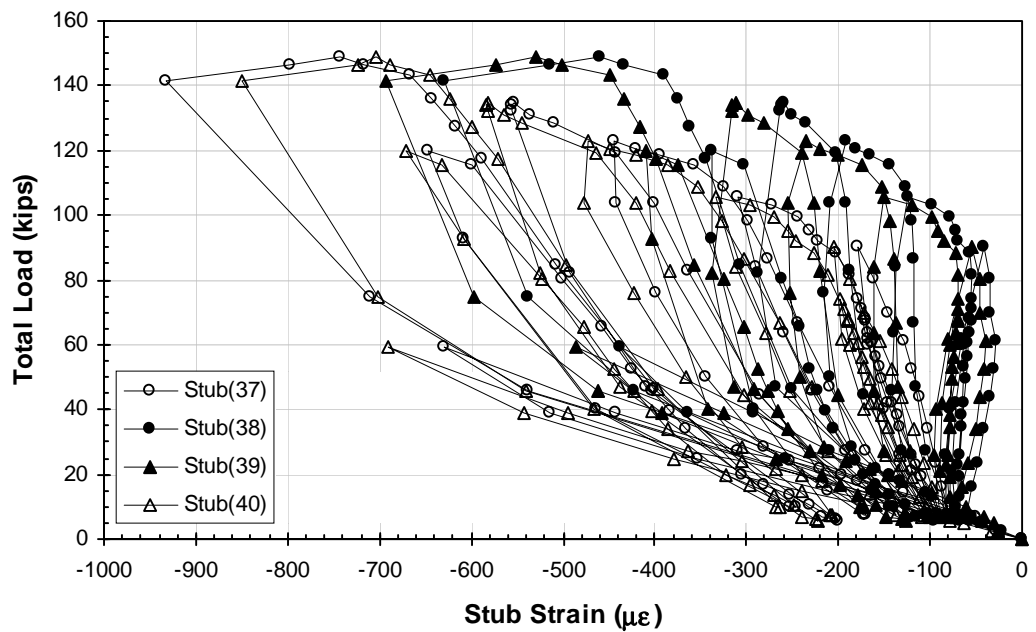
**Figure B.4.3 Total Load vs. Slip of EGL**



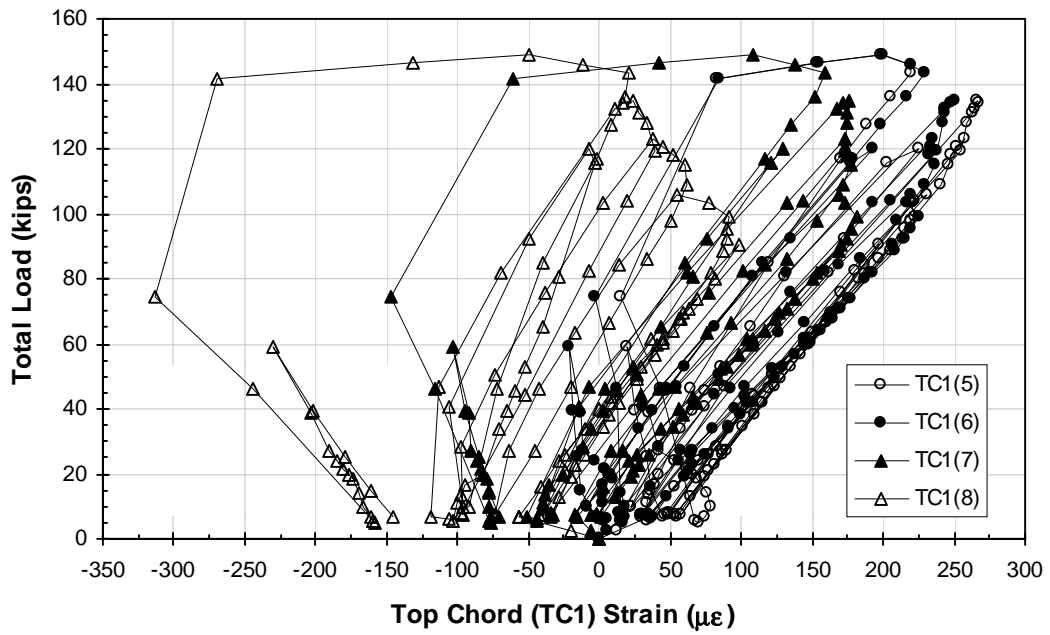
**Figure B.4.4 Total Load vs. Concrete Strain of EGL**



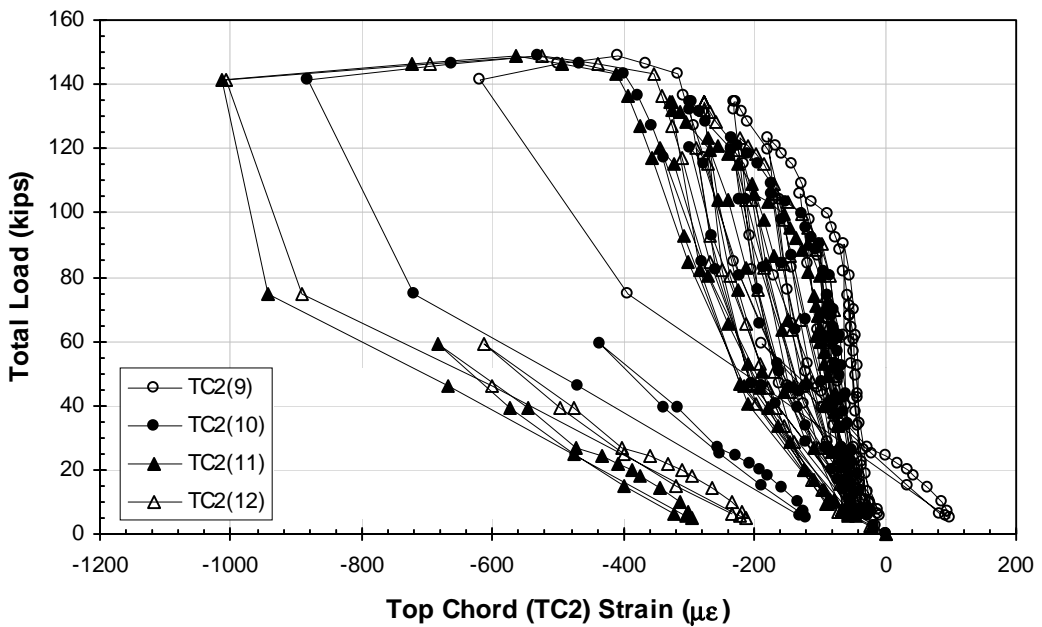
**Figure B.4.5 Total Load vs. Bottom Chord Strain of EGL**



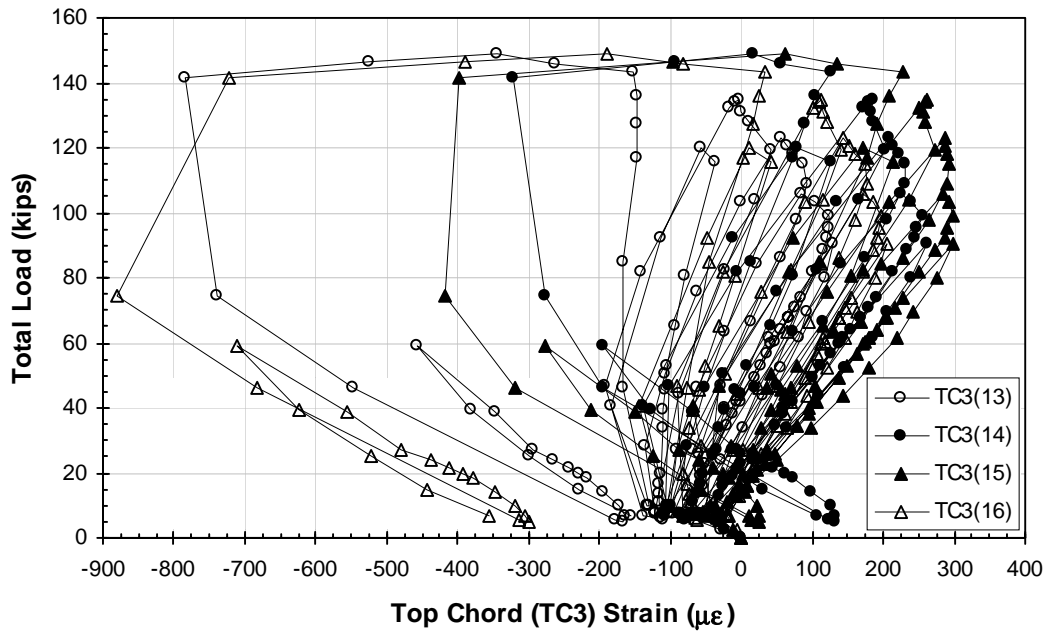
**Figure B.4.6 Total Load vs. Stub Strain of EGL**



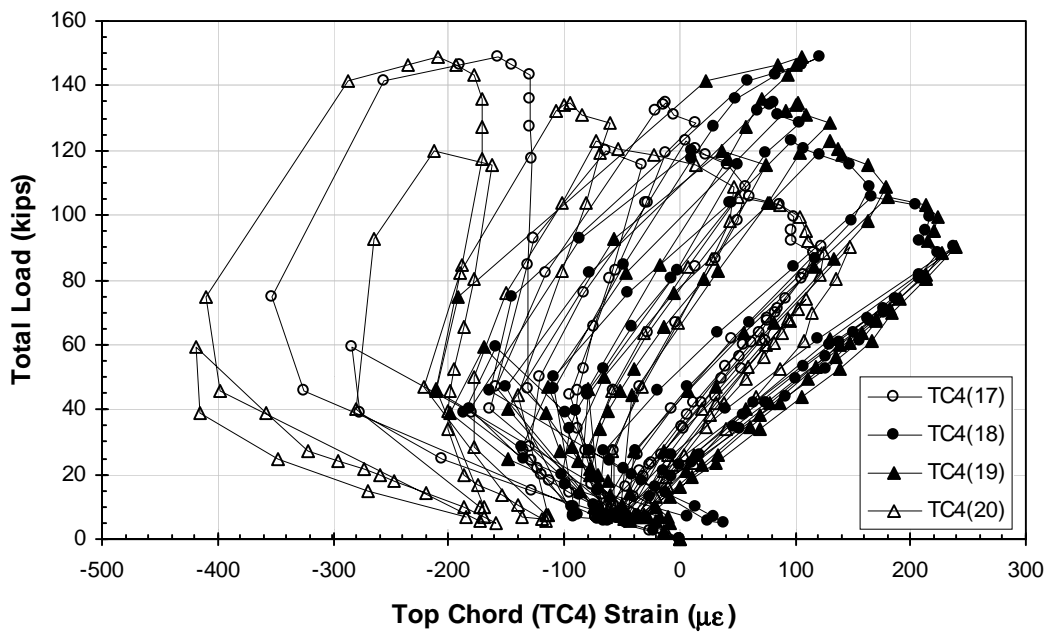
**Figure B.4.7 Total Load vs. Top Chord (TC1) Strain of EGL**



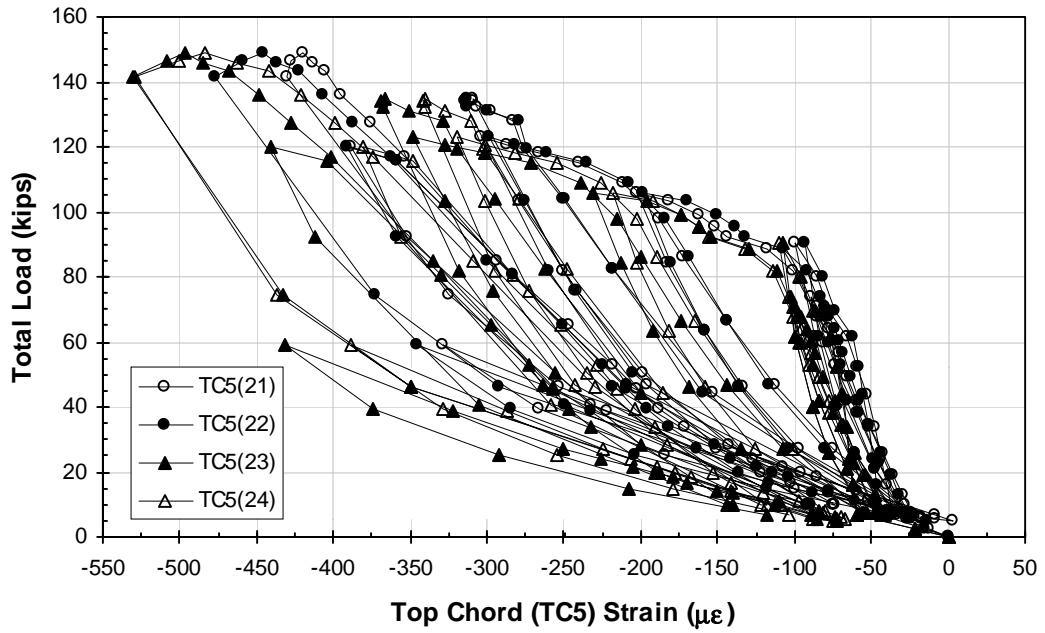
**Figure B.4.8 Total Load vs. Top Chord (TC2) Strain of EGL**



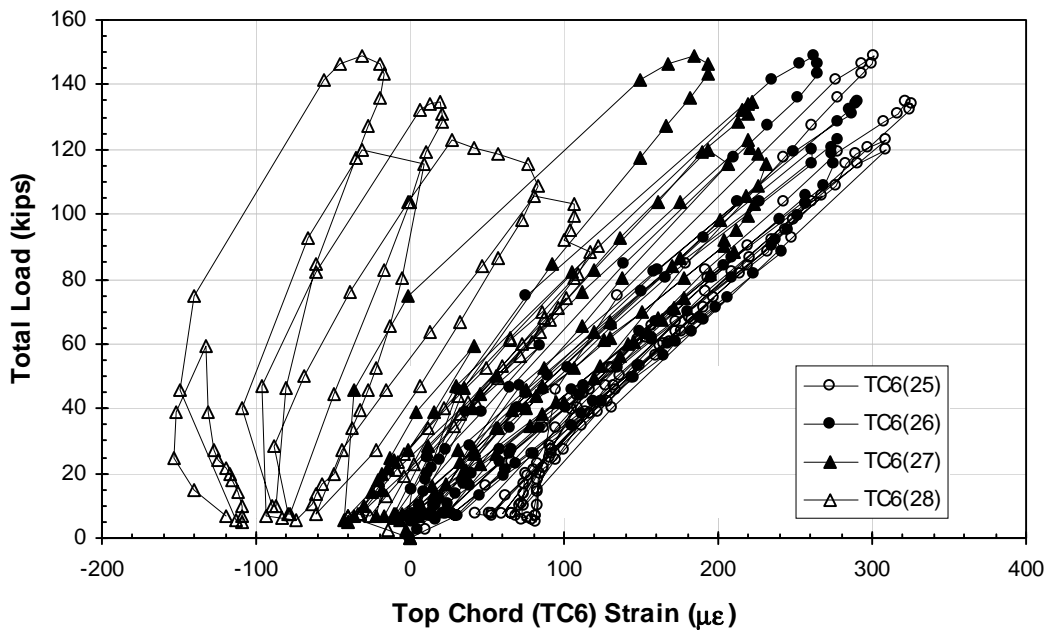
**Figure B.4.9 Total Load vs. Top Chord (TC3) Strain of EGL**



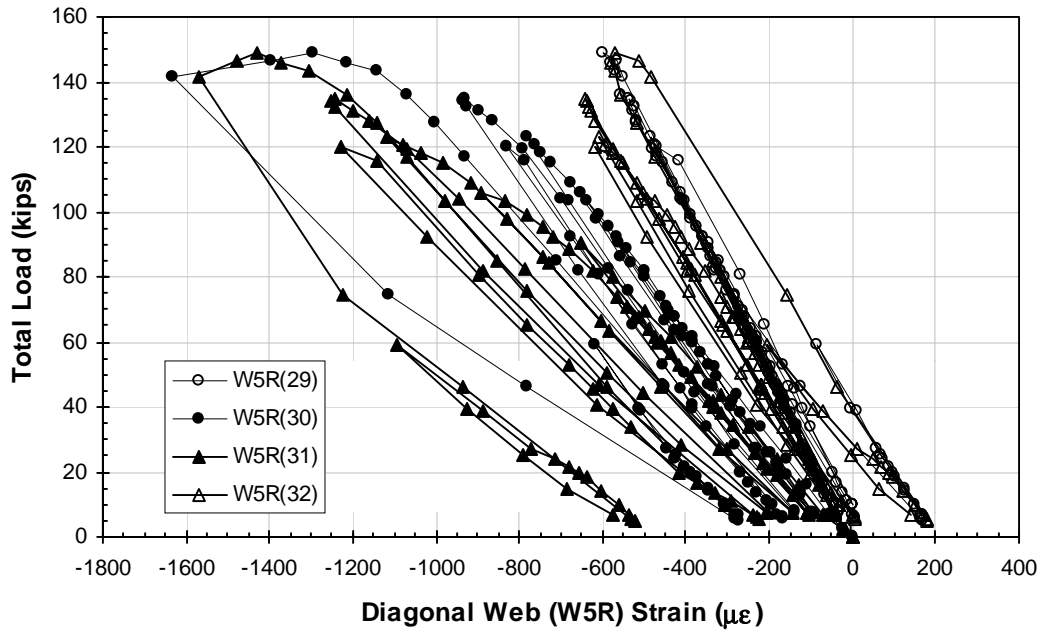
**Figure B.4.10 Total Load vs. Top Chord (TC4) Strain of EGL**



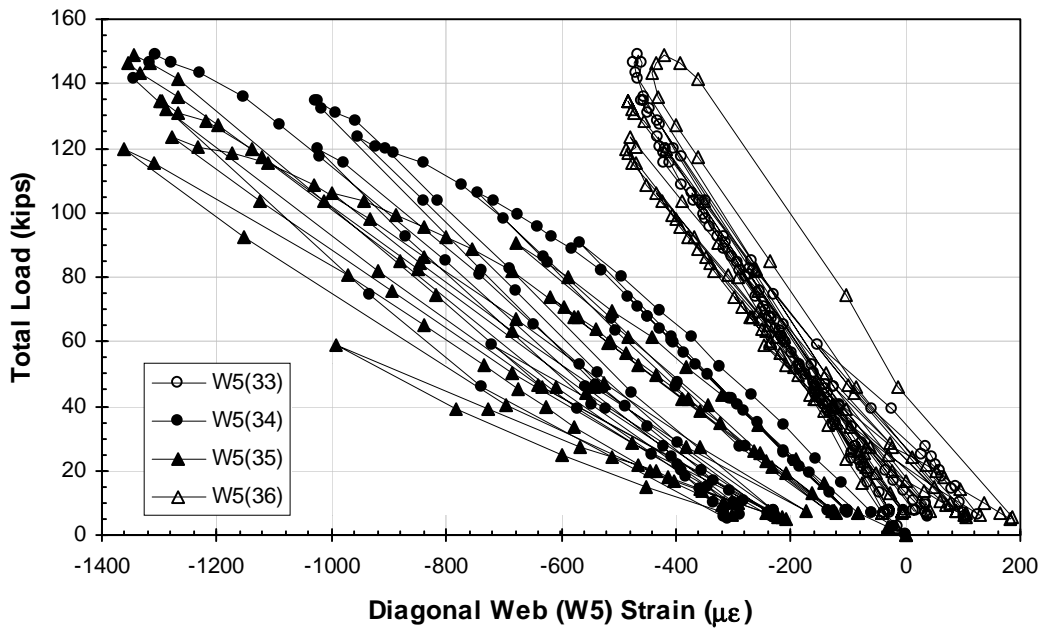
**Figure B.4.11 Total Load vs. Top Chord (TC5) Strain of EGL**



