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System-Level Simulation of Floating Platform and Wind Turbine Using High-Fidelity and Engineering Models

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Overview



➤ Introduction

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- Review

➤ Approach

- Computational methods
- System geometry
- Test cases and flow conditions
- Computation resource
- Analysis methods

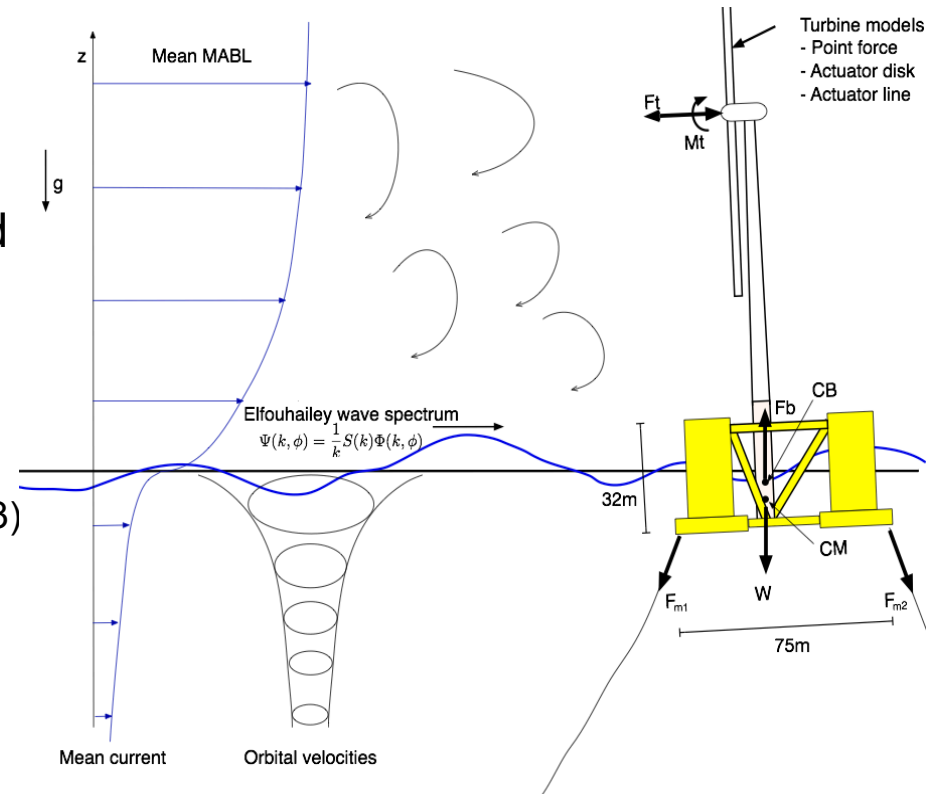
➤ Preliminary Results

➤ Conclusion and Future Work

Objectives

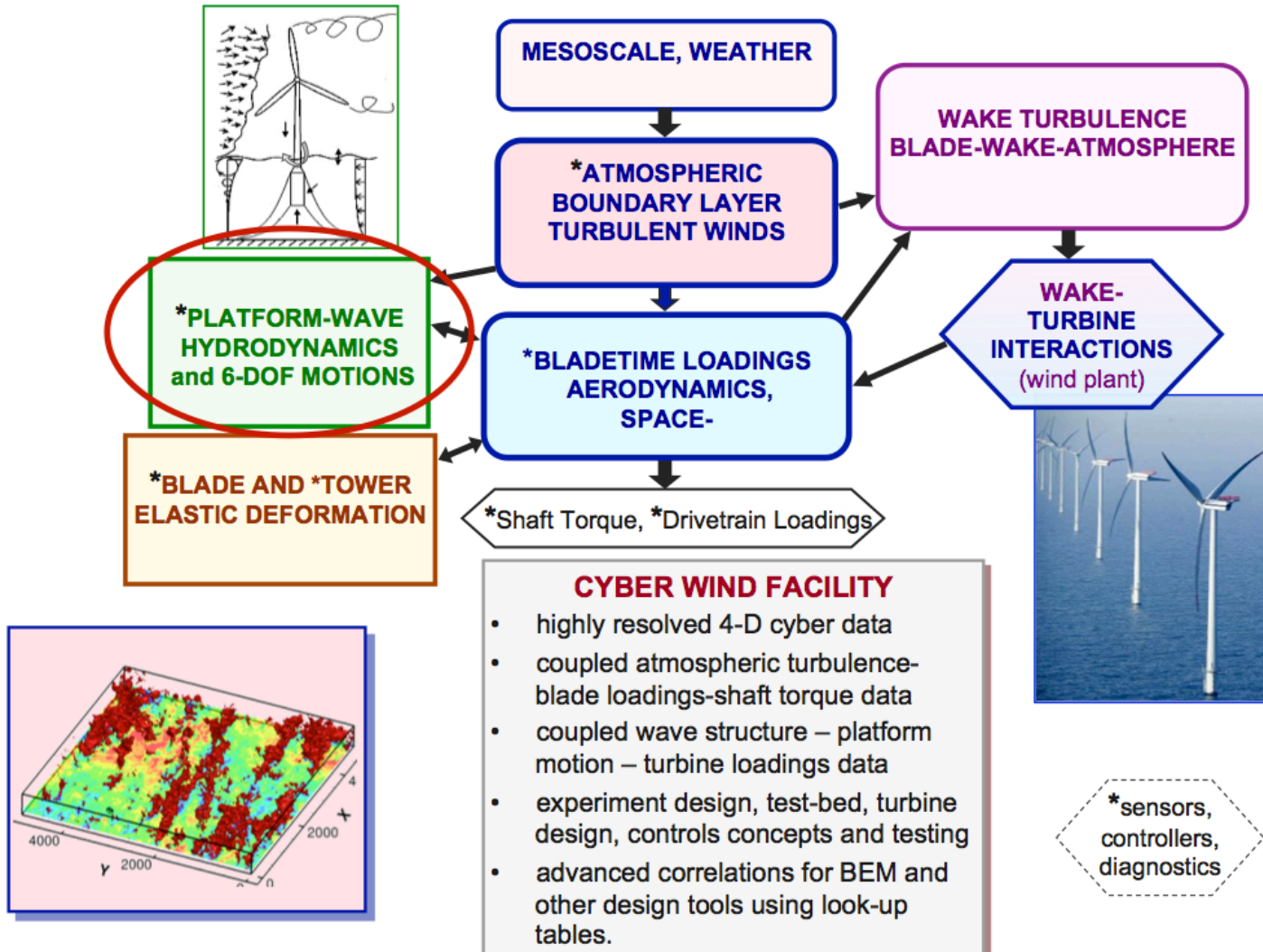
- Study the effect of mooring system on offshore wind turbine dynamics
 - Full-system simulations, including mooring-line and turbine aerodynamics
 - Based on OC3 configurations
- Study the interaction of wave field and wind-turbine platform dynamics
 - From linear waves to real wave fields
 - Quantify impact of platform motion and waves on turbine inflow
 - Validate against limited experimental data (OC3)
- Analyze turbine performance near Virginia coastline
 - Wave and meteorological data from statistics

