

Table 1. CERES launch dates and spacecraft information.

| Spacecraft                    | TRMM               | EOS-AM                | EOS-PM                |
|-------------------------------|--------------------|-----------------------|-----------------------|
| <b>Instruments</b>            | Proto-Flight Model | Flight Models 1 and 2 | Flight Models 3 and 4 |
| <b>Launch Date</b>            | 1 November 1997    | June 1998             | December 2000         |
| <b>Inclination</b>            | 35 deg             | 81 deg                | 81 deg                |
| <b>Altitude</b>               | 350 km             | 705 km                | 705 km                |
| <b>Local Observation Time</b> | precessing         | 10:30 AM              | 1:30 PM               |

Table 2. Spectral bands of interest for the study of Earth/atmosphere energetics.

| <b>Passband<br/>(<math>\mu\text{m}</math>)</b> | <b>Scientific Perspective</b>                                                   |
|------------------------------------------------|---------------------------------------------------------------------------------|
| 0.3 - 0.4                                      | Sensitive to changing O <sub>3</sub> abundances                                 |
| 0.4 - 0.7                                      | Drives biological systems; foliage amounts                                      |
| 0.7 - 1.6                                      | Sensitive to changing H <sub>2</sub> O abundances                               |
| 1.6 - 4.5                                      | Near IR, Far Solar effects                                                      |
| 4.5 - 8.0                                      | 6.3 $\mu\text{m}$ band of H <sub>2</sub> O; upper tropospheric H <sub>2</sub> O |
| 8.0 - 12.0                                     | CERES channel                                                                   |
| 12.0 - 17.0                                    | Sensitive to changing CO <sub>2</sub> abundances                                |
| 17.0 - 100                                     | Sensitive to changing H <sub>2</sub> O abundances                               |
| 0.3 - 5.0                                      | CERES channel                                                                   |
| 0.3 - 100                                      | CERES channel                                                                   |
| 5.0 - 100                                      | Continuity check for total - shortwave                                          |
| 8.0 - 9.1                                      | Surface emissivity                                                              |
| 9.1 - 10.2                                     | Sensitive to changing O <sub>3</sub> abundances                                 |
| 10.2 - 12.0                                    | Sensitive to cirrus clouds                                                      |

Table 3. Nominal component values for the CERES PFM total channel pre-amplifier circuit.

| Component       | Nominal Value | Units |
|-----------------|---------------|-------|
| R <sub>1</sub>  | 140.0         | kΩ    |
| R <sub>2</sub>  | 140.0         | kΩ    |
| R <sub>3</sub>  | 140.0         | kΩ    |
| R <sub>4</sub>  | 140.0         | kΩ    |
| R <sub>5</sub>  | 2.22          | kΩ    |
| R <sub>6</sub>  | 10.0          | kΩ    |
| R <sub>7</sub>  | 10.0          | kΩ    |
| R <sub>8</sub>  | 10.0          | kΩ    |
| R <sub>9</sub>  | 10.0          | kΩ    |
| R <sub>10</sub> | 10.0          | kΩ    |
| R <sub>11</sub> | 10.0          | kΩ    |
| R <sub>12</sub> | 2.843         | kΩ    |
| R <sub>13</sub> | 2.843         | kΩ    |
| R <sub>14</sub> | 500           | kΩ    |
| R <sub>15</sub> | 10.0          | kΩ    |
| R <sub>16</sub> | 10.0          | kΩ    |
| C <sub>1</sub>  | 0.001         | μf    |

Table 4. Nominal component values for the CERES PFM total channel Bessel filter circuit.

| Component       | Nominal Value | Units |
|-----------------|---------------|-------|
| R <sub>1</sub>  | 20.0          | kΩ    |
| R <sub>2</sub>  | 10.0          | kΩ    |
| R <sub>3</sub>  | 20.0          | kΩ    |
| R <sub>4</sub>  | 10.0          | kΩ    |
| R <sub>5</sub>  | 108.43        | kΩ    |
| R <sub>6</sub>  | 100.02        | kΩ    |
| R <sub>7</sub>  | 1.29          | MΩ    |
| R <sub>8</sub>  | 100.02        | kΩ    |
| R <sub>9</sub>  | 8.4074        | kΩ    |
| R <sub>10</sub> | 156.9         | kΩ    |
| R <sub>11</sub> | 89.219        | kΩ    |
| R <sub>12</sub> | 206.83        | kΩ    |
| R <sub>13</sub> | 89.219        | kΩ    |
| R <sub>14</sub> | 67.680        | kΩ    |
| C <sub>1</sub>  | 0.05          | μf    |
| C <sub>2</sub>  | 0.05          | μf    |
| C <sub>3</sub>  | 0.05          | μf    |
| C <sub>4</sub>  | 0.05          | μf    |

Table 5. Nominal and modeled specifications for the detector module assembly.