**Figure B.4.12 Total Load vs. Top Chord (TC6) Strain of EGL**



**Figure B.4.13 Total Load vs. Diagonal Web (W5R) Strain of EGL**



**Figure B.4.14 Total Load vs. Diagonal Web (W5) Strain of EGL**

## COMPOSITE STUB JOIST-GIRDER TEST SUMMARY SHEET

GIRDER DESIGNATION: IG

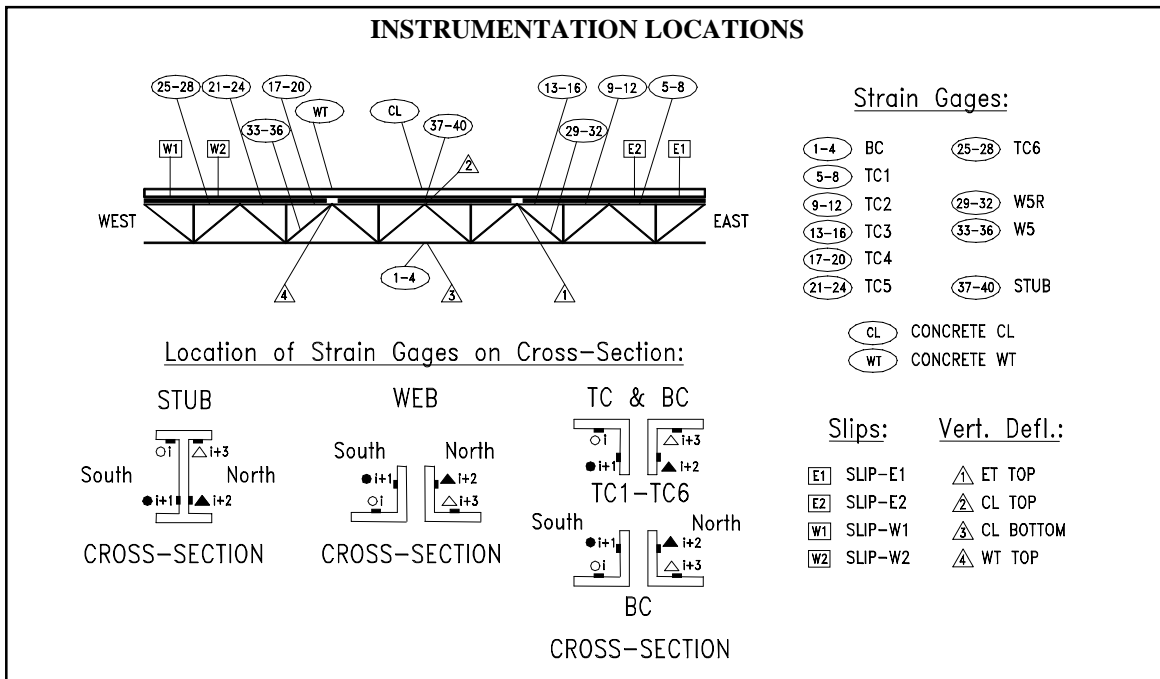
TEST DATES: 4-6 June 1996

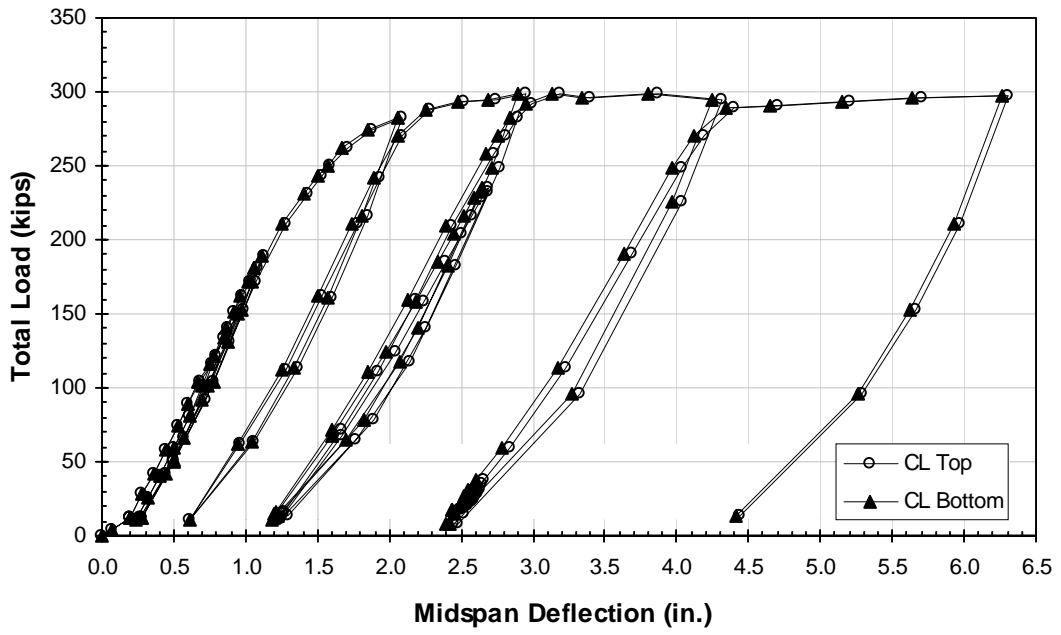
TEST DESCRIPTION				
<b>Joist-Girder:</b>	Span:	<u>30'-0"</u>	Weight:	<u>94.4 plf</u>
	Depth:	<u>25 in.</u>	Spacing:	<u>7 ft</u>
	Top Chord:	<u>2L-4.00x4.00x0.375</u>		
	Bottom Chord:	<u>2L-5.00x5.00x0.625</u>	Yield Stress:	<u>59.4 ksi</u>
	Stub:	<u>S5x10</u>		
<b>Deck:</b>	Type:	<u>2 VL</u>	Gage:	<u>18 ga</u>
<b>Slab:</b>	Total Depth:	<u>5 in.</u>	Compressive Strength:	<u>3000 psi</u>
<b>Shear Connector:</b>	Type:	<u>3/4 in. x 4 1/2 in. Welded Headed Shear Studs</u>		
	Quantity:	<u>28 per half-span, 56 total</u>		

THEORETICAL CALCULATIONS	
Theoretical Max. Total Load on Joist-Girder:	<u>370.6 kips</u>
Theoretical Moment of Inertia:	<u>5930 in.<sup>4</sup></u>

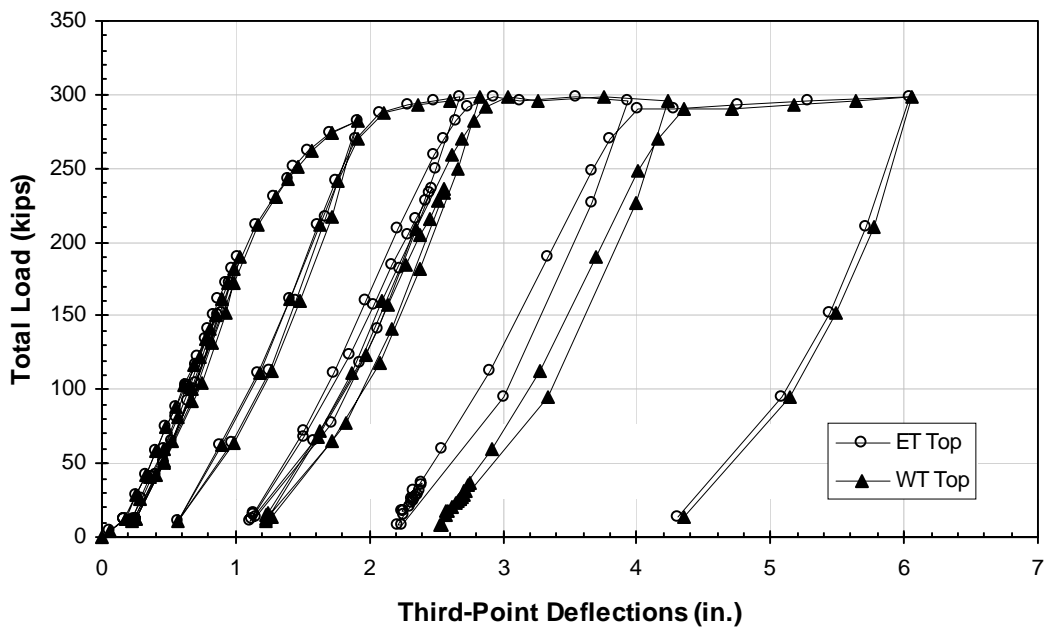
TEST RESULTS	
Total Load on Joist-Girder at Failure:	<u>299.0 kips</u>
Maximum Total Load on Joist-Girder:	<u>299.0 kips</u>
Midspan Deflection at Failure:	<u>3.87 in.</u>
Experimental Moment of Inertia:	<u>5709 in.<sup>4</sup></u>
Mode of Failure:	<u>Crushing of concrete at load points</u>

COMPARISON OF ACTUAL TO THEORETICAL	
Maximum Total Load on Joist-Girder	= 0.81
Theoretical Max. Total Load on Joist-Girder	

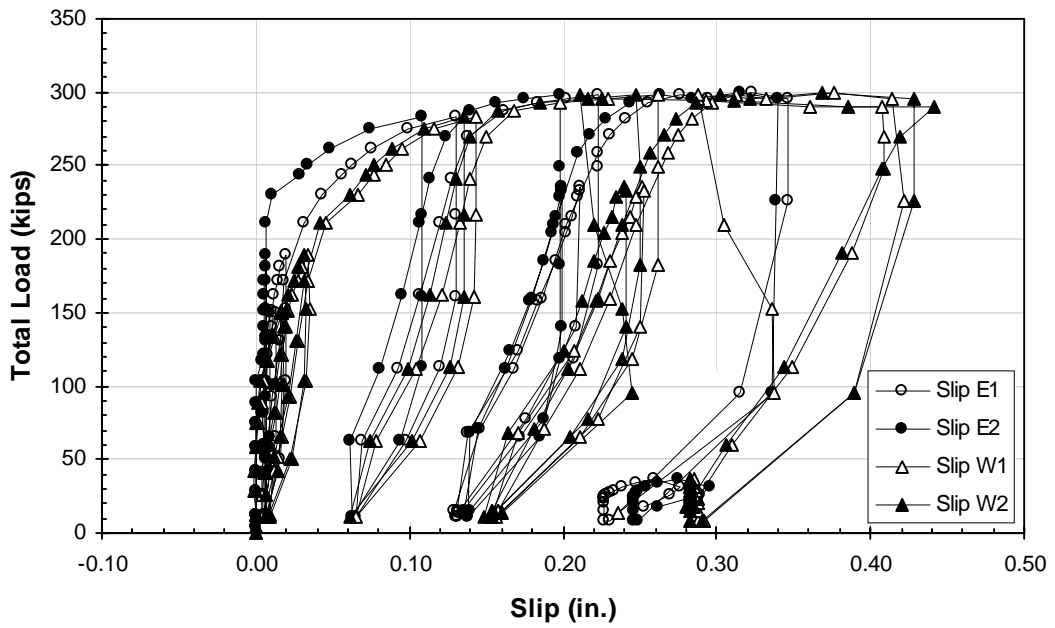




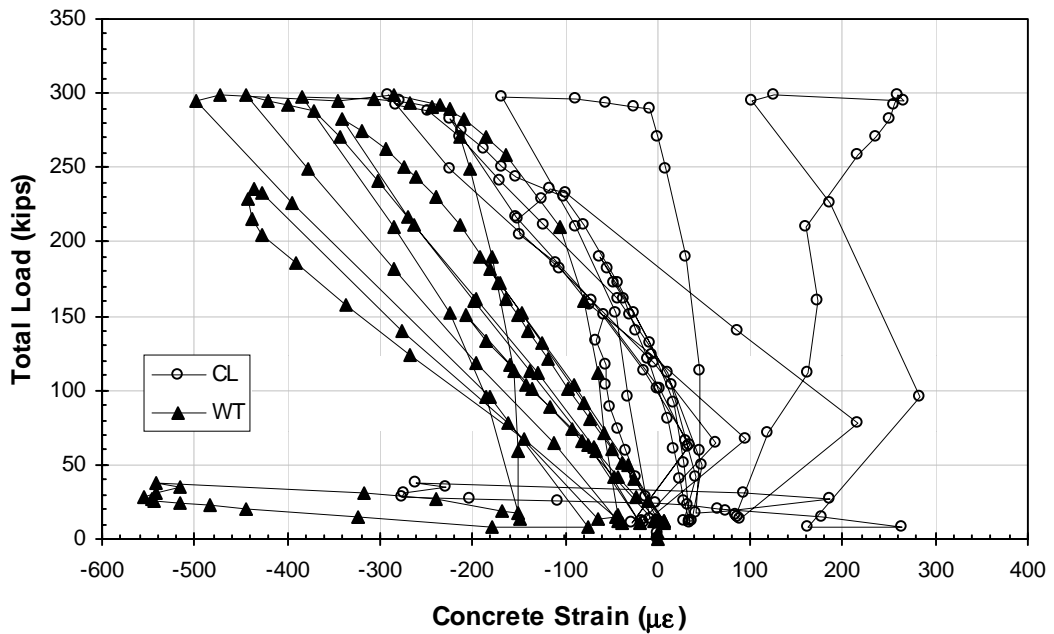
**Figure B.5.1 Total Load vs. Midspan Deflections of IG**



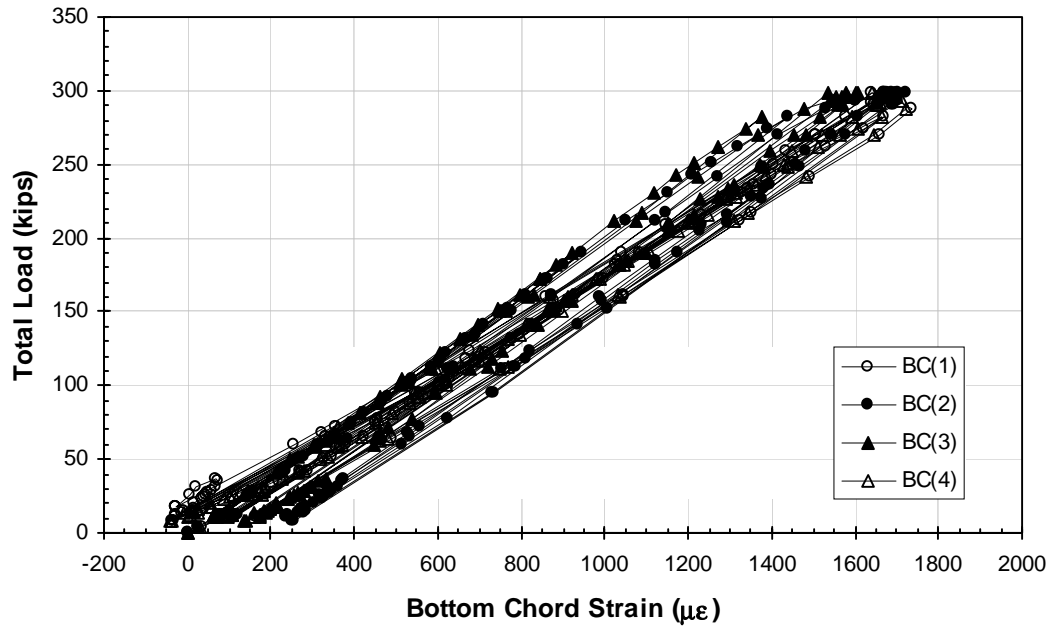
**Figure B.5.2 Total Load vs. Third-Point Deflections of IG**



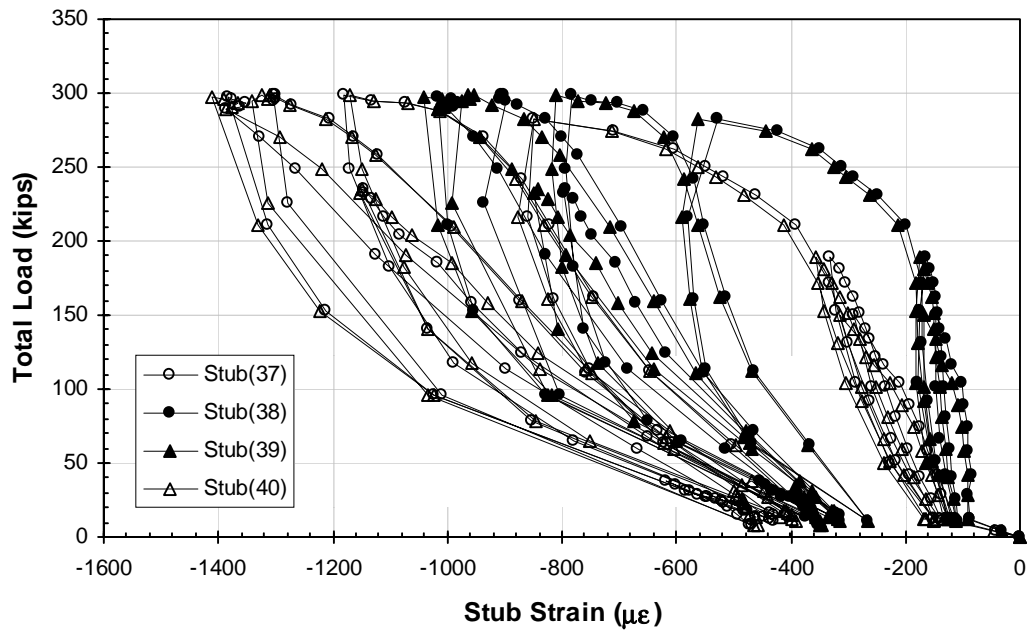
**Figure B.5.3 Total Load vs. Slip of IG**



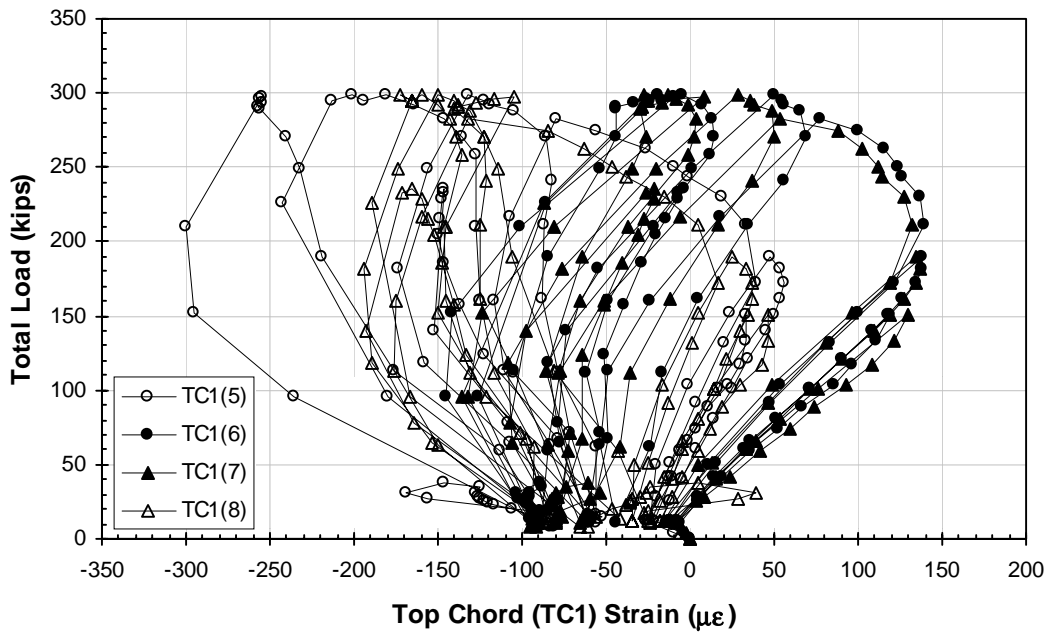
**Figure B.5.4 Total Load vs. Concrete Strain of IG**



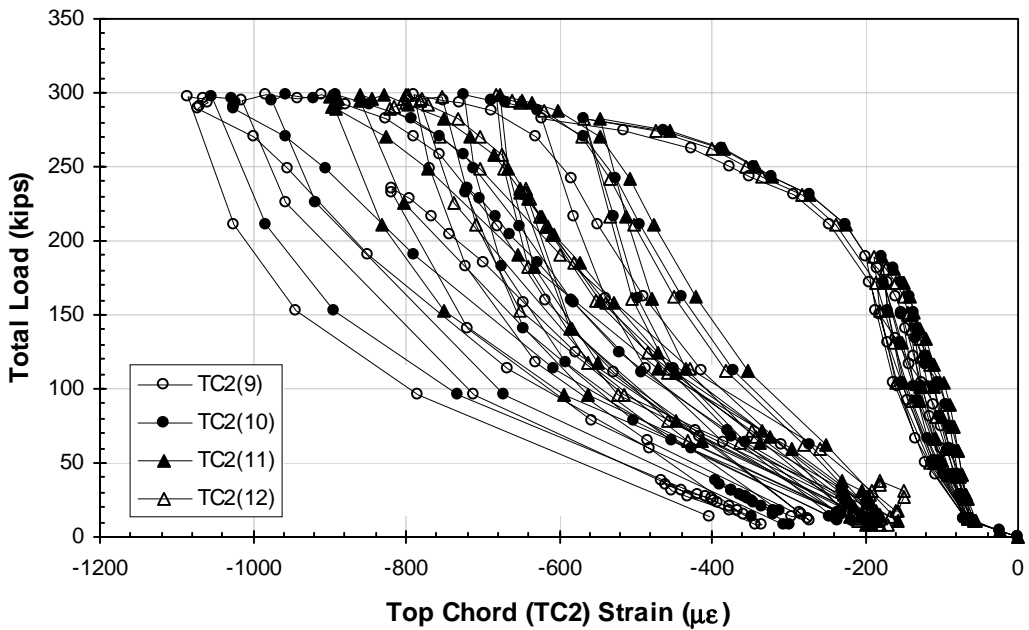
**Figure B.5.5 Total Load vs. Bottom Chord Strain of IG**