Full hydrodynamic model





Cyber Wind Facility



➤ **Turbine platform hydrodynamics by CFD**

- Dunbar et al. (2013) – coupled solver
- Calderer et al. (2014) – fluid structure interaction

➤ **Turbine and buoy**

- Jonkman et al. (2009) - 5MW Turbine
- Jonkman et al. (2010) – OC3 spar buoy

➤ **Mooring line modeling**

- Faltinsen (1990) – catenary line

➤ **Actuator Line model(ALM)**

- Sørensen and Shen (2002) – ALM theories
- Churchfield et al. (2012) - SOWFA
- Jha et al., 2014 - CWF

➤ **Waves**

- Jacobsen et al.(2012) – waves2Foam

➤ **Offshore statistics**

- National Buoy Data Center(DBDC)

➤ **Cyber Wind Facility(CWF)**

- Vijayakumar et al. (2014) – blade aerodynamics module
- Jha et al. (2013) – wake modulations module
- Motta-Mena et al. (2013) – structural dynamics module
- Dunbar et al. (2014) – hydrodynamic module

➤ Implementation steps:

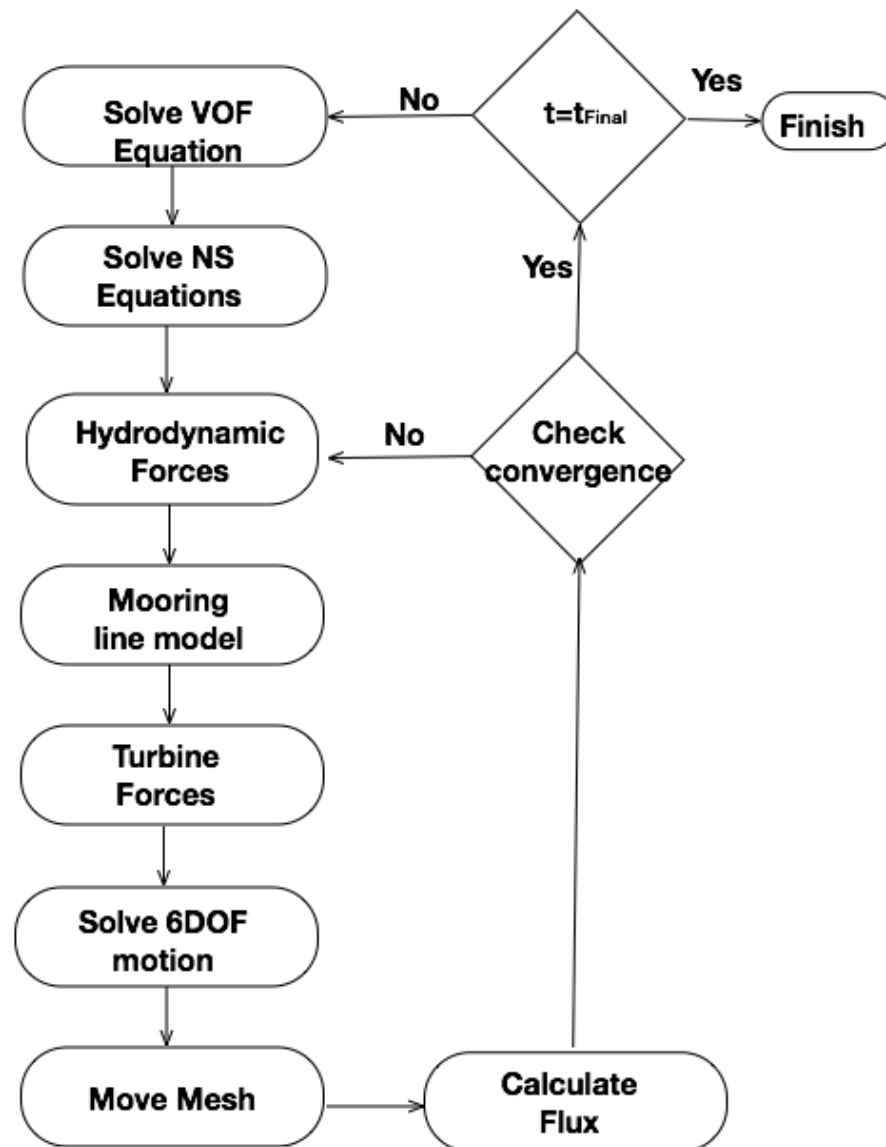
- 1) Generate surface wave with wave2Foam library and inspect the platform response: Done
- 2) Implement mooring line model in CFD code: Done
- 3) Integrate ALM with multi-phase solvers: Done
- 4) Run simulations on the cases with OC3 configurations: In-progress
- 5) Incorporate mooring line model and ALM with tightly-coupled 6DOF solver: Under-development

Multiphase CFD + 6DOF solver



CFD solver: interDyMFoam

- Two-phase incompressible solver
- Interface tracking technique with Volume of Fluid (VOF) field alpha
- Pressure Implicit with Splitting of Operator(PISO) algorithm solves the pressure-velocity coupled system
- Coupled with 6DOF solver:
 - Extract force and moment from pressure and viscous effects
 - Calculate acceleration according to the mass of the object
 - Move center of mass
 - Rotate and translate patches



➤ **Tightly-coupled solver introduces inner loop for algorithm stability under large structure displacement (Dunbar et al. 2013)**