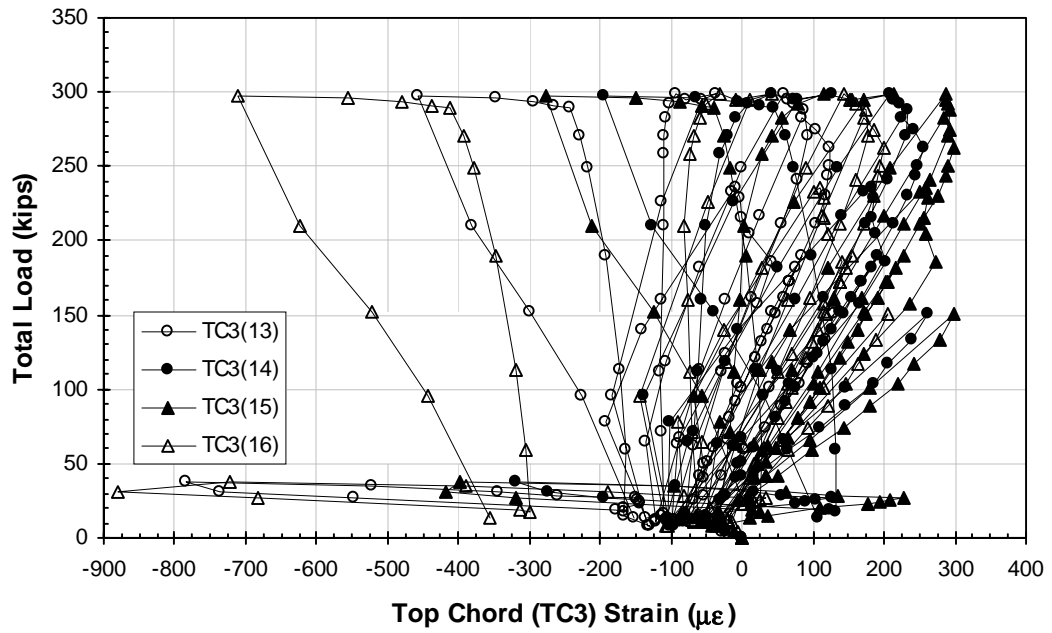
**Figure B.5.6 Total Load vs. Stub Strain of IG**



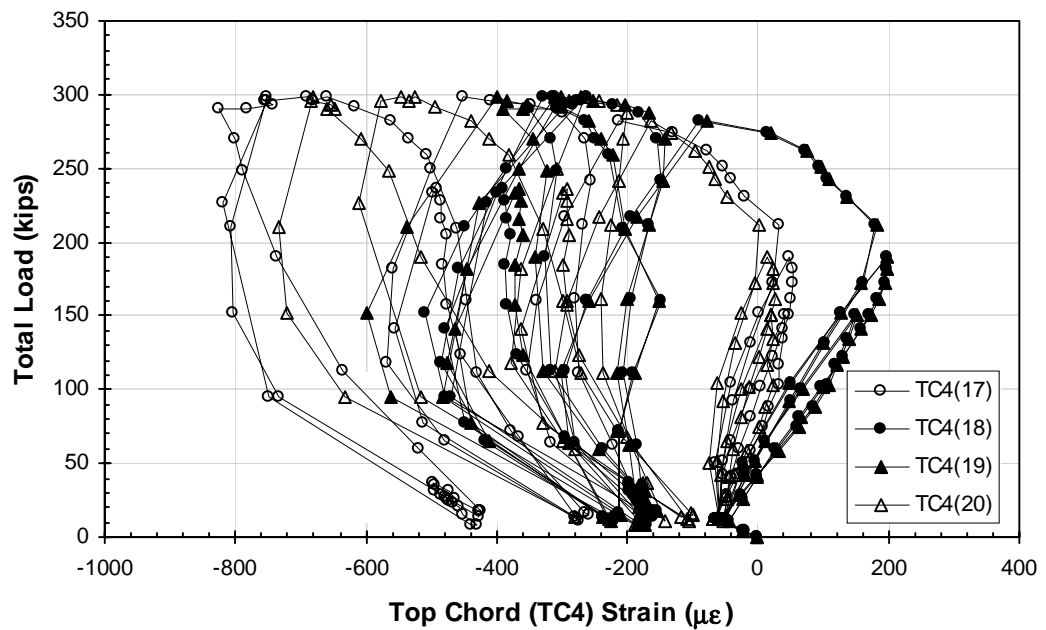
**Figure B.5.7 Total Load vs. Top Chord (TC1) Strain of IG**



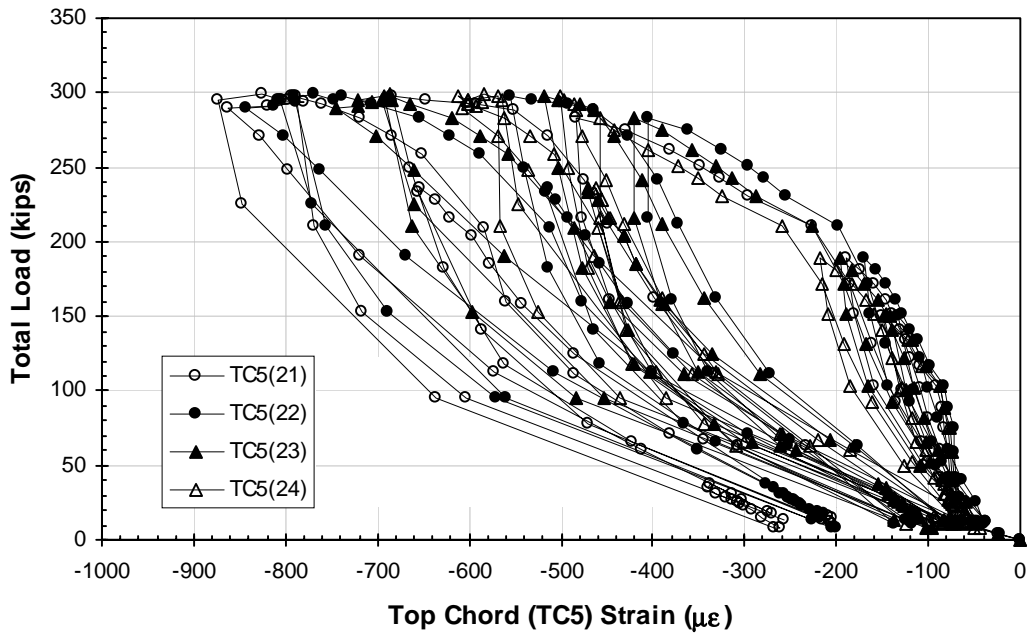
**Figure B.5.8 Total Load vs. Top Chord (TC2) Strain of IG**



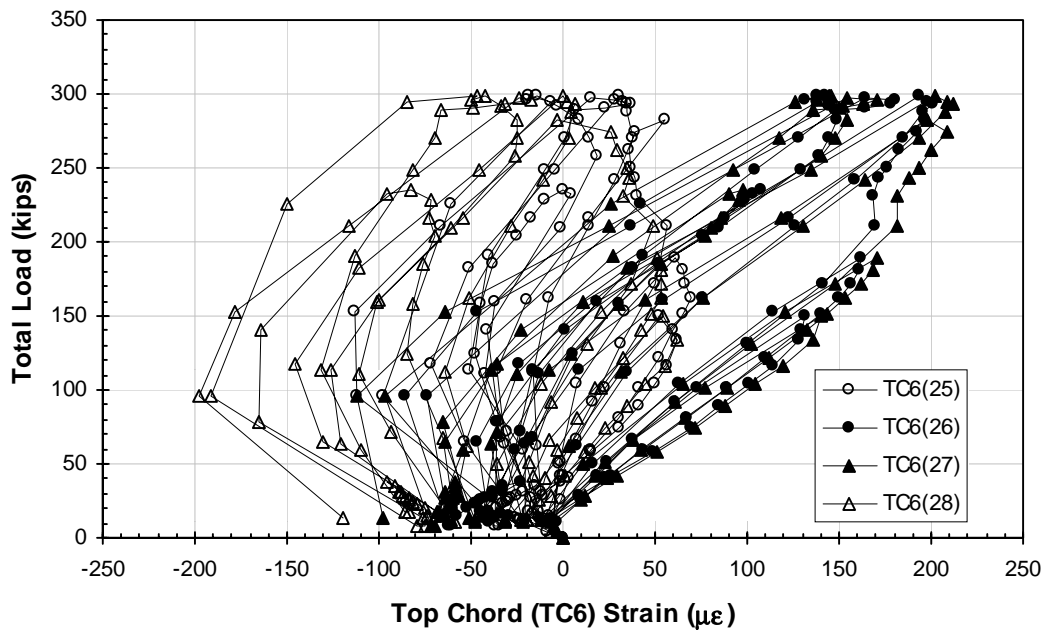
**Figure B.5.9 Total Load vs. Top Chord (TC3) Strain of IG**



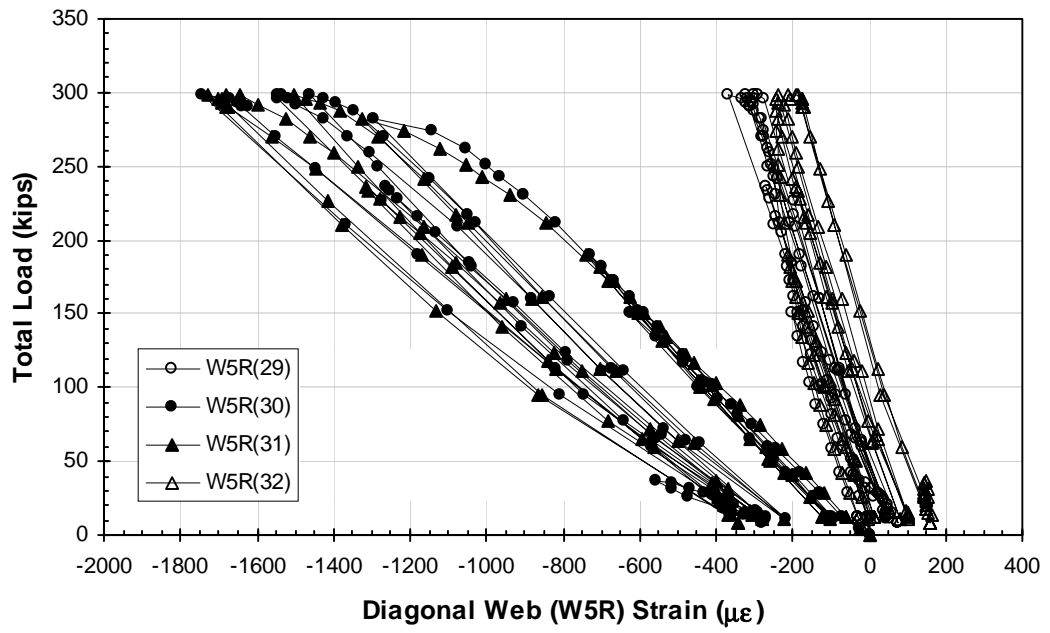
**Figure B.5.10 Total Load vs. Top Chord (TC4) Strain of IG**



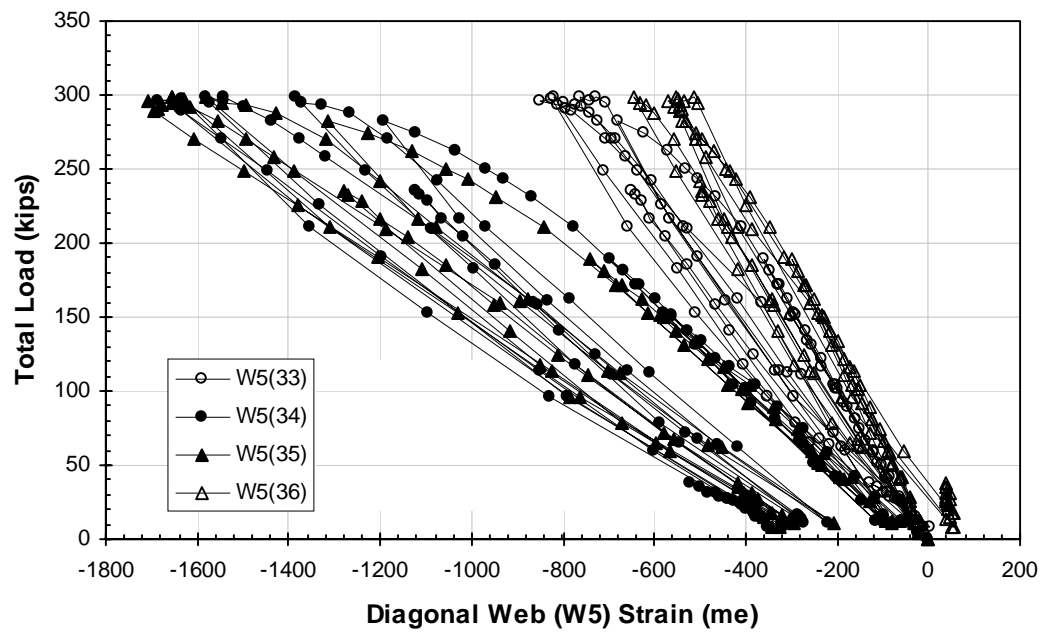
**Figure B.5.11 Total Load vs. Top Chord (TC5) Strain of IG**



**Figure B.5.12 Total Load vs. Top Chord (TC6) Strain of IG**



**Figure B.5.13 Total Load vs. Diagonal Web (W5R) Strain of IG**



**Figure B.5.14 Total Load vs. Diagonal Web (W5) Strain of IG**

## COMPOSITE STUB JOIST-GIRDER TEST SUMMARY SHEET

GIRDER DESIGNATION: EGR

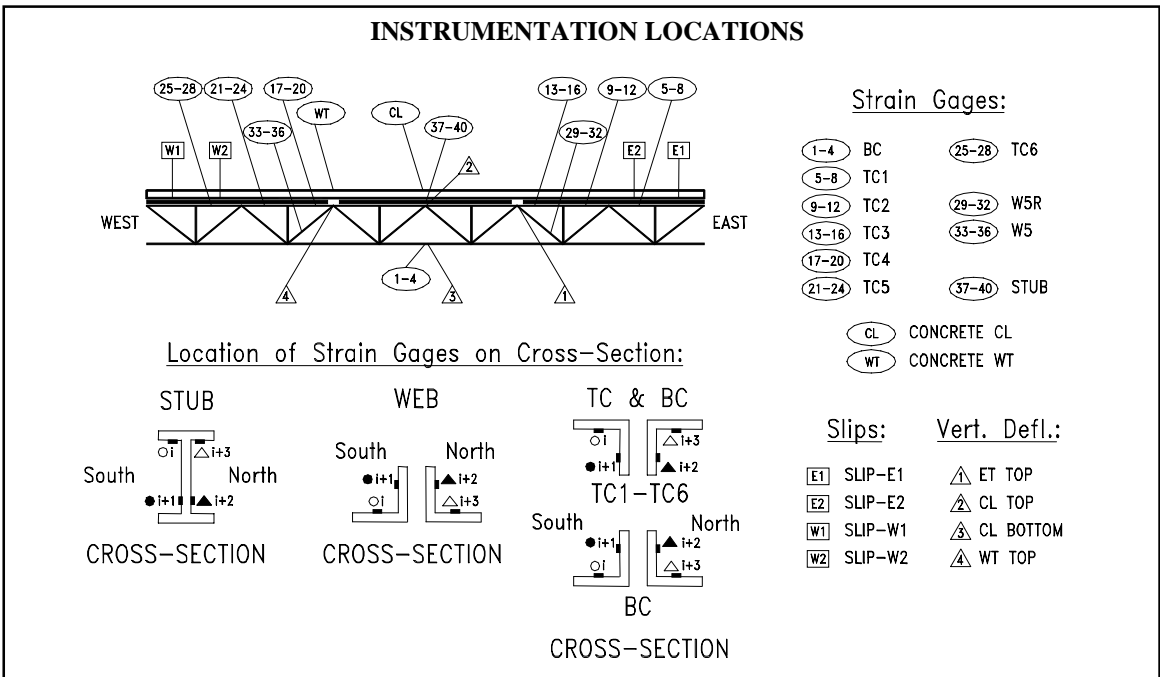
TEST DATES: 4-6 June 1996

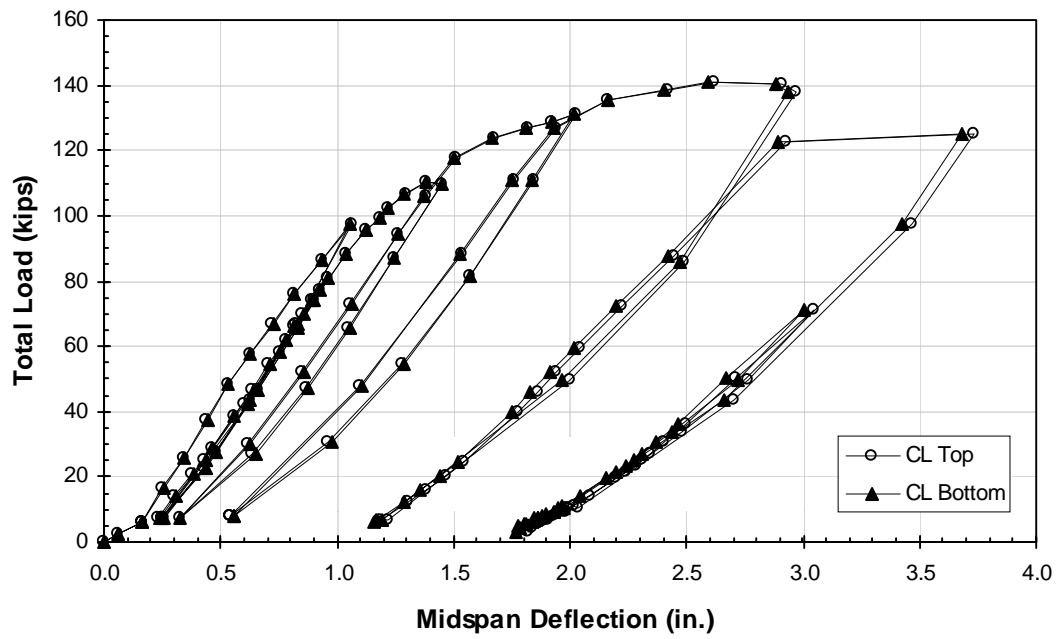
TEST DESCRIPTION				
<b>Joist-Girder:</b>	Span:	<u>30'-0"</u>	Weight:	<u>52.8 plf</u>
	Depth:	<u>25 in.</u>	Spacing:	<u>7 ft</u>
	Top Chord:	<u>2L-3.00x3.00x0.250</u>		
	Bottom Chord:	<u>2L-4.00x4.00x0.375</u>	Yield Stress:	<u>53.5 ksi</u>
	Stub:	<u>S5x10</u>		
<b>Deck:</b>	Type:	<u>2 VL</u>	Gage:	<u>18 ga</u>
<b>Slab:</b>	Total Depth:	<u>5 in.</u>	Compressive Strength:	<u>3000 psi</u>
<b>Shear Connector:</b>	Type:	<u>3/4 in. x 4 1/2 in. Welded Headed Shear Studs</u>		
	Quantity:	<u>14 per half-span, 28 total</u>		

THEORETICAL CALCULATIONS	
Theoretical Max. Total Load on Joist-Girder:	<u>166.4 kips</u>
Theoretical Moment of Inertia:	<u>3077 in.<sup>4</sup></u>