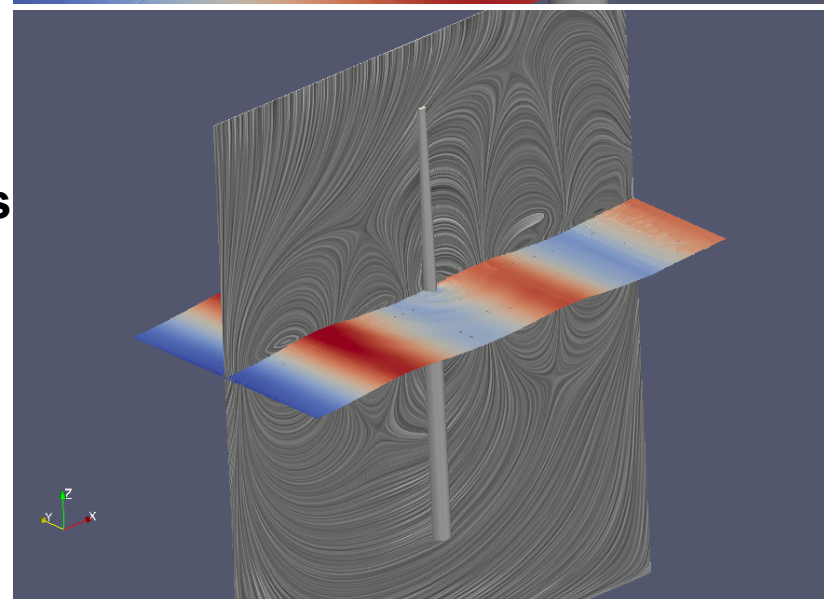
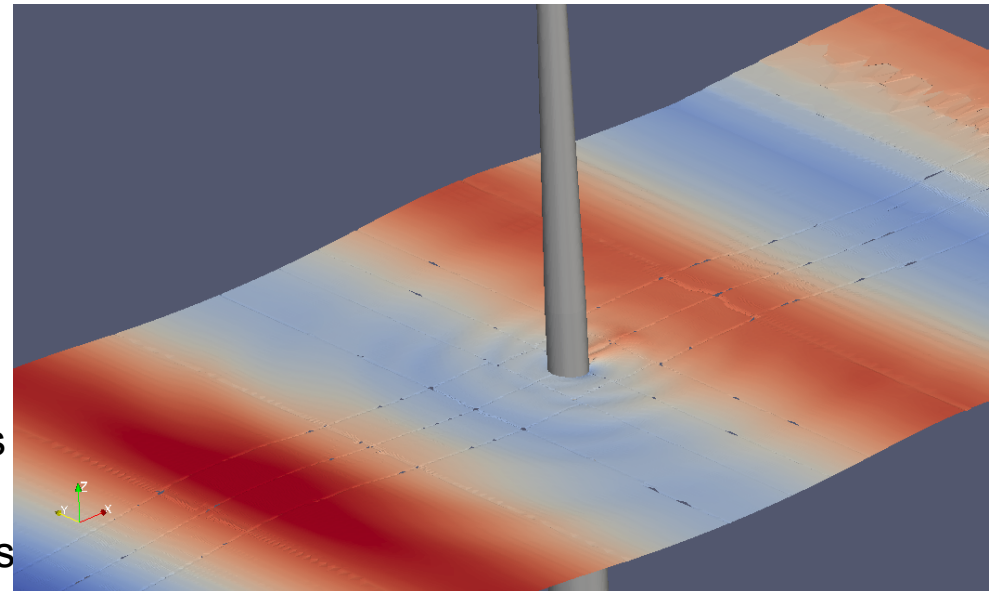
➤ **Waves2Foam: wave generating toolbox**

- Common wave theories
 - Potential current
 - Regular waves: Stokes wave
 - Solitary wave
 - Irregular waves
- Boundary conditions apply wave theories to corresponding field
- Relaxation zones control wave reflections on boundaries
- Utilities that initialize wave field

➤ **Wave forces on OC3 spar buoy has been studied by direct CFD and Morison equation**

- Morison equation is a pure empirical approach

Wave elevation on free surface ($H=7m$, $L=90m$)



Wave elevation on free surface with wave-induced circulations in y-plane ($H=7m$, $L=90m$)

Mooring-line model

➤ Quasi-static mooring line

- Based on catenary line equation
- Mooring system dynamics are ignored
- Mooring force is calculated at each time step according to current geometry

➤ Pseudo code of mooring-line model implementation in OpenFOAM

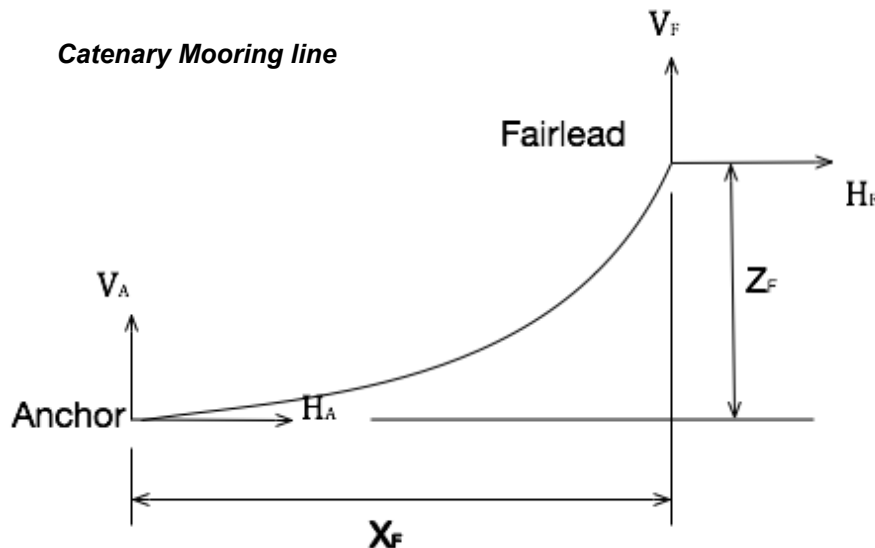
```
//test if the cable touches seabed
touch=testTouch(L,w,EA,CB,XF,ZF);

//initialize vertical and horizontal force
HF1=iniHF(w,XF,ZF,L);
VF1=iniVF(w,XF,ZF,L);

do {
    if touch{
        HF2=solveTouchHF(L,w,EA,CB,XF,ZF,HF1);
        VF2=solveTouchVF(L,w,EA,CB,XF,ZF,VF1);
    }else{
        HF2=solveUntouchHF(L,w,EA,CB,XF,ZF,HF1);
        VF2=solveUntouchVF(L,w,EA,CB,XF,ZF,VF1);
    }
    del_HF=abs(HF1-HF2);
    del_VF=abs(VF1-VF2);

    //set for next iteration
    HF1=HF2;
    VF1=VF2;

    //test if converged
}while(del_HF>epi_HF & del_VF>epi_VF);
```