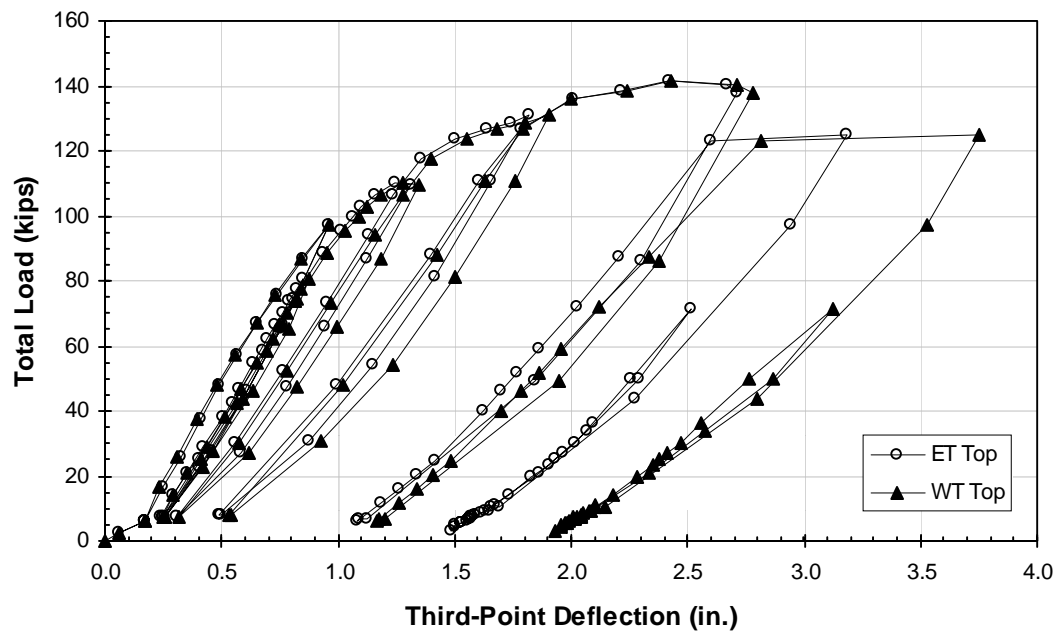
TEST RESULTS	
Total Load on Joist-Girder at Failure:	<u>141.3 kips</u>
Maximum Total Load on Joist-Girder:	<u>141.3 kips</u>
Midspan Deflection at Failure:	<u>2.62 in.</u>
Experimental Moment of Inertia:	<u>3137 in.<sup>4</sup></u>
Mode of Failure:	<u>Loss of shear connection along west third of span</u>

COMPARISON OF ACTUAL TO THEORETICAL	
Maximum Total Load on Joist-Girder	= 0.85
Theoretical Max. Total Load on Joist-Girder	

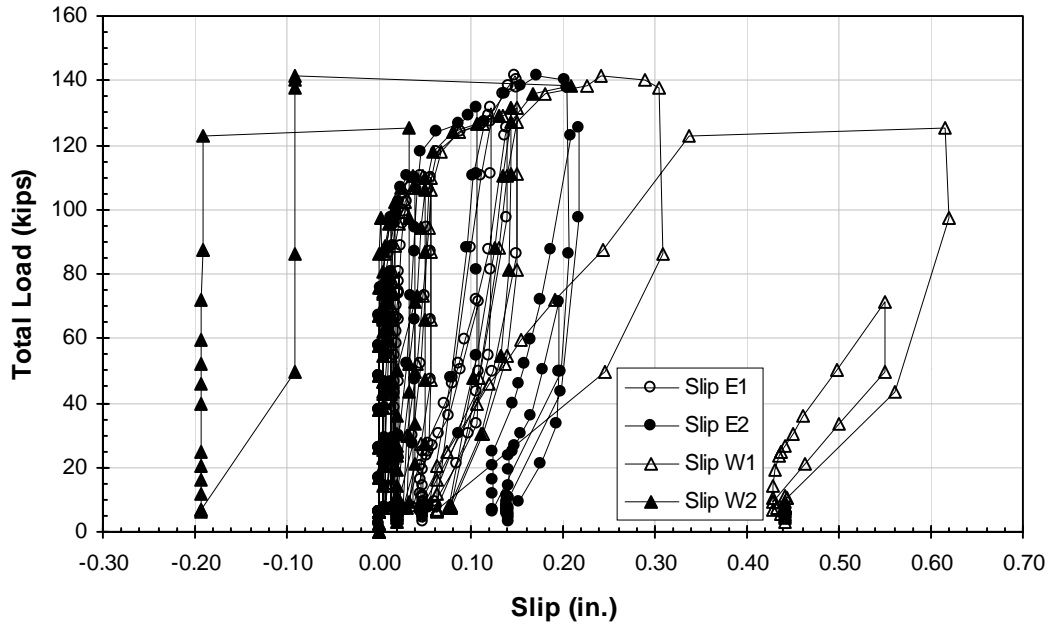




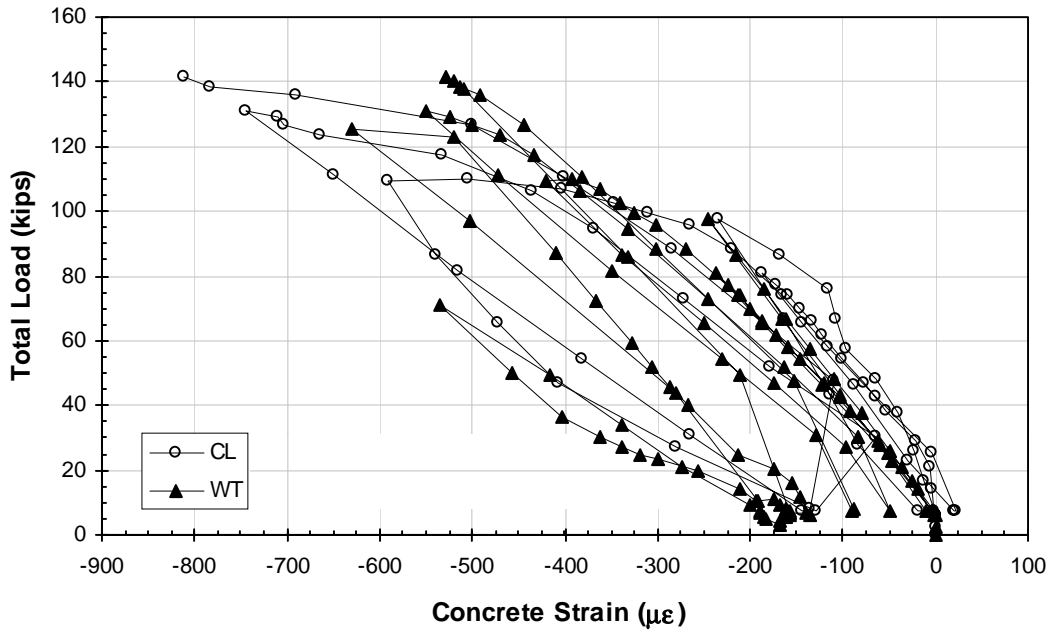
**Figure B.6.1 Total Load vs. Midspan Deflections of EGR**



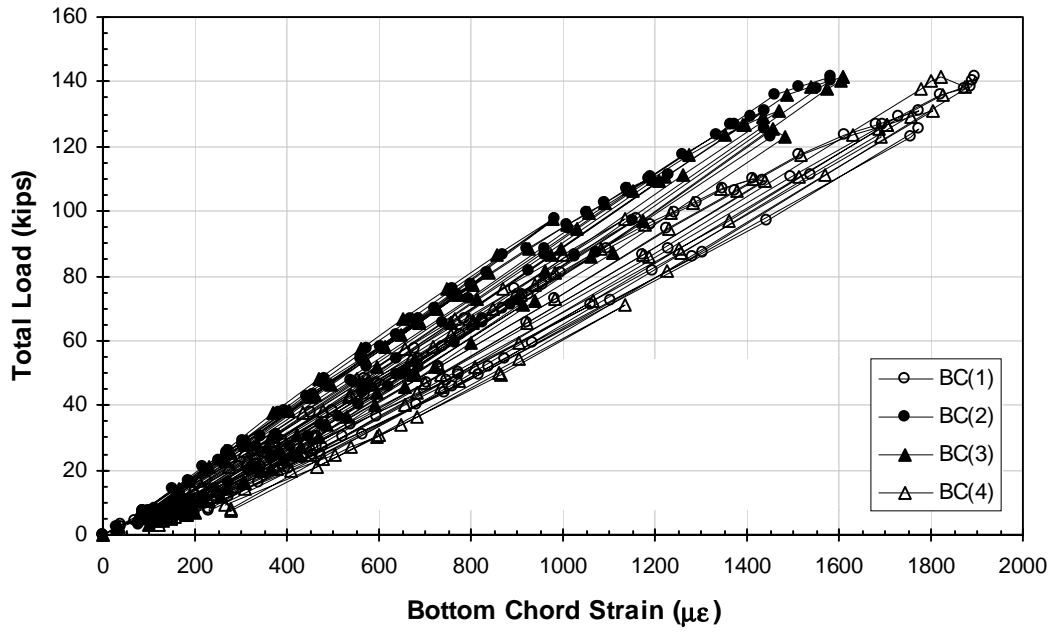
**Figure B.6.2 Total Load vs. Third-Point Deflections of EGR**



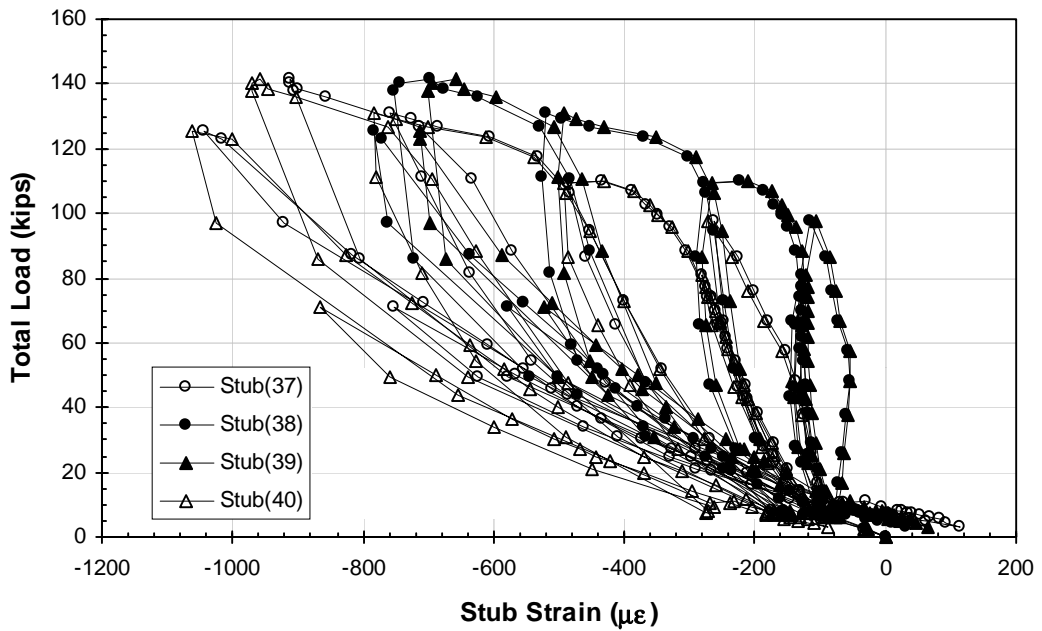
**Figure B.6.3 Total Load vs. Slip of EGR**



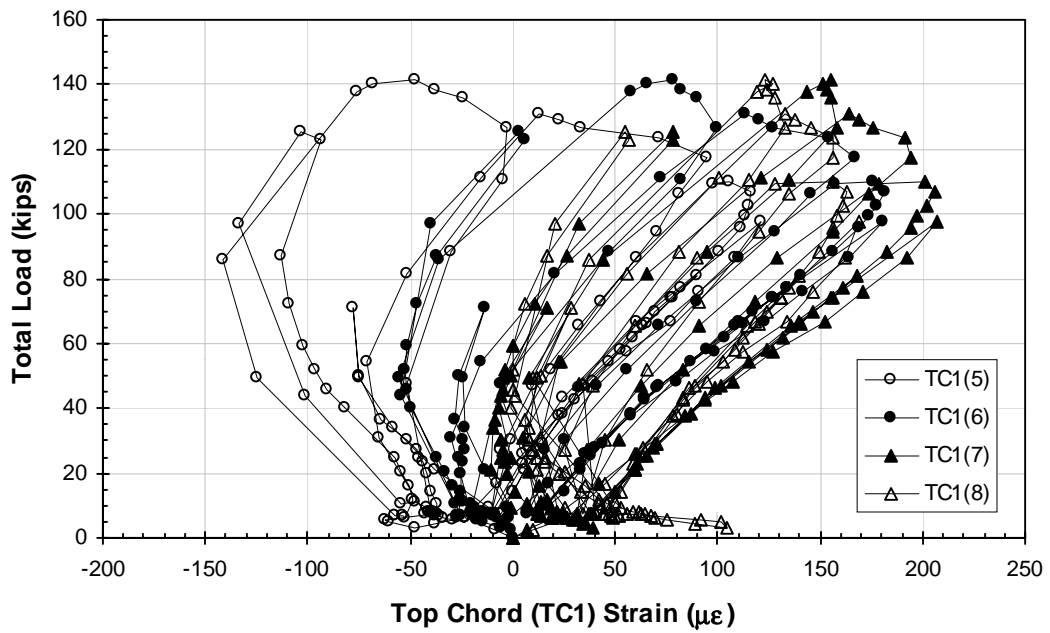
**Figure B.6.4 Total Load vs. Concrete Strain of EGR**



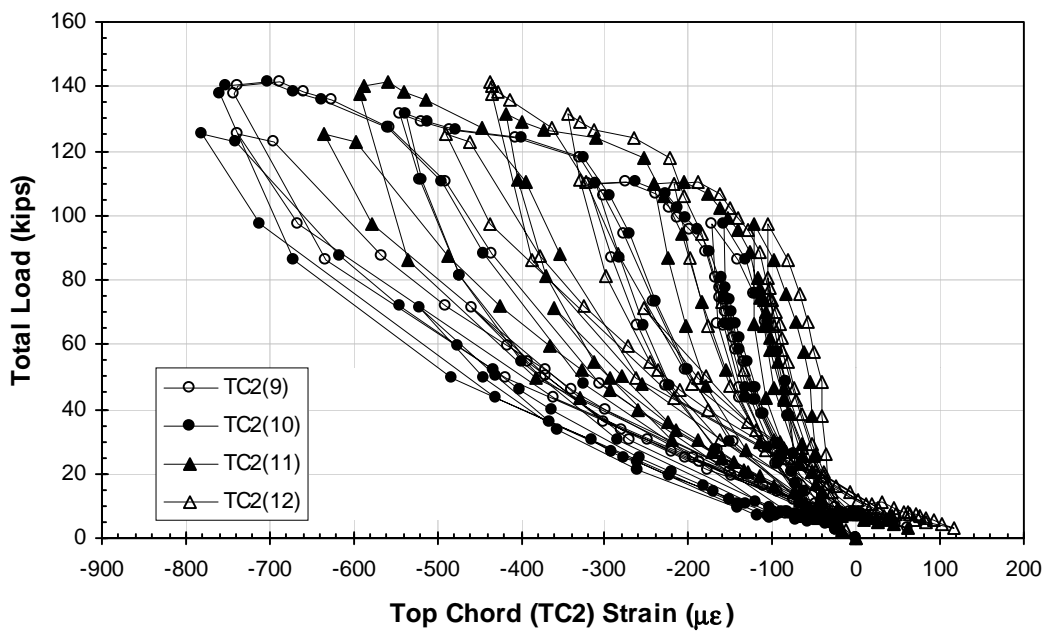
**Figure B.6.5 Total Load vs. Bottom Chord Strain of EGR**



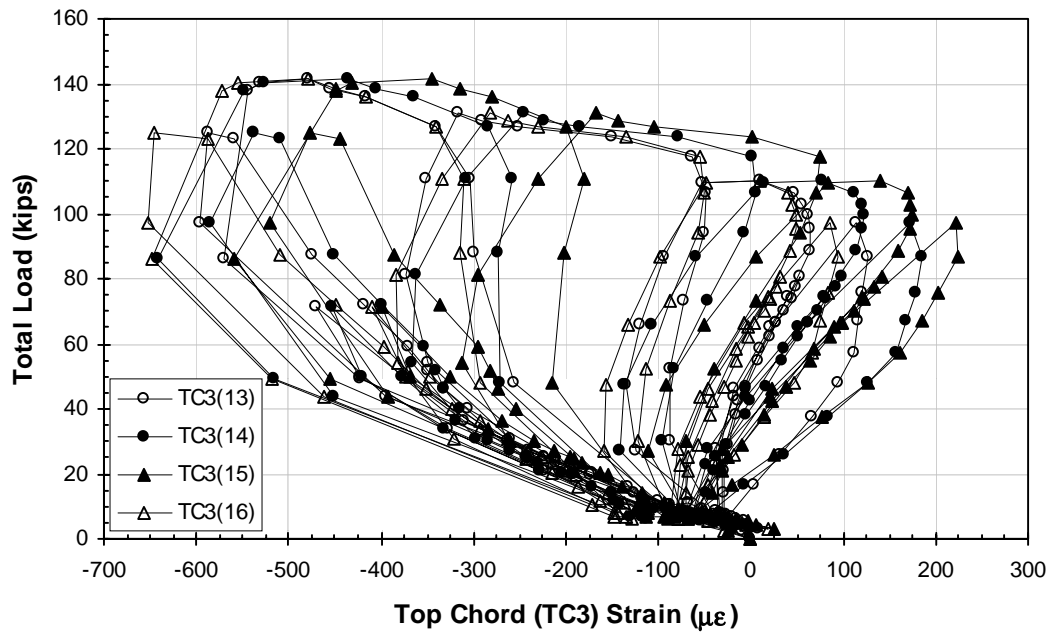
**Figure B.6.6 Total Load vs. Stub Strain of EGR**



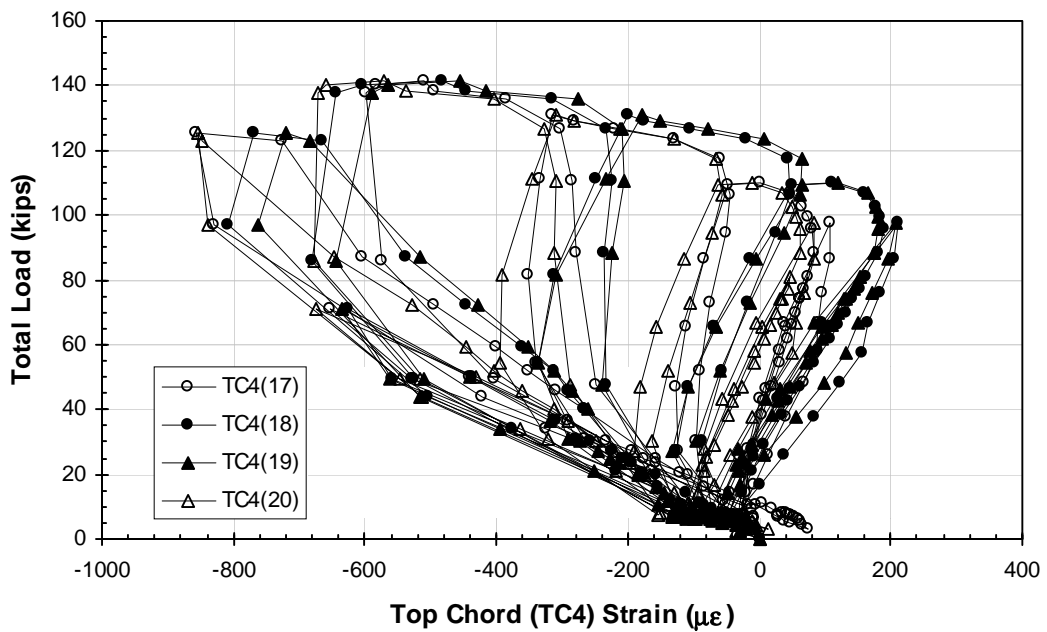
**Figure B.6.7 Total Load vs. Top Chord (TC1) Strain of EGR**



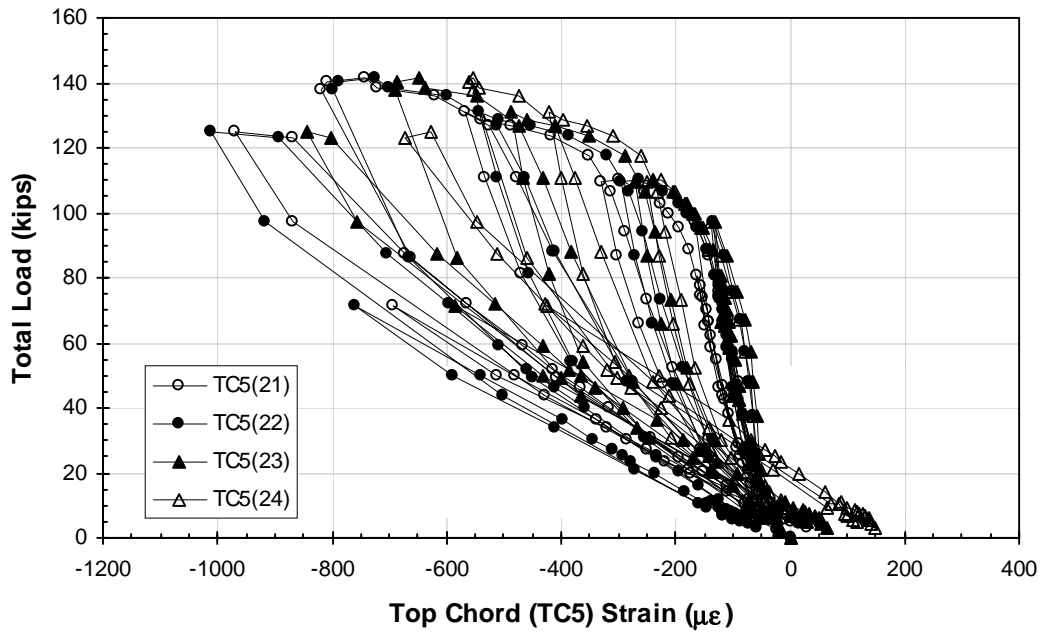
**Figure B.6.8 Total Load vs. Top Chord (TC2) Strain of EGR**