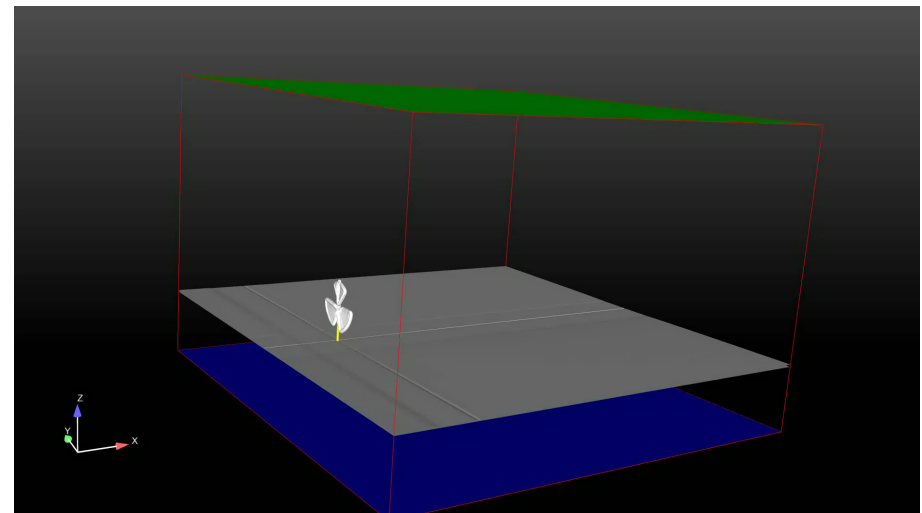
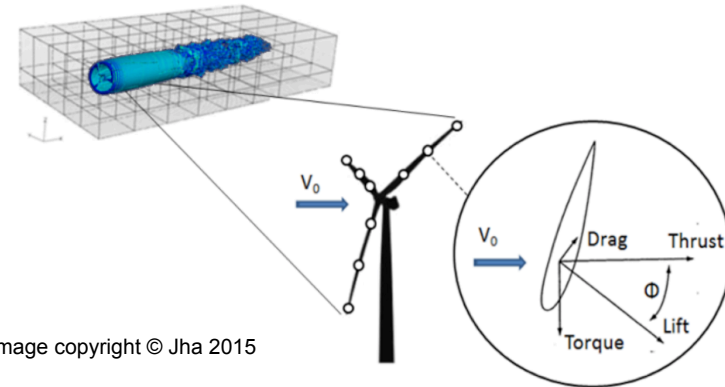


Actuator-Line Model

➤ Actuator Line Model (ALM) – Pankaj / Churchfield

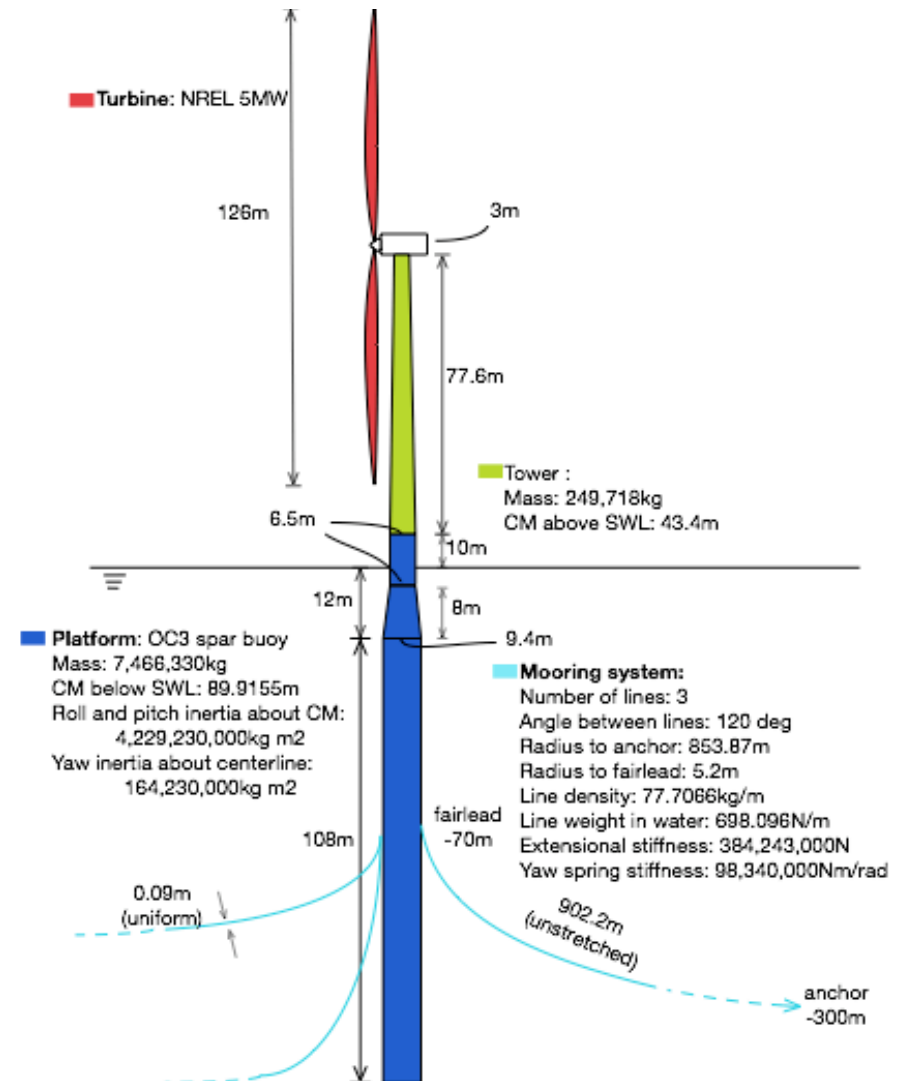
- Discretize each blade into sections, assume uniform blade configuration and flow condition for each section
- Sectional force of each element is calculated according to local flow conditions and airfoil lookup table
- Spread sectional force from each element by Gaussian distribution as additional body force at each cell

➤ Multiphase solver with ALM was tested



OC3 System Geometry

- **NREL 5MW turbine**
 - Diameter: 126m
- **OC3 spar buoy**
 - Total draft: 120m
 - Weight: 7,466,330kg
- **Uniform mooring cables**
 - Fairlead at 70m below Still Water Line(SWL)
 - Anchor point at 320m below SWL
 - 853.87m from buoy centerline to anchor
 - The vertical force on buoy is $-1.66e6N$



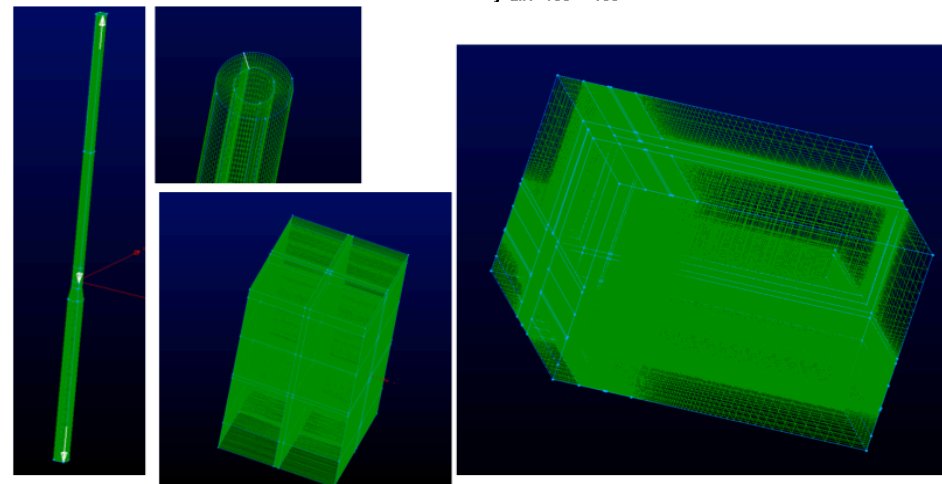
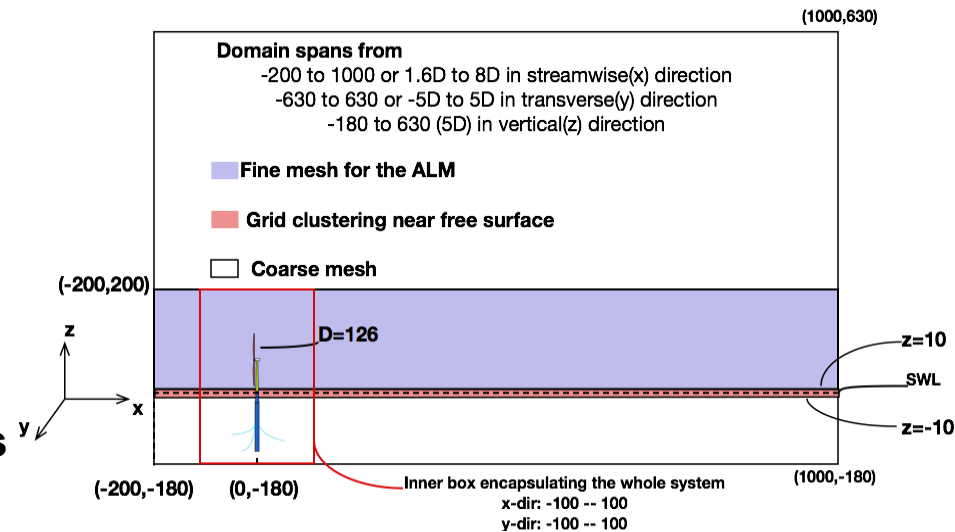
Test Cases and Flow Conditions

- In order to study the effect of free surface on turbine performance, 6 cases are tested:

Free surface	LES	DES	RANS
Level ground	LES	DES	RANS

- LES: Smagorinsky
- DES: SpalartAllmarasDDES
- RANS: Standard SpalartAllmaras
- Domain is cut at the SWL ($z=0$) for cases with solid surface**
- Flow conditions:**
 - $U=8\text{m/s}$ uniform in air
 - Water is kept still
 - Structure is fixed

Computational domain with free surface



Computational Resource

- **All simulations are supported by Advanced Research Computing(ARC) in VT**
 - Blueridge: 408-nodes Cray cs-300 cluster
 - Release in 2013
 - Two octa-core Intel Sandy Bridge CPUs per node
 - 64 GB of memory per node
 - Each case is ran on 64 cores
 - 7.2 millions cells for free surface cases
 - 1.12e5 cells/core
 - Simulation walltime is set to 72-hours
 - Initial turbine rotational speed ad 11rpm
 - Approximately 9.7rpm in steady state
 - Simulation runs until $\approx 120s$
 - 0.6hour/revolution
 - Post-processing by Enight
 - Parallel client-server using 4 cores