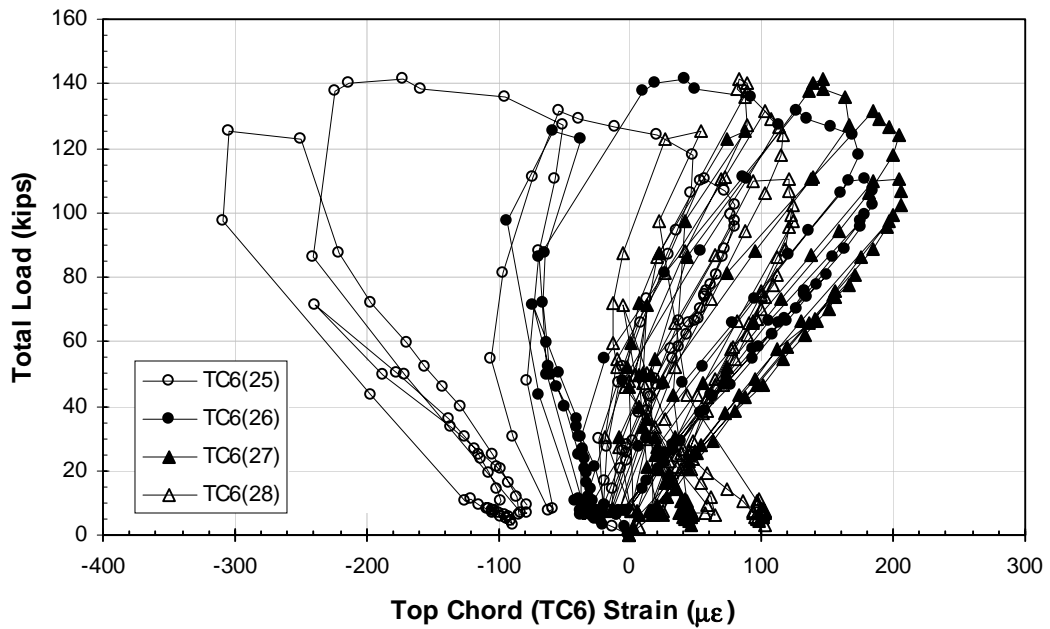
**Figure B.6.9 Total Load vs. Top Chord (TC3) Strain of EGR**



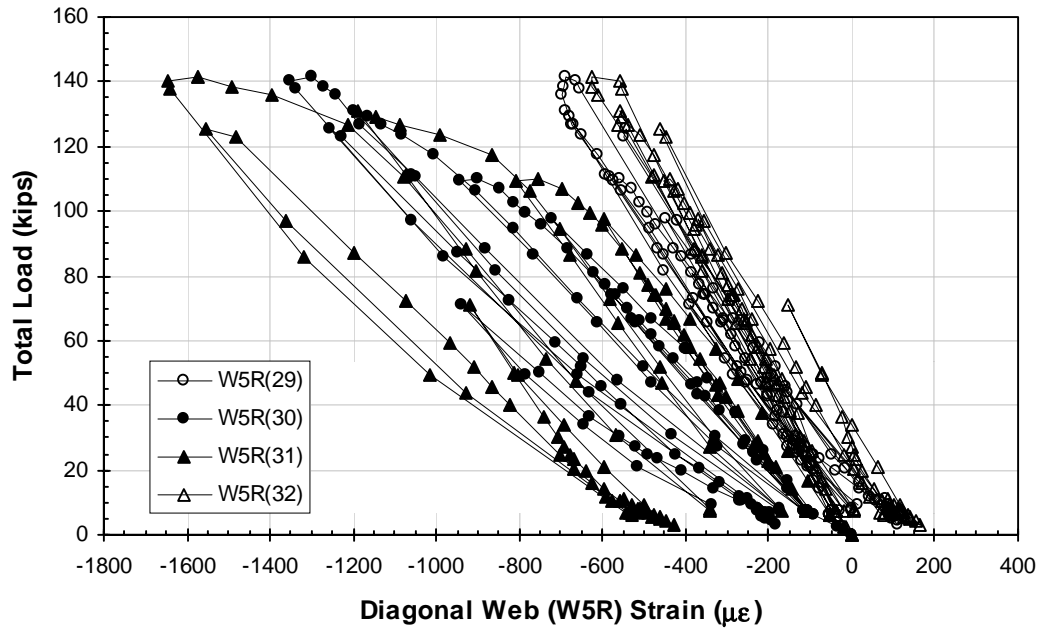
**Figure B.6.10 Total Load vs. Top Chord (TC4) Strain of EGR**



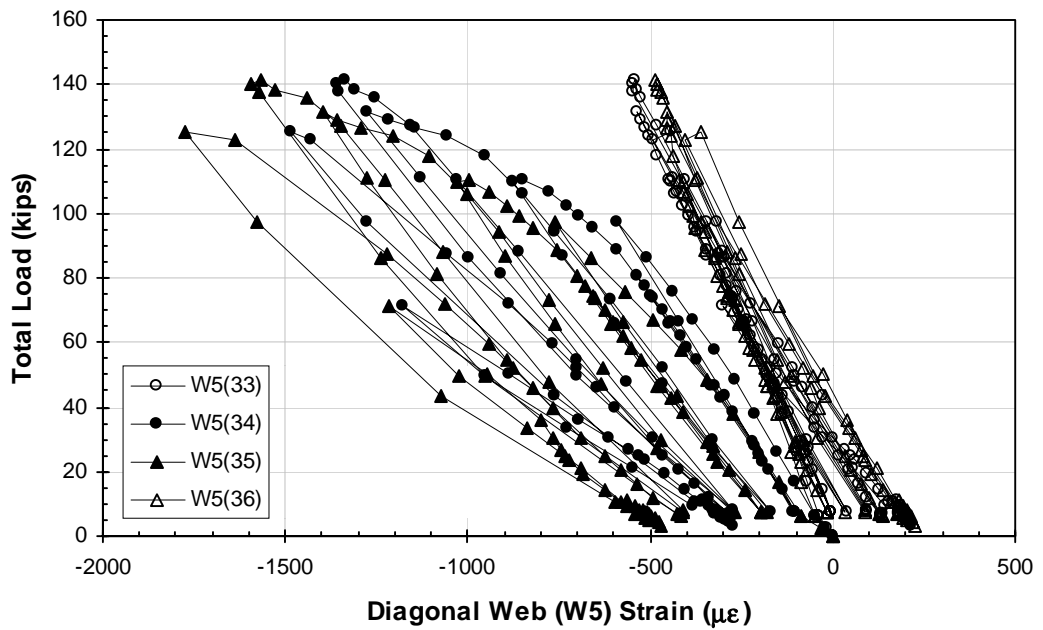
**Figure B.6.11 Total Load vs. Top Chord (TC5) Strain of EGR**



**Figure B.6.12 Total Load vs. Top Chord (TC6) Strain of EGR**



**Figure B.6.13 Total Load vs. Diagonal Web (W5R) Strain of EGR**



**Figure B.6.14 Total Load vs. Diagonal Web (W5) Strain of EGR**

## COMPOSITE HAUNCHED JOIST-GIRDER TEST SUMMARY SHEET

GIRDER DESIGNATION: EGL

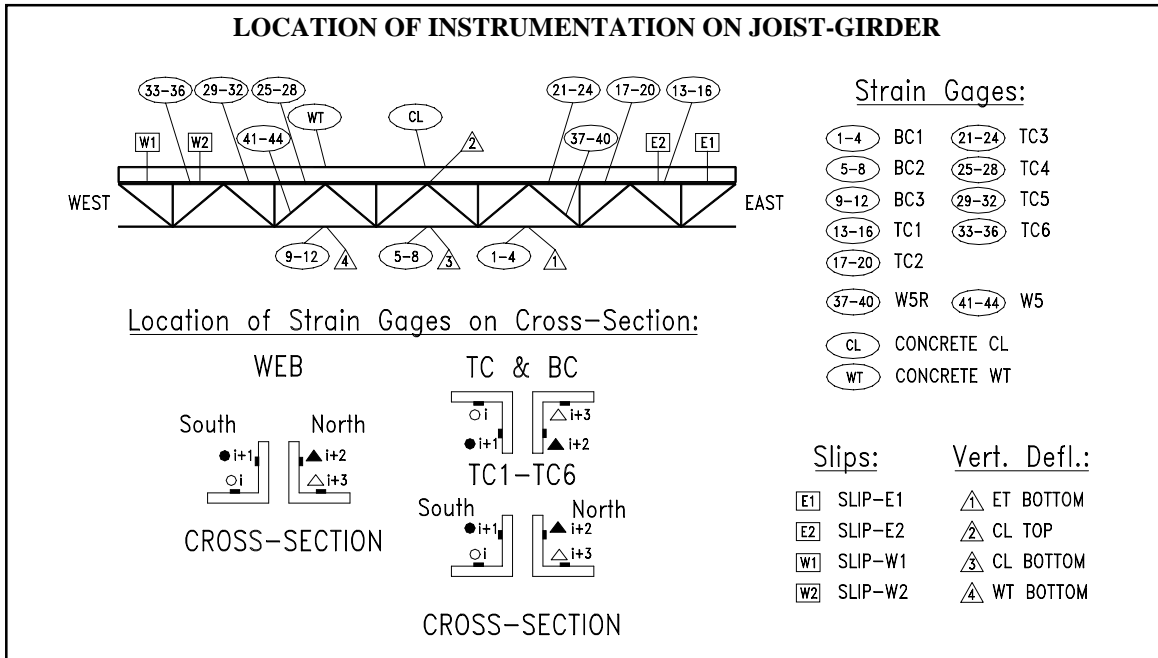
TEST DATES: 17-19 December 1996

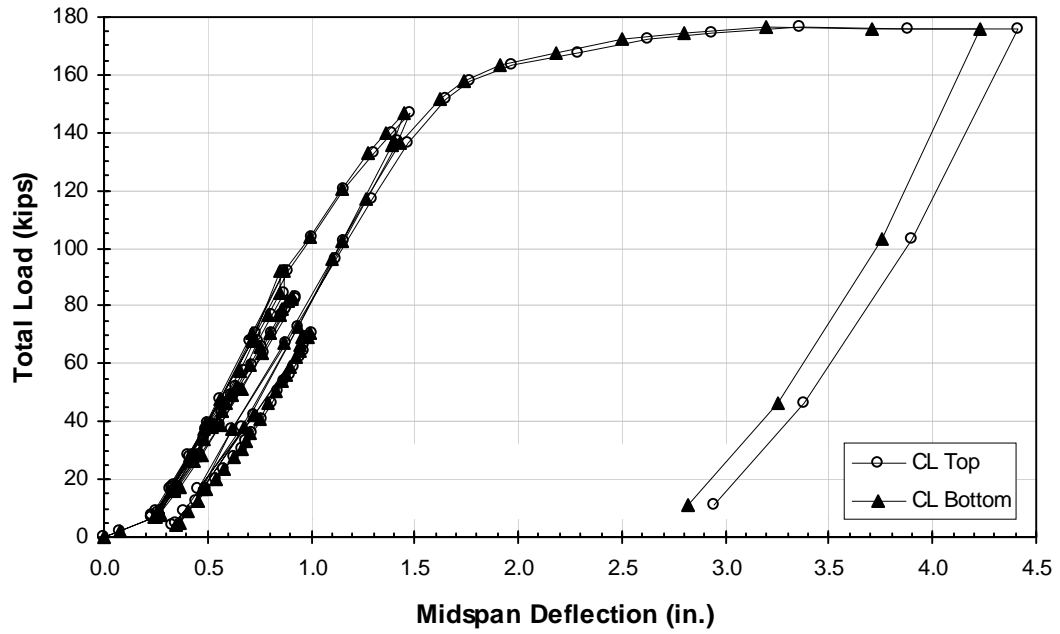
TEST DESCRIPTION				
<b>Joist-Girder:</b>	Span:	<u>30'-0"</u>	Weight:	<u>46.1 plf</u>
	Depth:	<u>25 in.</u>	Spacing:	<u>6 ft - 9 in.</u>
	Top Chord:	<u>2L-3.00x3.00x0.250</u>	Yield Stress:	<u>58.0 ksi</u>
	Bottom Chord:	<u>2L-4.00x4.00x0.375</u>	Yield Stress:	<u>55.3 ksi</u>
	<b>Deck:</b>	Type:	<u>2 VL</u>	Gage:
<b>Slab:</b>	Total Depth:	<u>5 in.</u>	Compressive Strength:	<u>4500 psi</u>
	Haunch:	<u>5 in.</u>		
<b>Shear Connector:</b>	Type:	<u>3/4 in. x 8.0 in. Welded Headed Shear Studs</u>		
	Quantity:	<u>27 per half-span, one at midspan, 55 total</u>		

THEORETICAL CALCULATIONS	
Theoretical Max. Total Load on Joist-Girder:	<u>181.7 kips</u>
Theoretical Moment of Inertia:	<u>3323 in.<sup>4</sup></u>

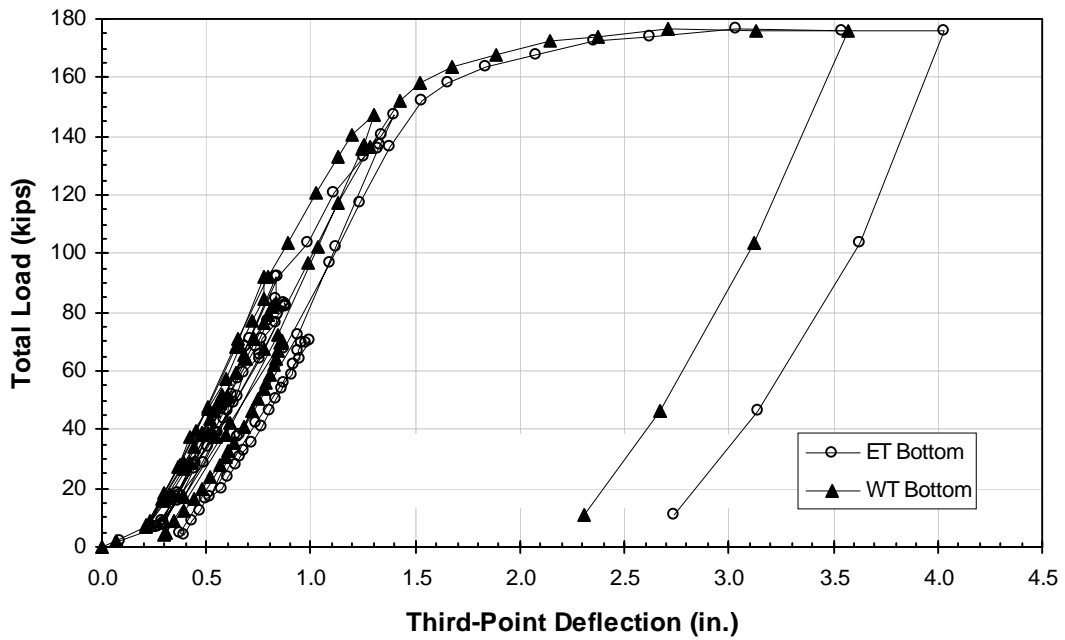
TEST RESULTS	
Total Load on Joist-Girder at Failure:	<u>176.6 kips</u>
Maximum Total Load on Joist-Girder:	<u>176.6 kips</u>
Midspan Deflection at Failure:	<u>3.36 in.</u>
Experimental Moment of Inertia:	<u>3694 in.<sup>4</sup></u>
Mode of Failure:	<u>Yielding of bottom chord</u>

COMPARISON OF ACTUAL TO THEORETICAL	
<u>Maximum Total Load on Joist-Girder</u>	= 0.97
Theoretical Max. Total Load on Joist-Girder	

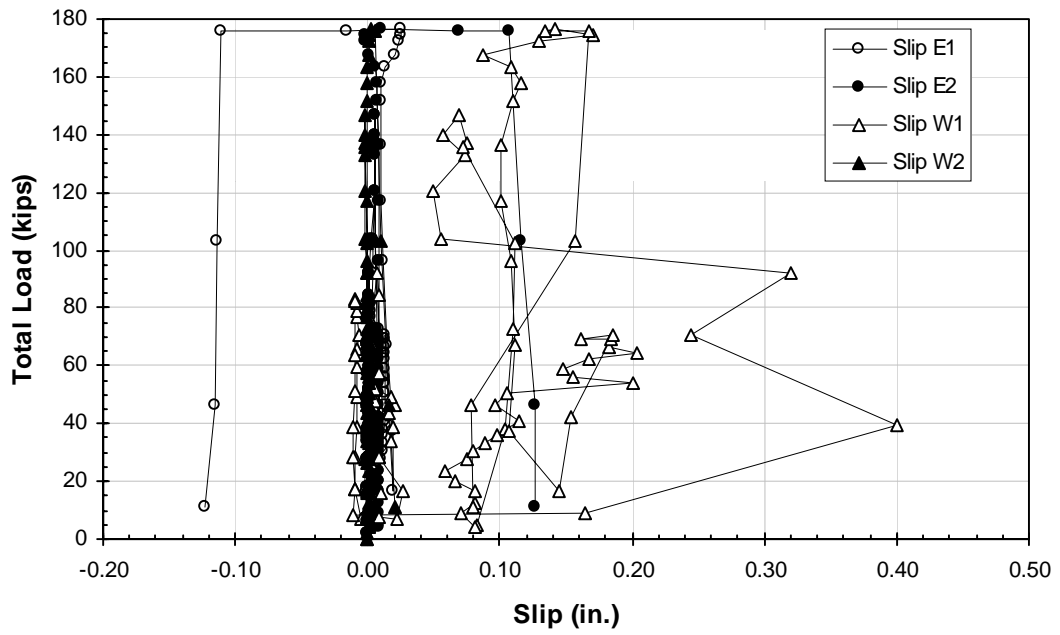




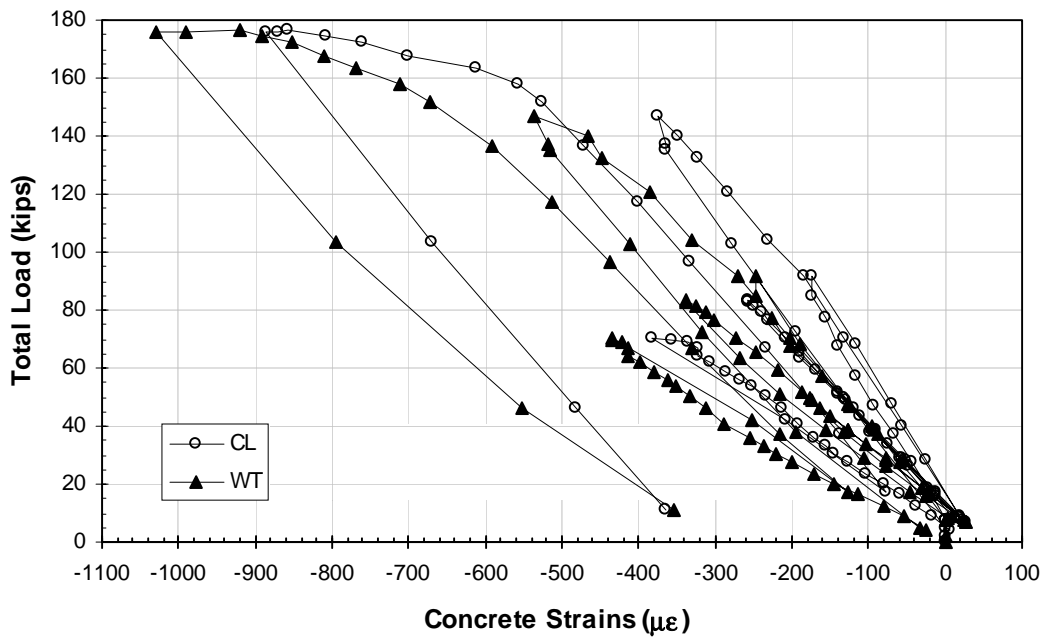
**Figure B.7.1 Total Load vs. Midspan Deflections of EGL**