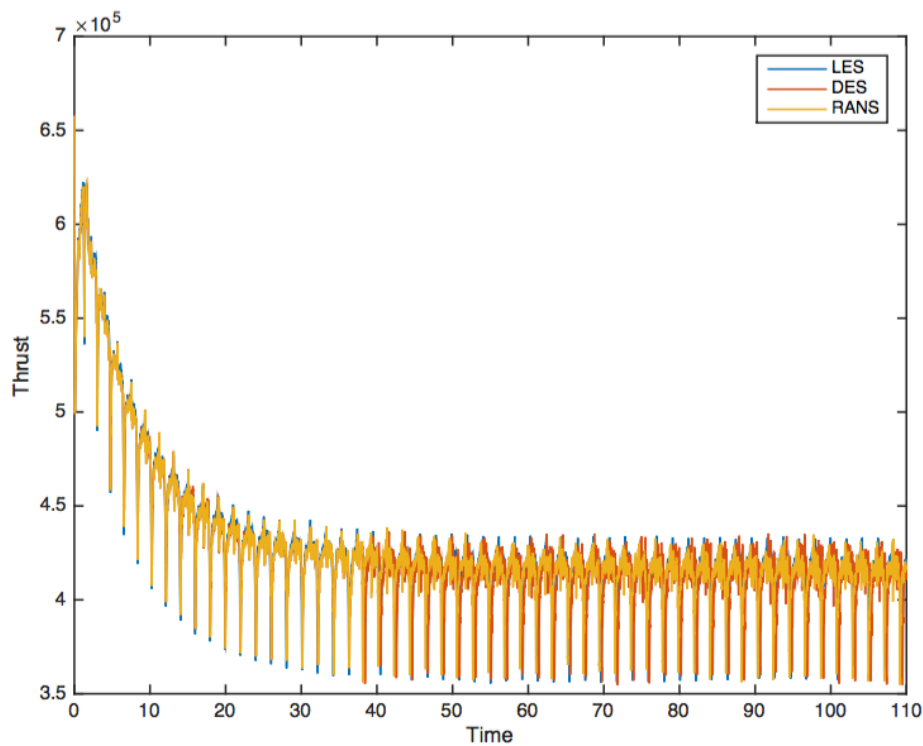
Analysis



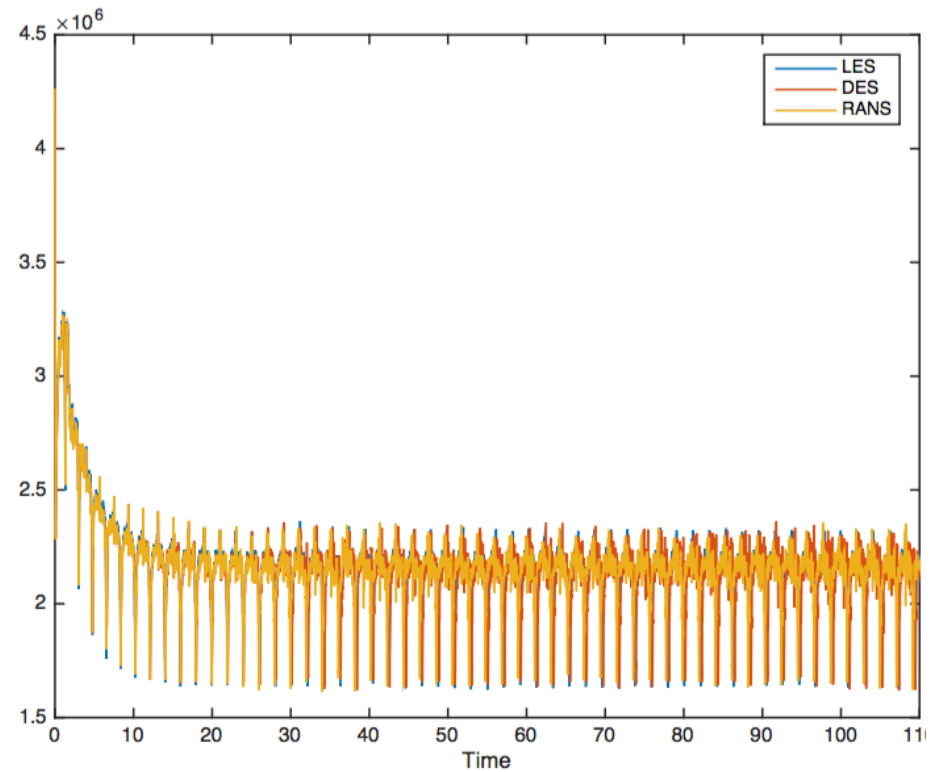
- The following fields will be analyzed:
 - Time history of thrust, torque on turbine blades
 - Diagnose angle-of-attack vs. radius over turbine rotation
 - Turbine wake at $x/D = 0.5, 1.0, 2.0$
 - Instantaneous U, TKE, vorticity
 - Mean U, TKE, vorticity
 - Surface shear stress and limiting streamlines on ground and water free surface
 - Wave field generated by turbine aerodynamics and platform hydrodynamics