**Figure B.7.2 Total Load vs. Third-Point Deflections of EGL**



**Figure B.7.3 Total Load vs. Slip of EGL**



**Figure B.7.4 Total Load vs. Concrete Strain of EGL**

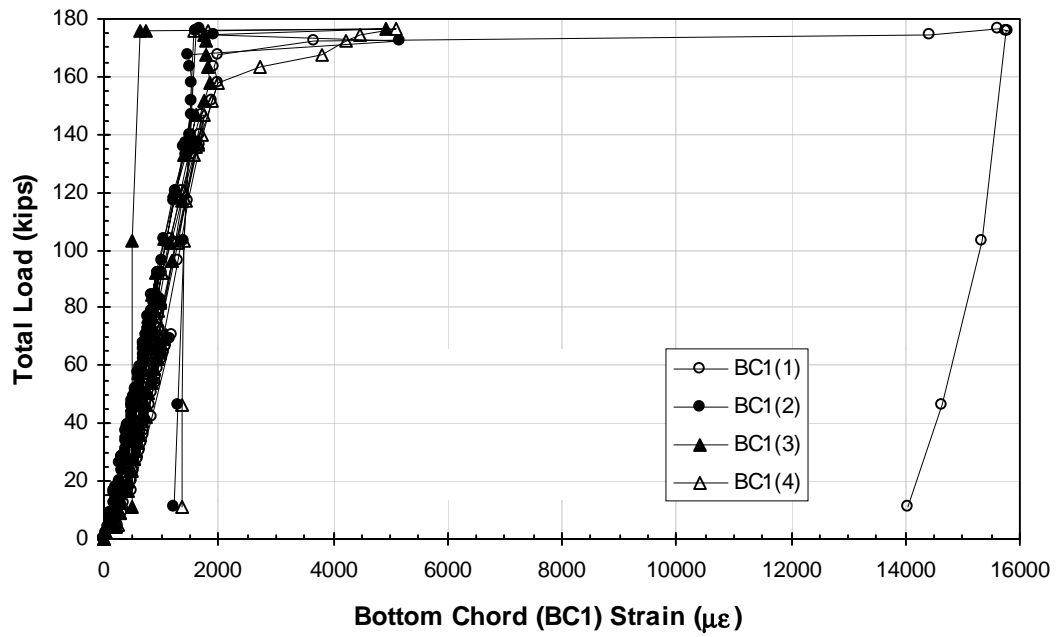


Figure B.7.5 Total Load vs. Bottom Chord (BC1) Strain of EGL

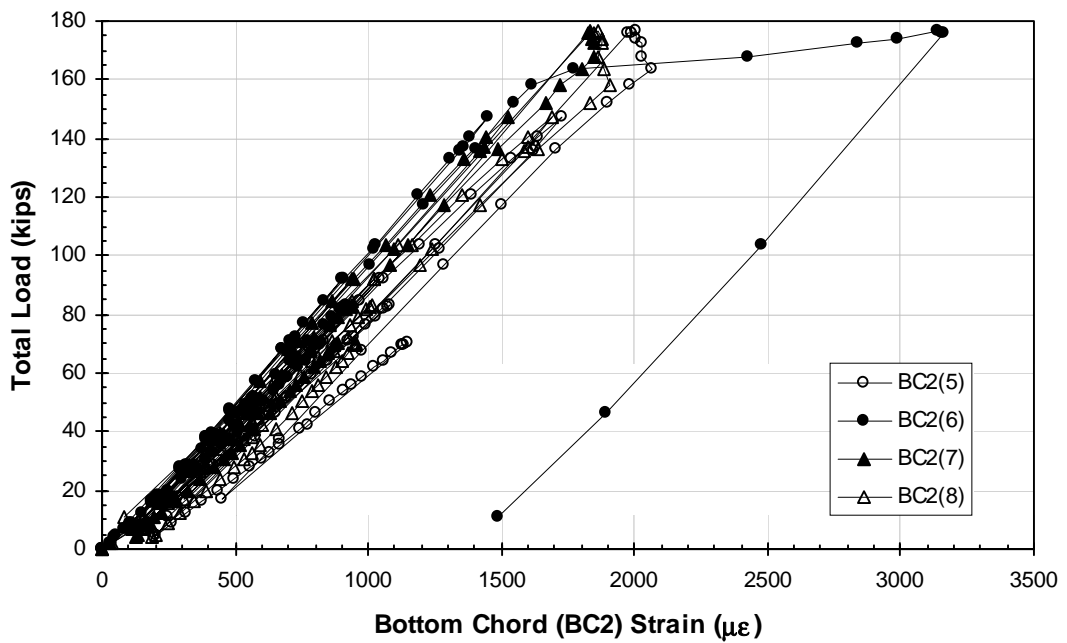
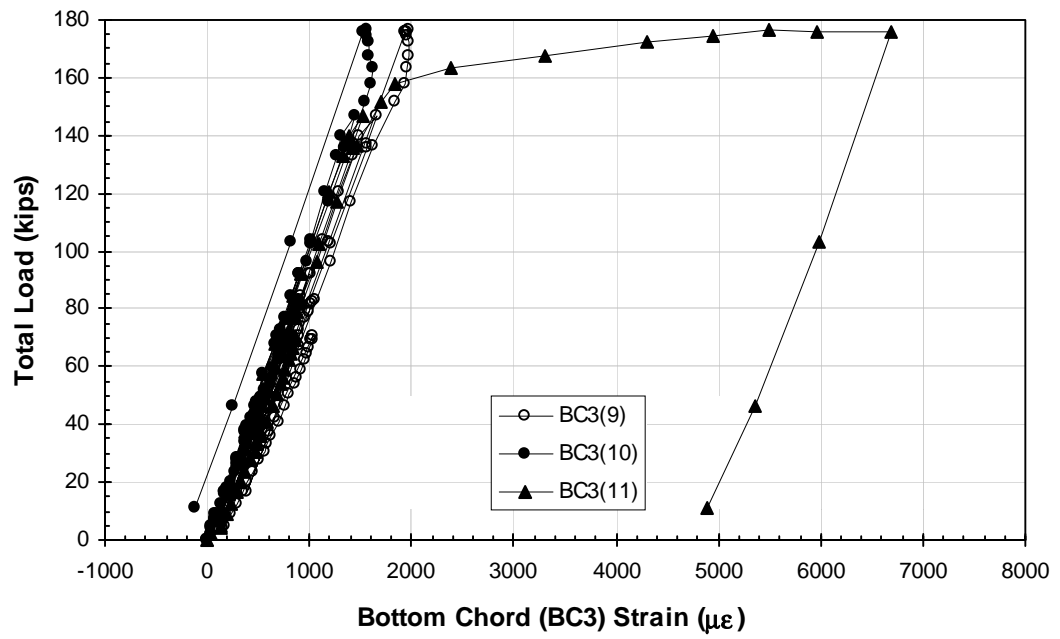
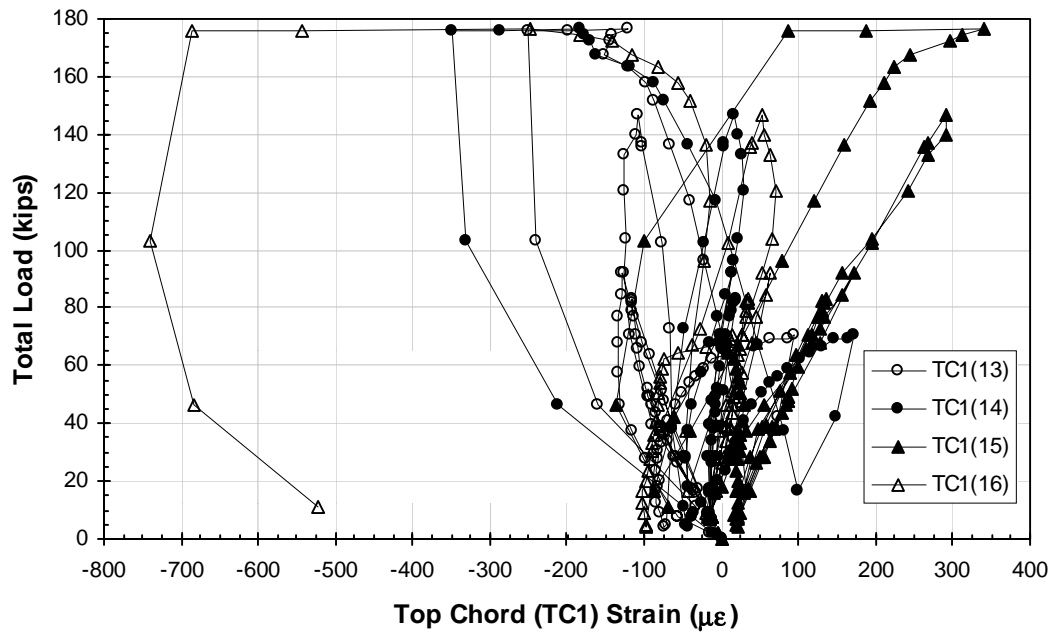


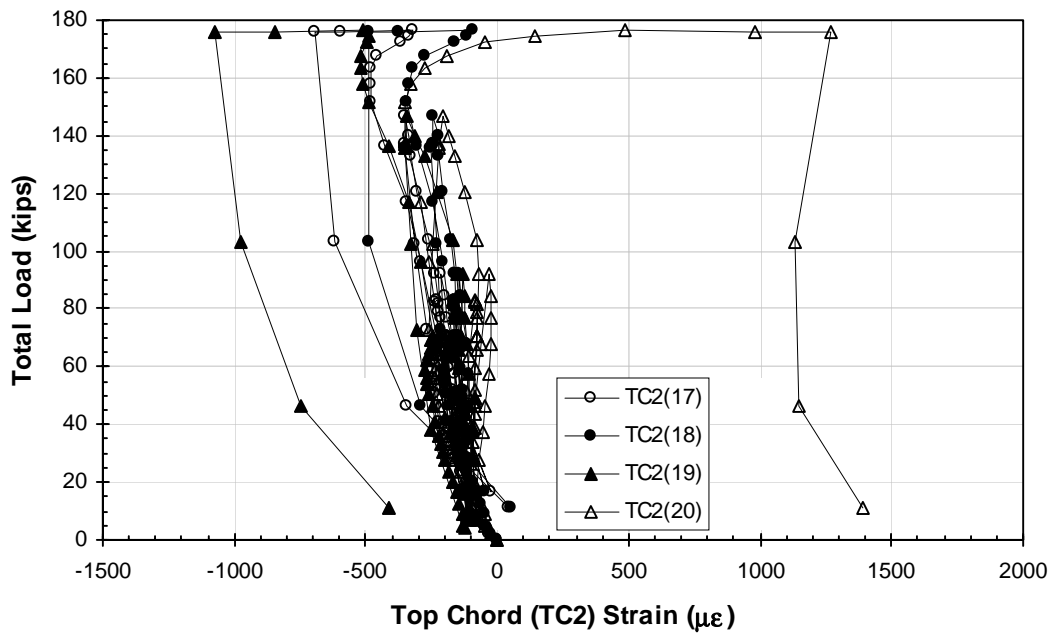
Figure B.4.6 Total Load vs. Bottom Chord (BC2) Strain of EGL



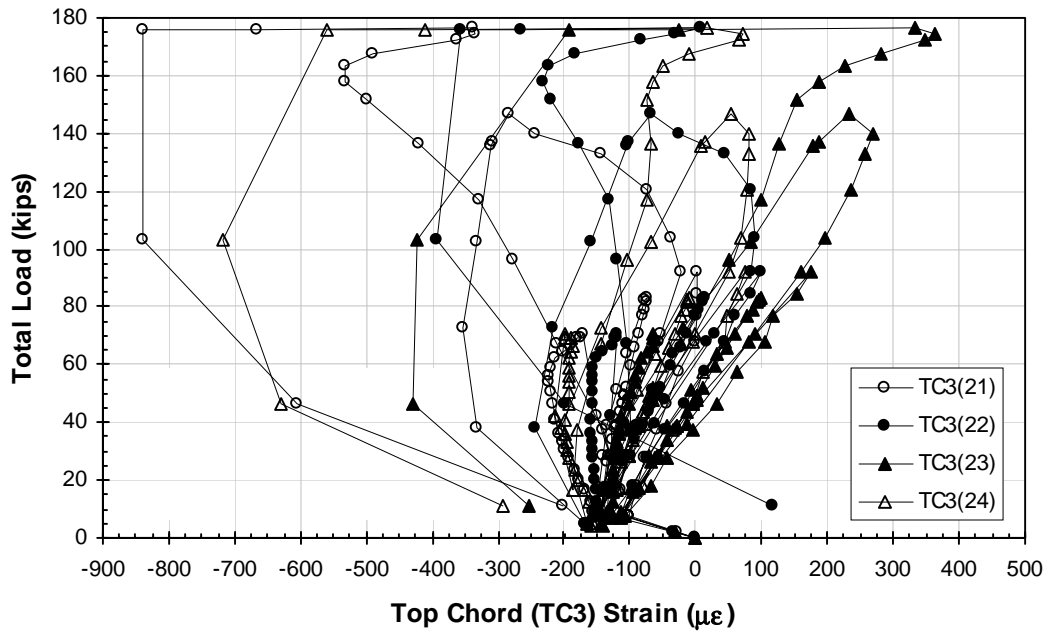
**Figure B.7.7 Total Load vs. Bottom Chord (BC3) Strain of EGL**



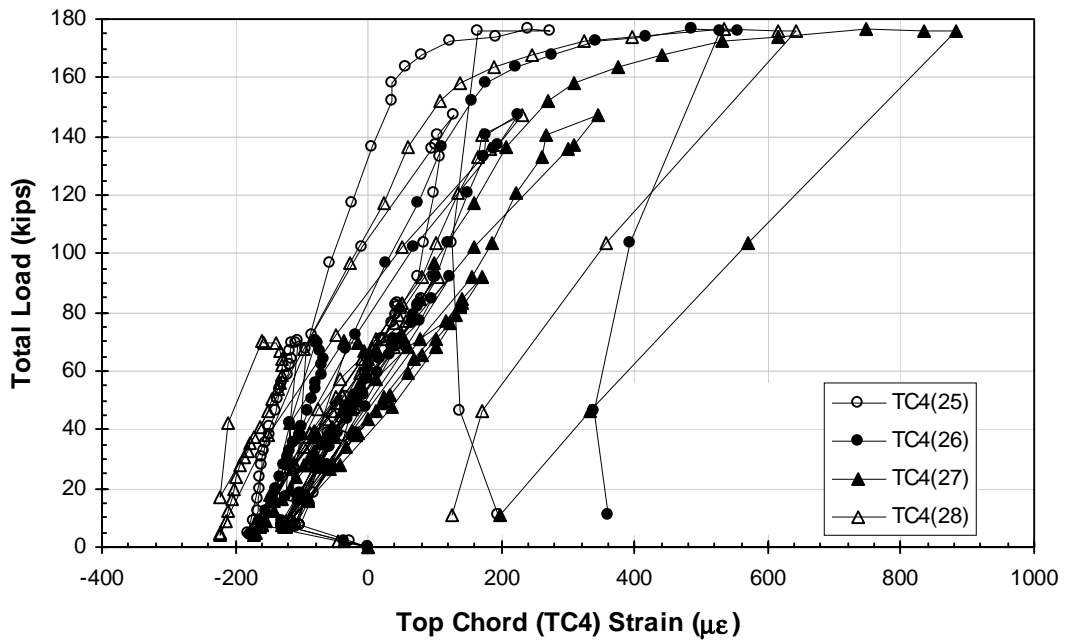
**Figure B.7.8 Total Load vs. Top Chord (TC1) Strain of EGL**



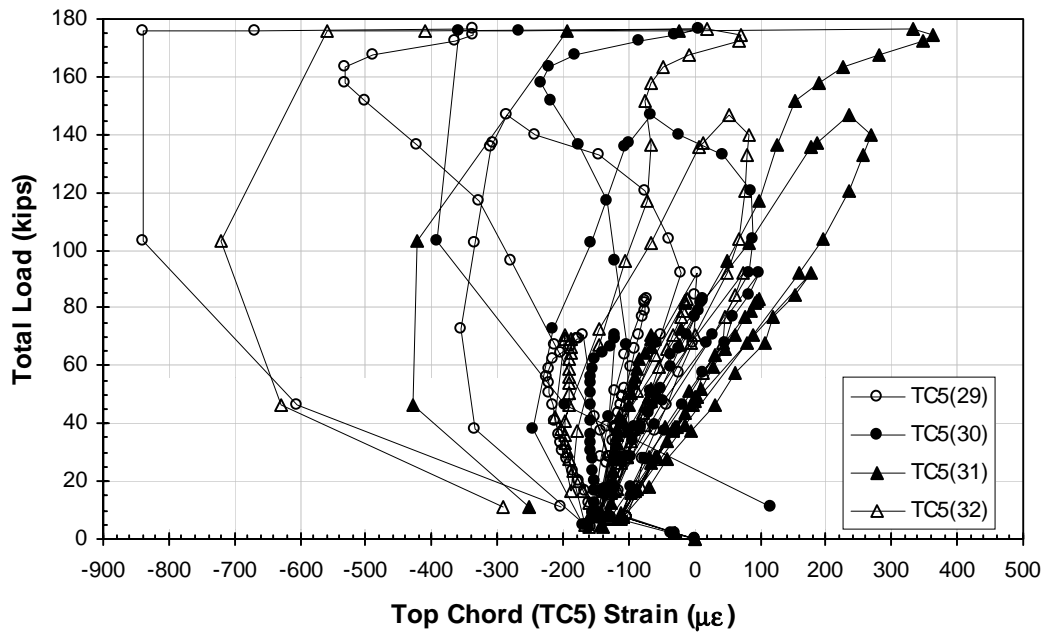
**Figure B.7.9 Total Load vs. Top Chord (TC2) Strain of EGL**



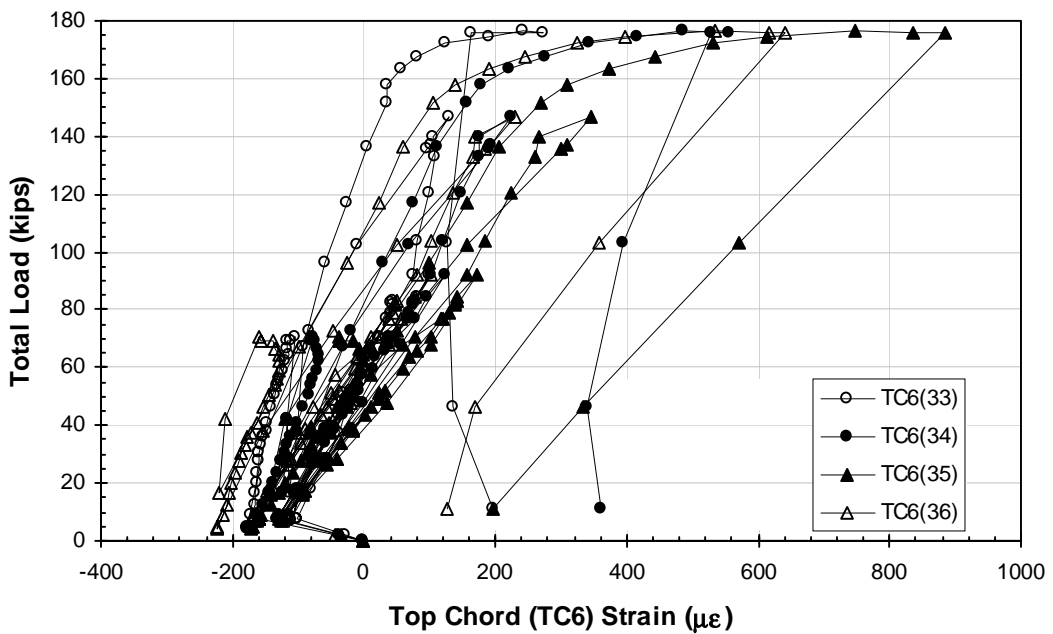
**Figure B.7.10 Total Load vs. Top Chord (TC3) Strain of EGL**



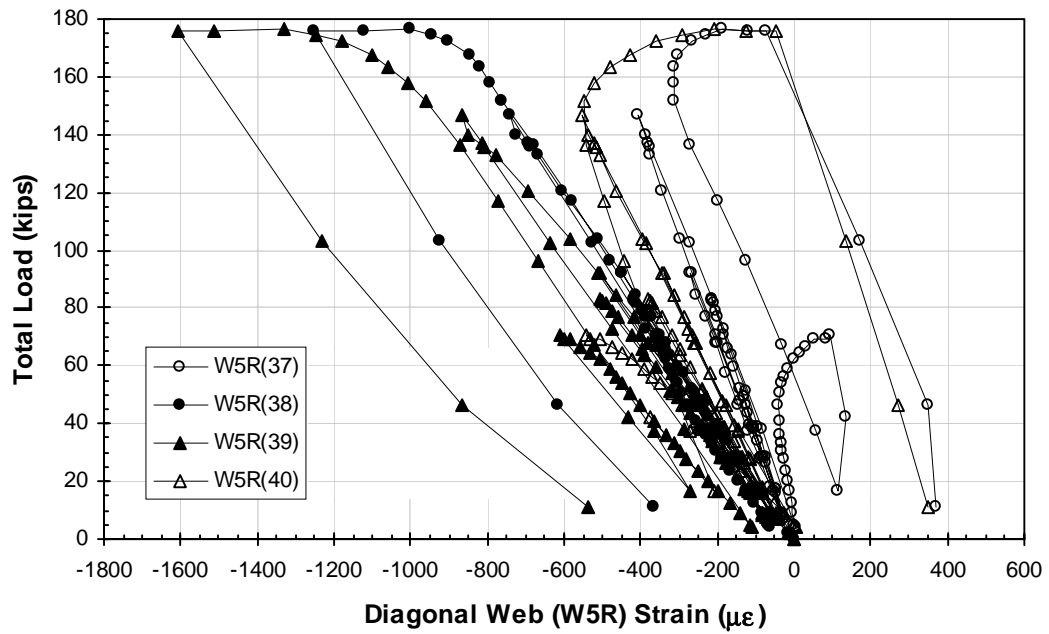
**Figure B.7.11 Total Load vs. Top Chord (TC4) Strain of EGL**



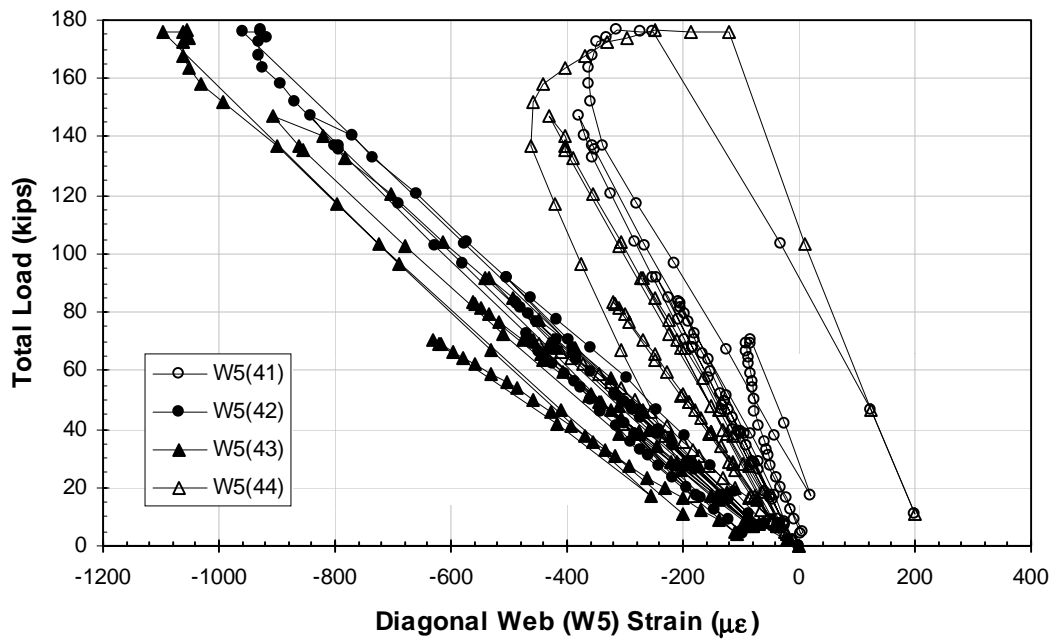
**Figure B.7.12 Total Load vs. Top Chord (TC5) Strain of EGL**



**Figure B.7.13 Total Load vs. Top Chord (TC6) Strain of EGL**



**Figure B.7.14 Total Load vs. Diagonal Web (W5R) Strain of EGL**



**Figure B.7.15 Total Load vs. Diagonal Web (W5) Strain of EGL**

## COMPOSITE HAUNCHED JOIST-GIRDER TEST SUMMARY SHEET

GIRDER DESIGNATION: IG

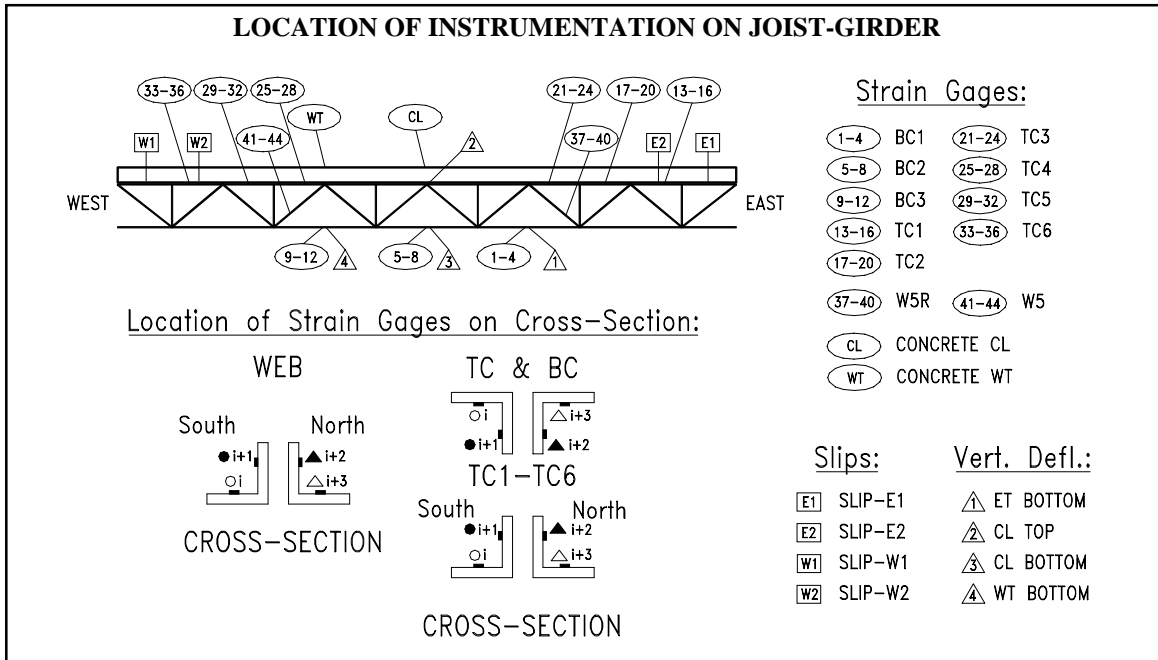
TEST DATES: 17-19 December 1996

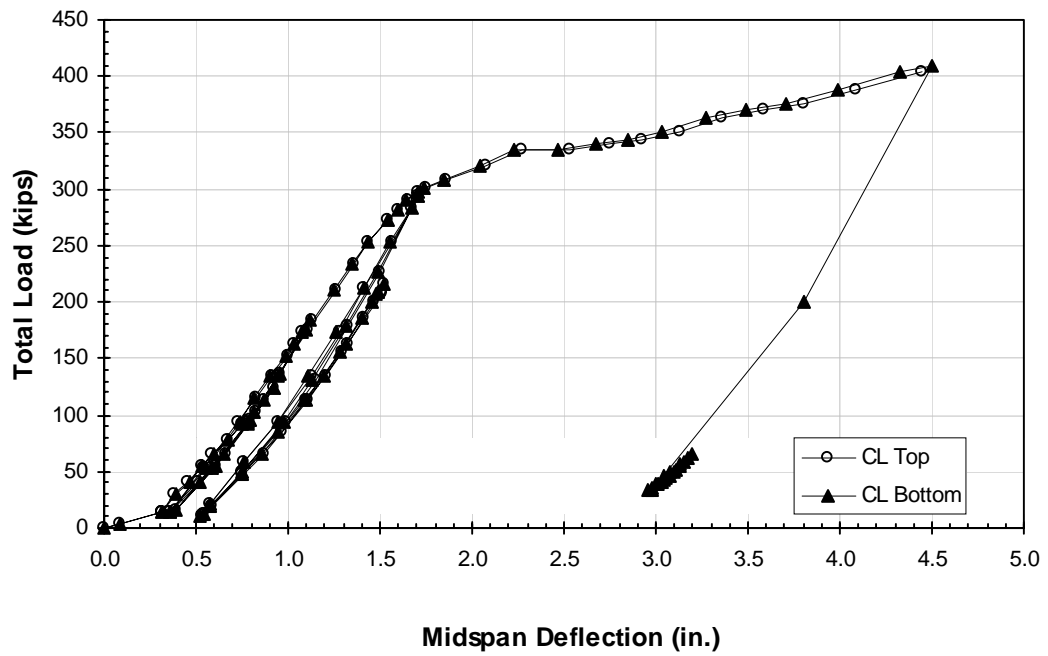
TEST DESCRIPTION				
<b>Joist-Girder:</b>	Span:	<u>30'-0"</u>	Weight:	<u>89.2 plf</u>
	Depth:	<u>25 in.</u>	Spacing:	<u>6 ft - 9 in.</u>
	Top Chord:	<u>2L-4.00x4.00x0.375</u>	Yield Stress:	<u>55.7 ksi</u>
	Bottom Chord:	<u>2L-5.00x5.00x0.625</u>	Yield Stress:	<u>53.4 ksi</u>
	<b>Deck:</b>	Type:	<u>2 VL</u>	Gage:
<b>Slab:</b>	Total Depth:	<u>5 in.</u>	Compressive Strength:	<u>4500 psi</u>
	Haunch:	<u>5 in.</u>		
<b>Shear Connector:</b>	Type:	<u>3/4 in. x 8.0 in. Welded Headed Shear Studs</u>		
	Quantity:	<u>53 per half-span, one at midspan, 107 total</u>		

THEORETICAL CALCULATIONS	
Theoretical Max. Total Load on Joist-Girder:	<u>353.2 kips</u>
Theoretical Moment of Inertia:	<u>6400 in.<sup>4</sup></u>

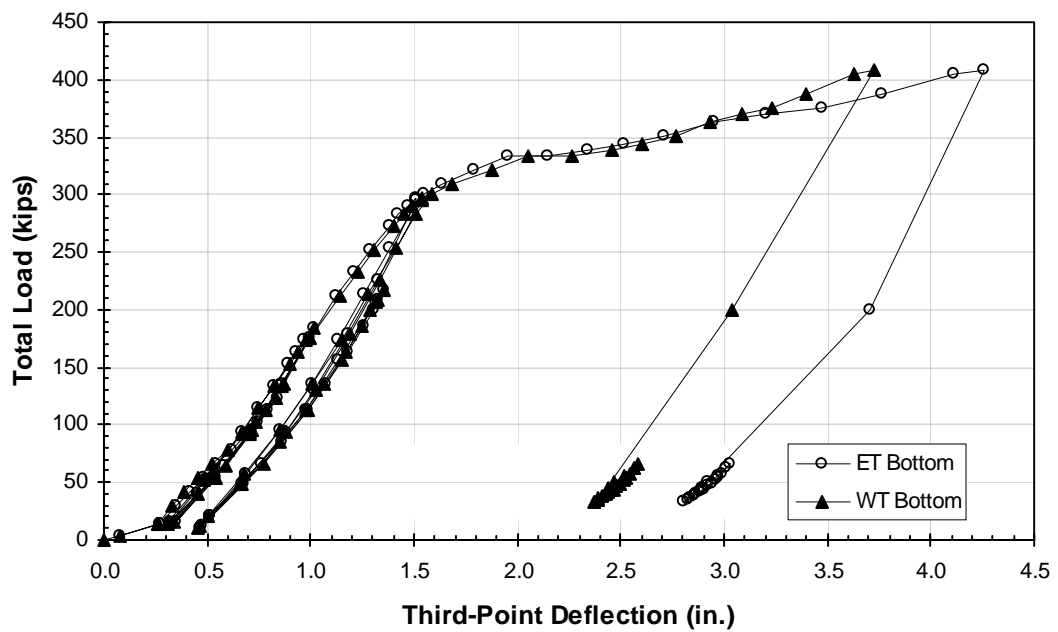
TEST RESULTS	
Total Load on Joist-Girder at Failure:	<u>334.0 kips</u>
Maximum Total Load on Joist-Girder:	<u>409.1 kips</u>
Midspan Deflection at Failure:	<u>2.28 in.</u>
Experimental Moment of Inertia:	<u>6152 in.<sup>4</sup></u>
Mode of Failure:	<u>Yielding of bottom chord at the east third point</u>

COMPARISON OF ACTUAL TO THEORETICAL	
<u>Maximum Total Load on Joist-Girder</u>	= 1.16
Theoretical Max. Total Load on Joist-Girder	