Preliminary Results

Turbine Thrust of the cases with level ground surface

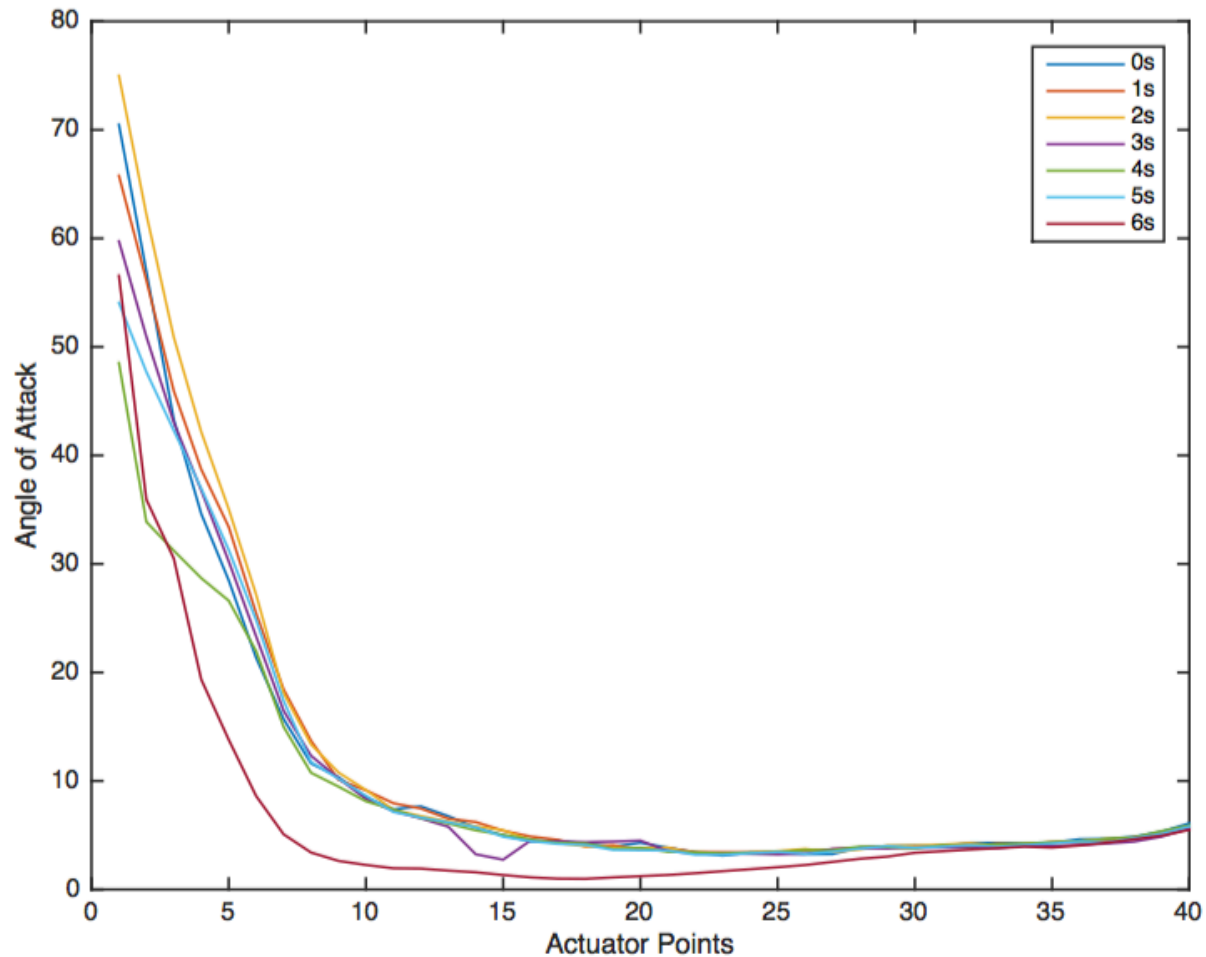


Turbine Torque of the cases with level ground surface



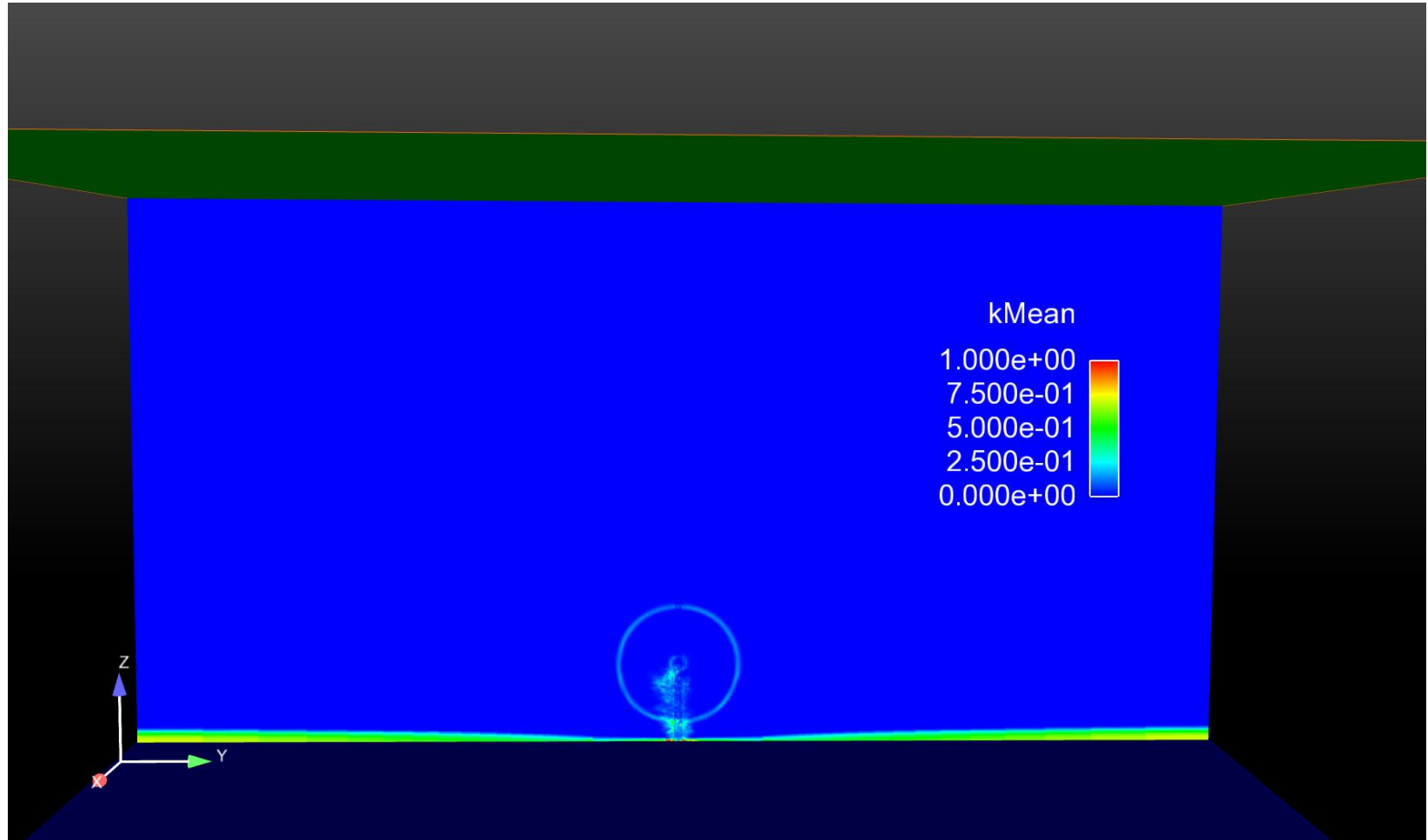
Preliminary Results

Angle of attack at each actuator point of turbine blade over one rotation



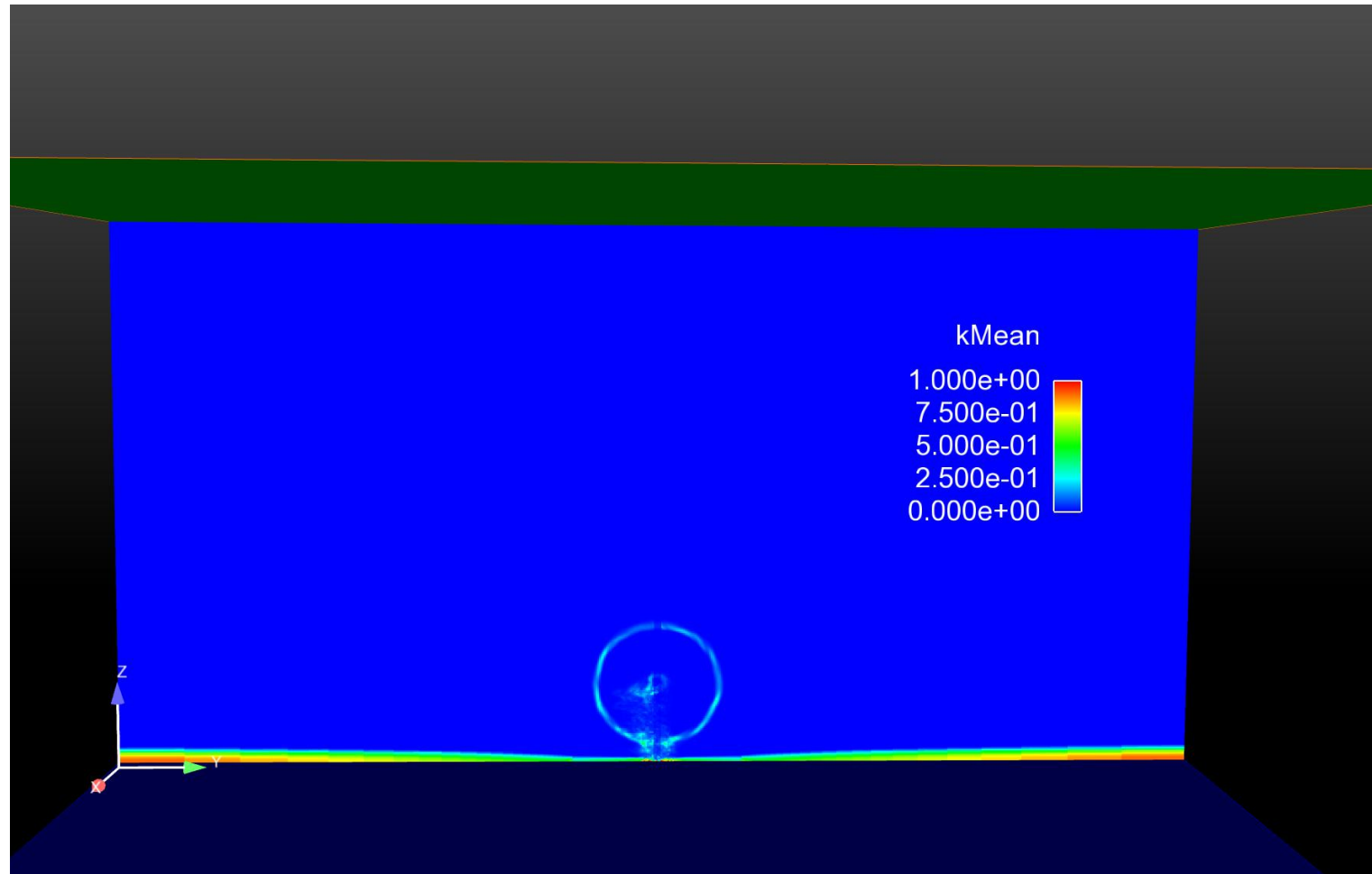
Preliminary Results

Mean turbulence kinetic energy 0.5D downstream



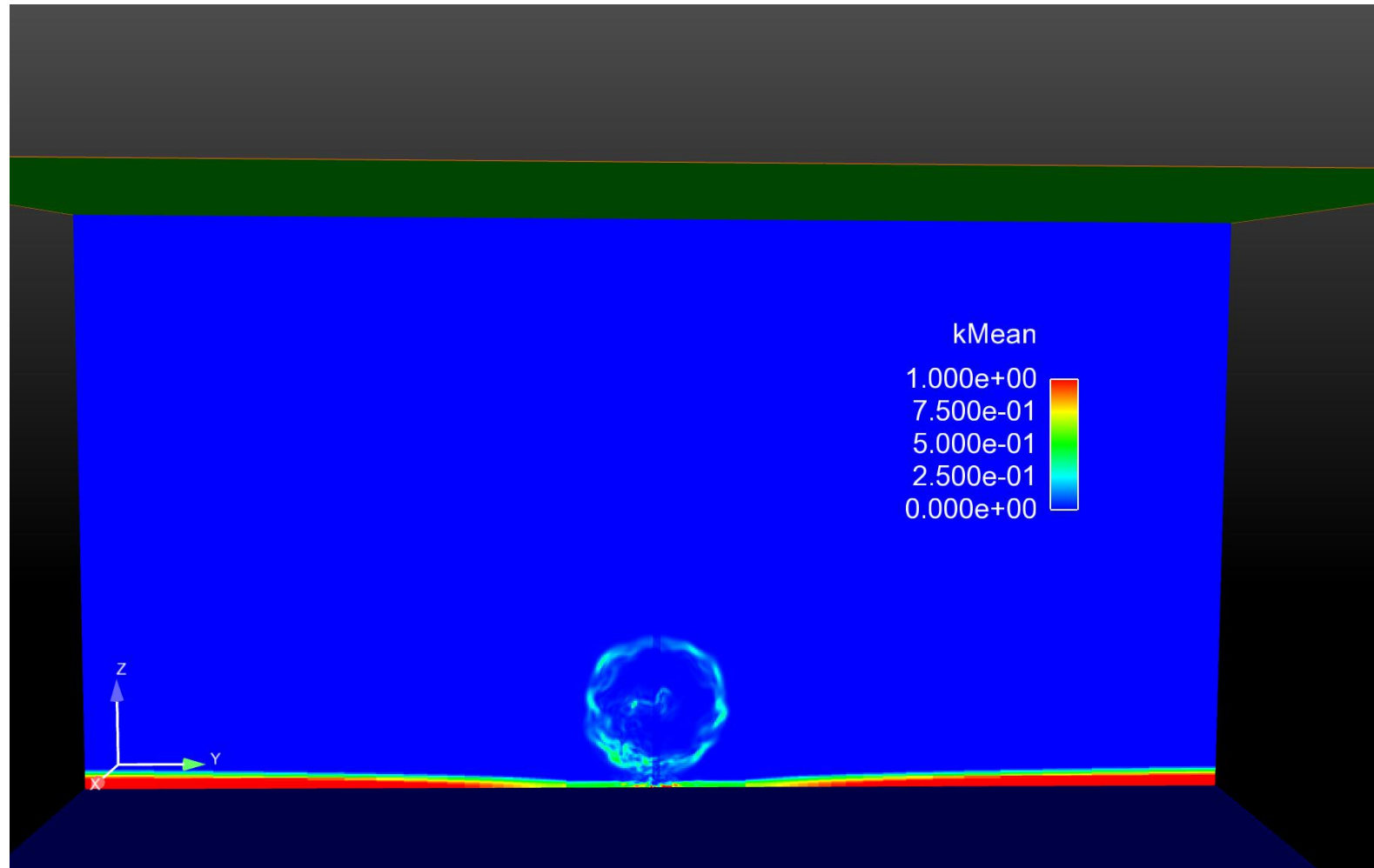
Preliminary Results

Mean turbulence kinetic energy 1D downstream



Preliminary Results

Mean turbulence kinetic energy 2D downstream



Conclusion and Future Work



- **The implementation of mooring-line model in OpenFOAM provides restoring force for the platform, further validation is needed(NREL's HydroDyN).**
- **Actuator Line Models works with multiphase solver, studies on turbine-wave interactions can be conducted bases on it.**
- **Use of robust HPC resources at VT-ARC gives good turn-around.**
- **Current multiphase solver was proven to be unstable under large structure displacement, tightly-coupled solver will be adopted in future work.**
- **waves2Foam supports various long-crest wave theories, in order to model statistical conditions, it needs to be extended for directional spectrum and short-crested wave model.**

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