**Figure B.8.1 Total Load vs. Midspan Deflections of IG**



**Figure B.8.2 Total Load vs. Third-Point Deflections of IG**

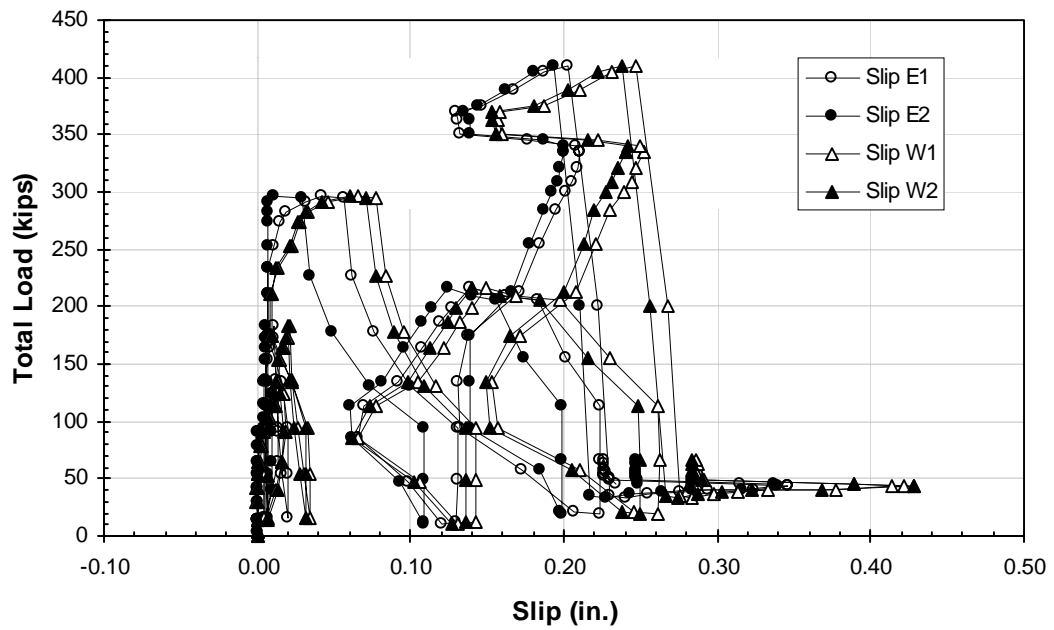


Figure B.8.3 Total Load vs. Slip of IG

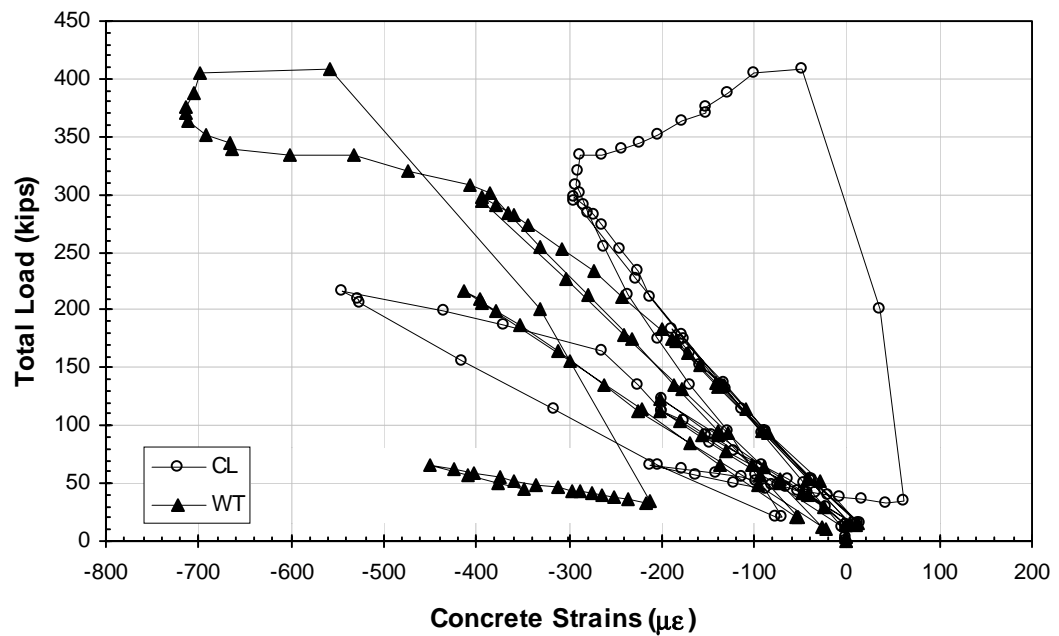


Figure B.8.4 Total Load vs. Concrete Strain of IG

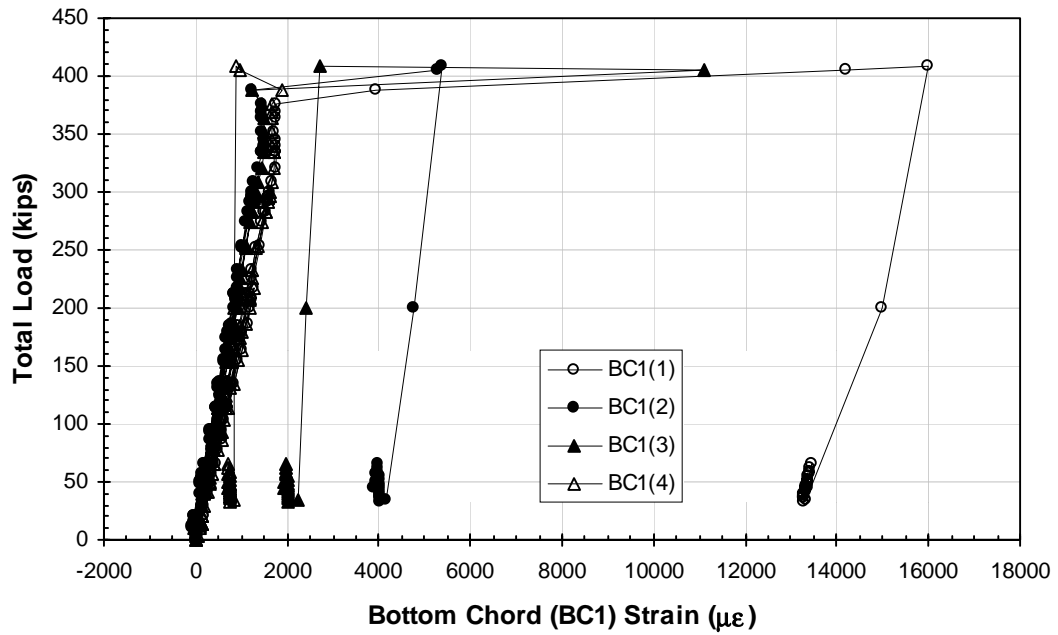


Figure B.8.5 Total Load vs. Bottom Chord (BC1) Strain of IG

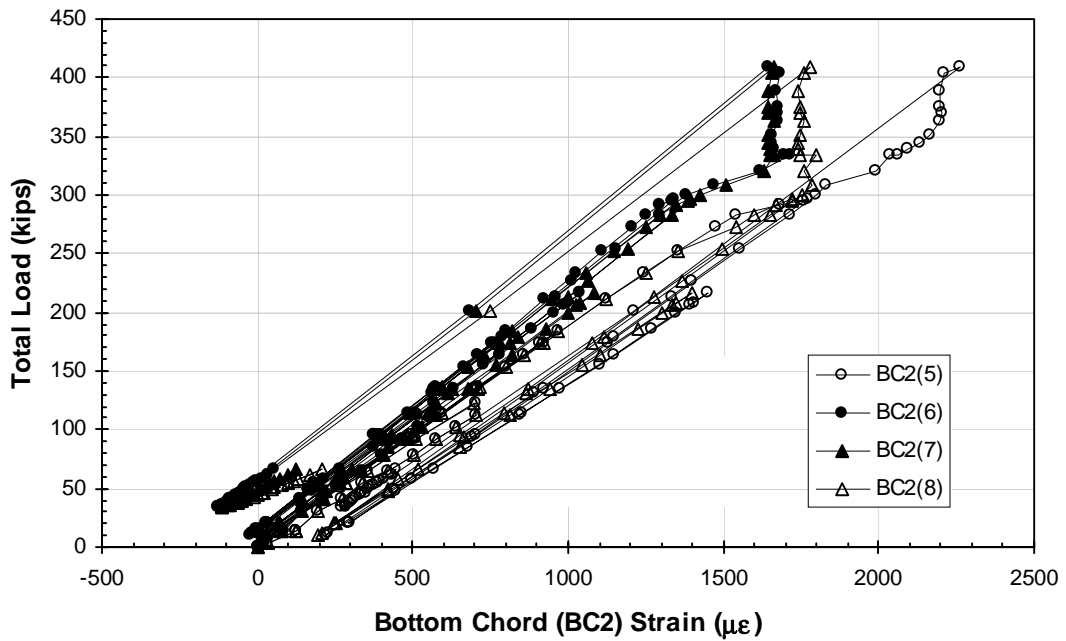
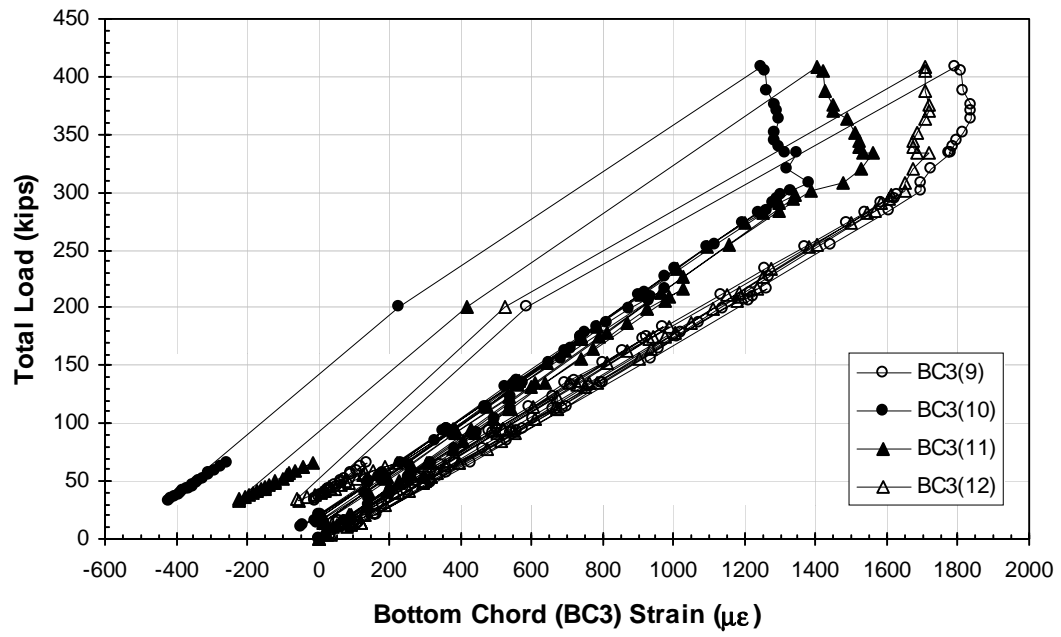
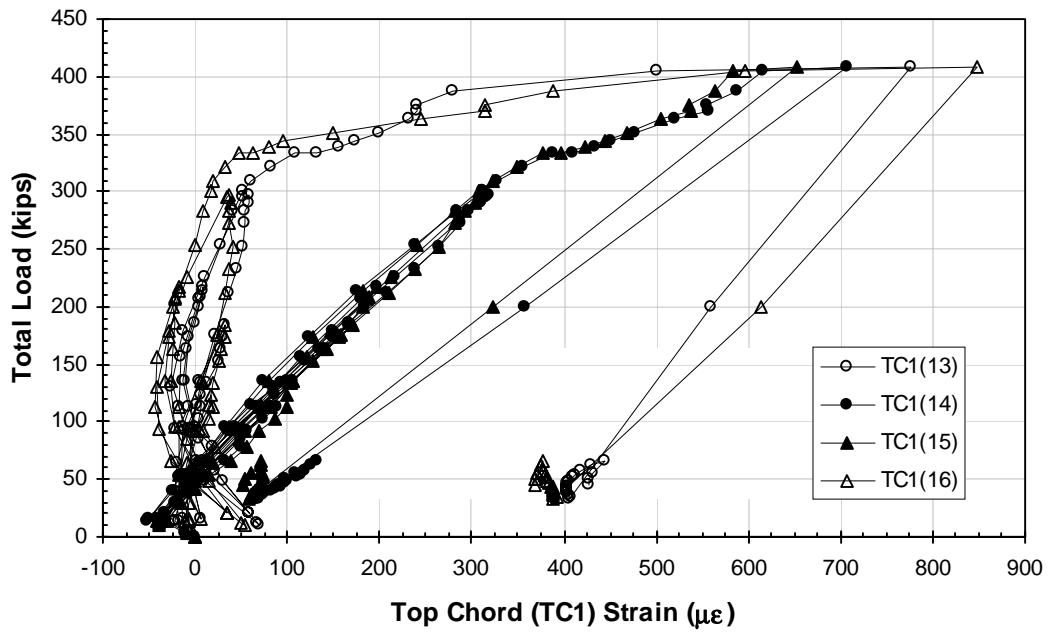


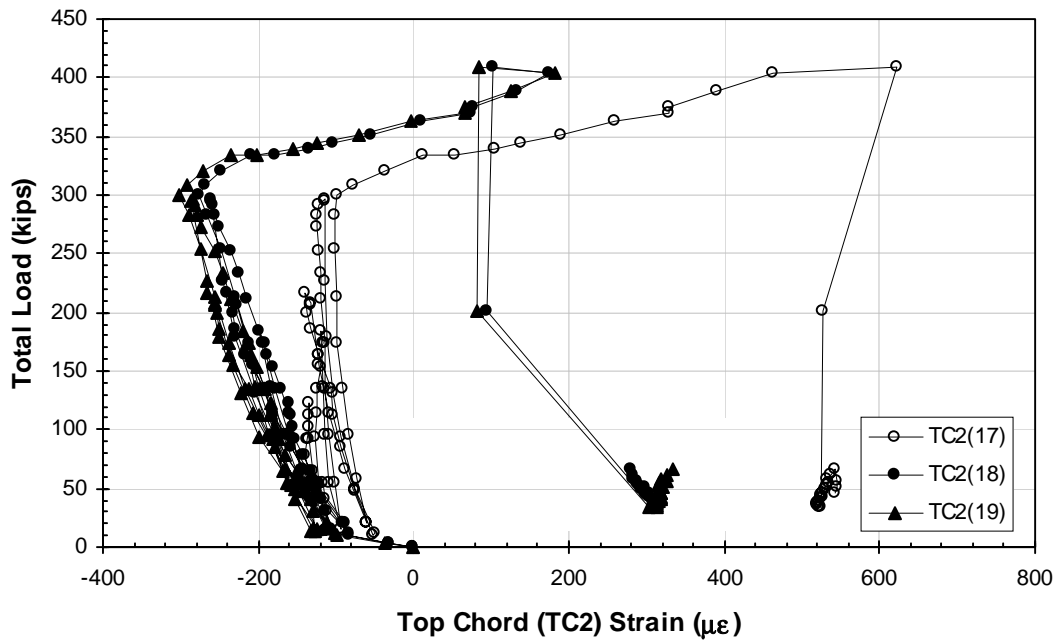
Figure B.8.6 Total Load vs. Bottom Chord (BC2) Strain of IG



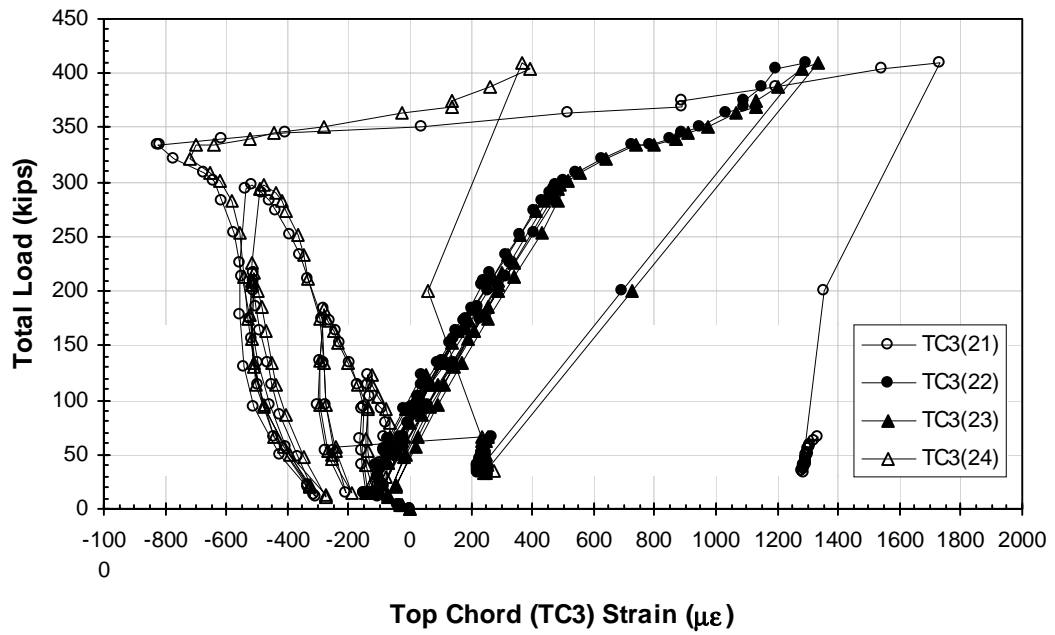
**Figure B.8.7 Total Load vs. Bottom Chord (BC3) Strain of IG**



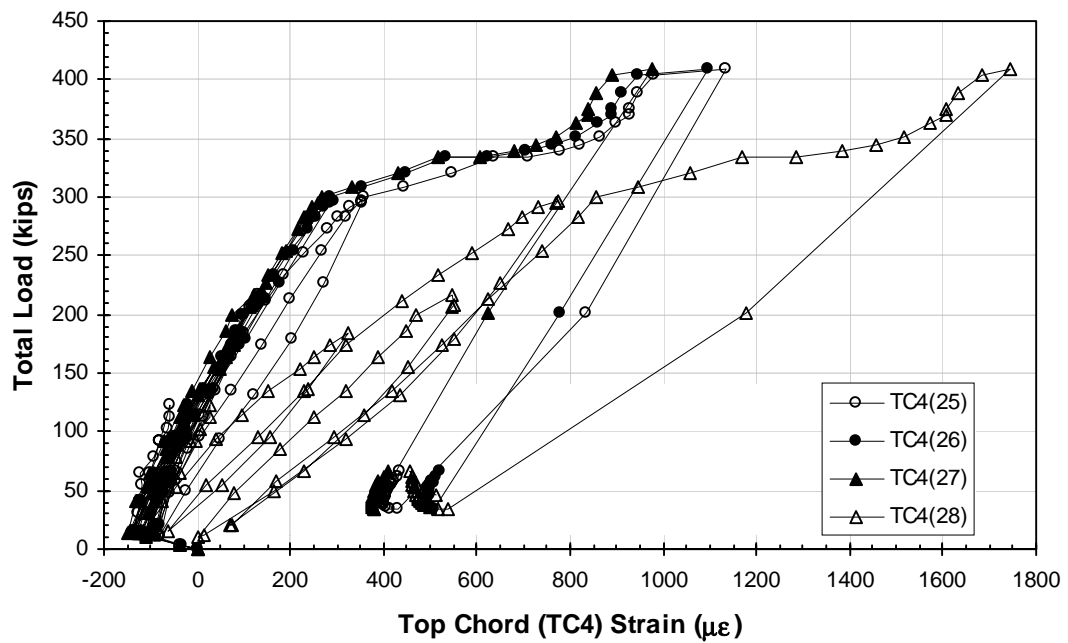
**Figure B.8.8 Total Load vs. Top Chord (TC1) Strain of IG**



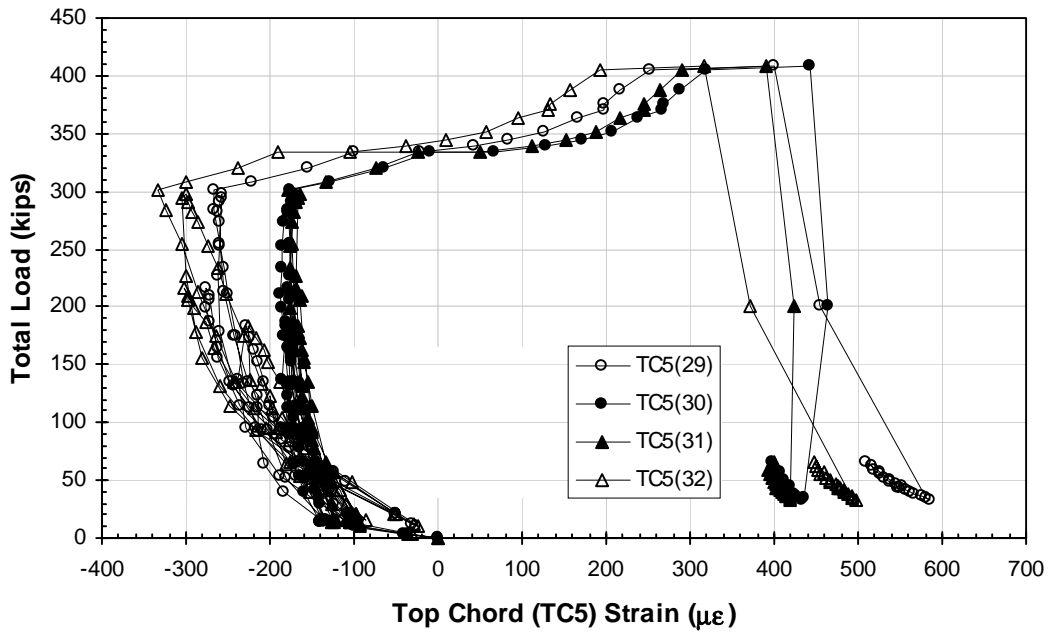
**Figure B.8.9 Total Load vs. Top Chord (TC2) Strain of IG**



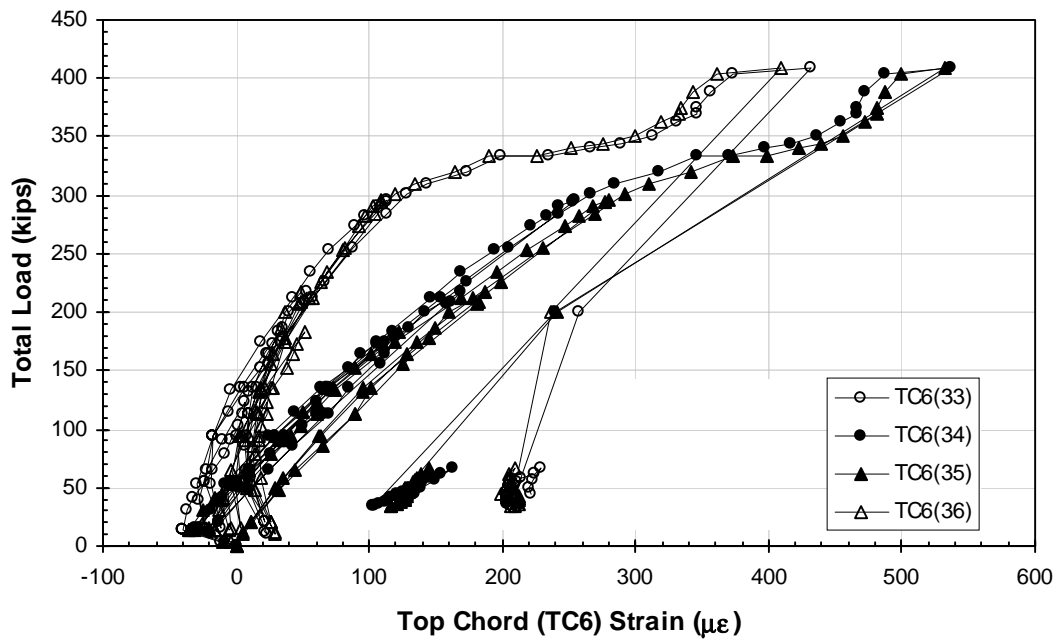
**Figure B.8.10 Total Load vs. Top Chord (TC3) Strain of IG**



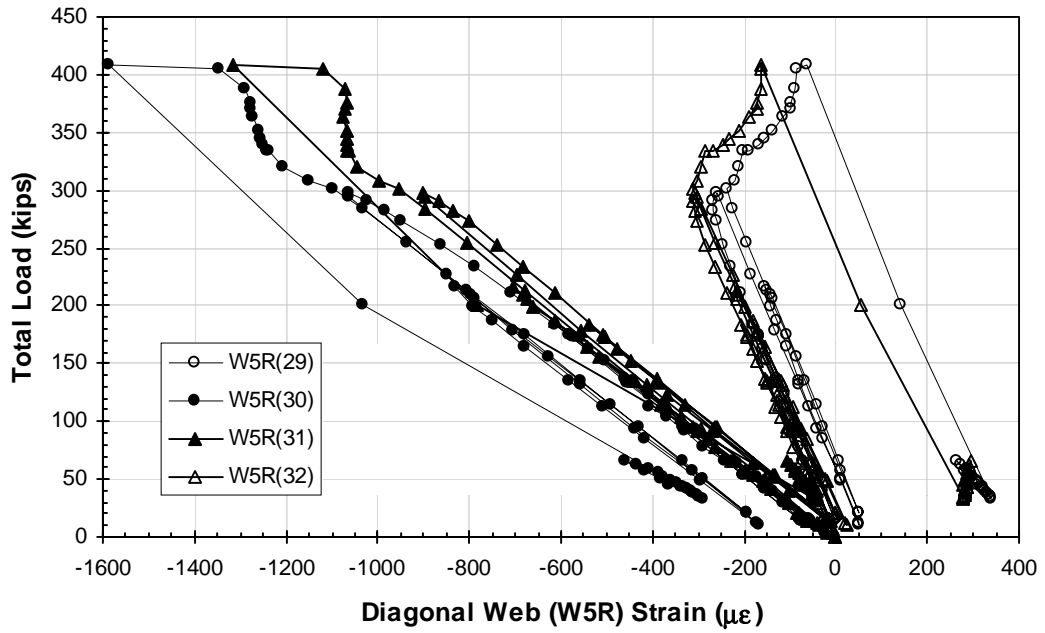
**Figure B.8.11 Total Load vs. Top Chord (TC4) Strain of IG**



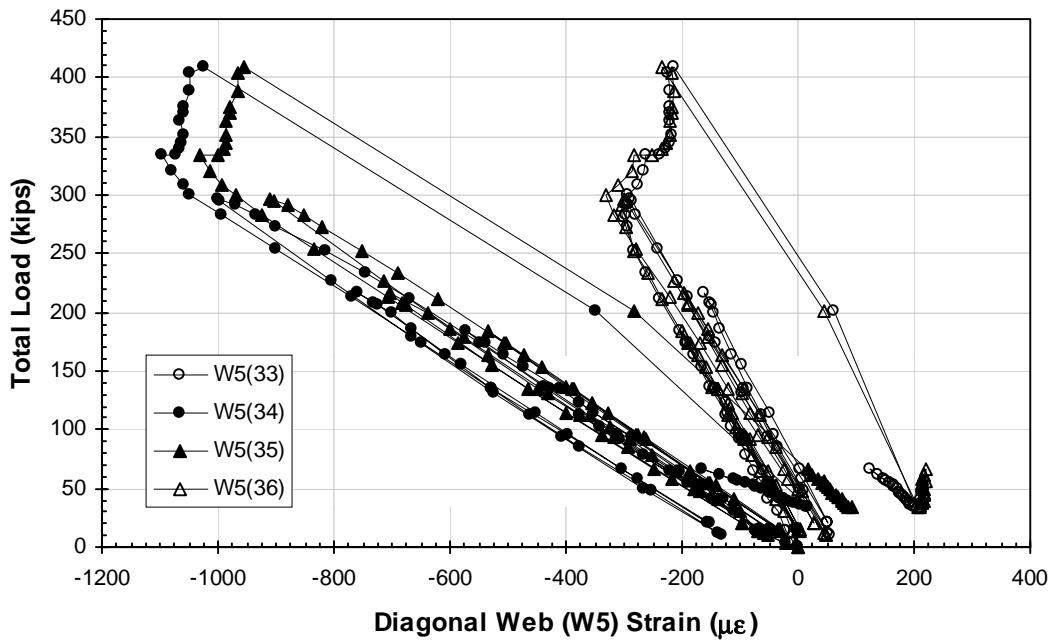
**Figure B.8.12 Total Load vs. Top Chord (TC5) Strain of IG**



**Figure B.8.13 Total Load vs. Top Chord (TC6) Strain of IG**



**Figure B.8.14 Total Load vs. Diagonal Web (W5R) Strain of IG**



**Figure B.8.15 Total Load vs. Diagonal Web (W5) Strain of IG**