| Layer         | Thermal Conductivity<br>W/mK | Volumetric<br>Mass<br>kg/m <sup>3</sup> | Specific Heat<br>J/kgK | Nominal Thickness<br>μm | Modeled Thickness<br>μm |
|---------------|------------------------------|-----------------------------------------|------------------------|-------------------------|-------------------------|
| Absorber      | 0.209                        | 1400                                    | 668.8                  | 10.6                    | 10.0                    |
| Epoxy/Varnish | 0.1                          | 1150                                    | 1000.0                 | 7.5                     | 4.90                    |
| Gold Pads     | 292.9                        | 19320                                   | 129.6                  | 0.5                     | 0.5                     |
| Thermistor    | 8.36                         | 5000                                    | 752.4                  | 15.0                    | 15.0                    |
| Upper Epoxy   | 0.1254                       | 1200                                    | 1045.0                 | 1.0                     | 0.75                    |
| Kapton        | 0.1200                       | 1420                                    | 1091.0                 | 7.62                    | 7.62                    |
| Lower Epoxy   | 0.1254                       | 1200                                    | 1045.0                 | 1.0                     | 0.25                    |
| Aluminum      | 237.0                        | 2700                                    | 903.0                  | 3668.0                  | 3668                    |
| Indium        | 80.84                        | 11480                                   | 240.3                  | 2.54                    | 2.54                    |

Table 6. Predicted time constant and responsivity sensitivities,  $\partial A / \partial B$ , where A equals either time constant,  $\tau$ , or Responsivity, R, and B equals layer thickness,  $\delta$ , of the CERES detector module assembly.

| <b>Detector Layer</b> | <b>Predicted Time Constant Sensitivity,<br/><math>\frac{\partial \tau}{\partial \delta}</math><br/>(ms/<math>\mu\text{m}</math>)</b> | <b>Predicted Responsivity Sensitivity,<br/><math>\frac{\partial R}{\partial \delta}</math><br/>(V/W/<math>\mu\text{m}</math>)</b> |
|-----------------------|--------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------|
| <b>Absorber</b>       | 0.24                                                                                                                                 | 0.01                                                                                                                              |
| <b>Epoxy/Varnish</b>  | 0.35                                                                                                                                 | 0.04                                                                                                                              |
| <b>Thermistor</b>     | 0.39                                                                                                                                 | 0.13                                                                                                                              |
| <b>Upper Epoxy</b>    | 1.35                                                                                                                                 | 7.35                                                                                                                              |
| <b>Kapton</b>         | 1.43                                                                                                                                 | 10.87                                                                                                                             |
| <b>Bottom Epoxy</b>   | 1.37                                                                                                                                 | 10.38                                                                                                                             |

Table 7. Narrow Field Black body (NFBB) temperatures, unfiltered and filtered radiances from the CERES ground calibration.

| NFBB Temperature<br>K | Unfiltered Radiances<br>W/m <sup>2</sup> sr | Filtered Radiances<br>W/m <sup>2</sup> sr |
|-----------------------|---------------------------------------------|-------------------------------------------|
| 206.40                | 32.864                                      | 28.314                                    |
| 216.03                | 39.443                                      | 34.027                                    |
| 230.37                | 51.007                                      | 44.082                                    |
| 246.06                | 66.385                                      | 57.476                                    |
| 253.04                | 74.243                                      | 64.329                                    |
| 264.98                | 89.277                                      | 77.452                                    |
| 278.04                | 108.221                                     | 94.009                                    |
| 284.86                | 119.236                                     | 103.646                                   |
| 290.74                | 129.391                                     | 112.536                                   |
| 297.61                | 142.063                                     | 123.637                                   |
| 304.95                | 156.609                                     | 136.388                                   |
| 311.84                | 171.255                                     | 149.236                                   |

Table 8. Comparison of gains determined during the CERES ground calibration to the predicted values determined with the end-to-end model.

| Gain Term | CERES<br>Ground<br>Calibration | Numerical<br>Simulation | Percent<br>Difference | units                                       |
|-----------|--------------------------------|-------------------------|-----------------------|---------------------------------------------|
| $A_V$     | 0.1499                         | 0.1464                  | 2.33                  | $\text{Wm}^{-2}\text{sr}^{-1}/\text{count}$ |
| $A_S$     | -                              | 0.1464                  | -                     | $\text{Wm}^{-2}\text{sr}^{-1}/\text{count}$ |
| $A_H$     | -                              | 1.6174                  | -                     | $\text{Wm}^{-2}\text{sr}^{-1}/\text{K}$     |
| $A_B$     | -                              | 0.0                     | -                     | $\text{Wm}^{-2}\text{sr}^{-1}/\text{V}$     |
| $A_D$     | -                              | 0.0                     | -                     | $\text{Wm}^{-2}\text{sr}^{-1}/\text{V}$     |

Table 9. Slow-mode numerical algorithm coefficient values in Eqs. 5.14 and 5.15 determined using the model.

| Coefficient | Value                   | Units |
|-------------|-------------------------|-------|
| $C_1$       | 0.99                    | -     |
| $C_2$       | 0.01                    | -     |
| $C_3$       | 0.00726                 | -     |
| $\tau_1$    | 8.5                     | ms    |
| $\tau_2$    | 43                      | ms    |
| $\tau_3$    | 310                     | ms    |
| $p_0$       | 0.9968                  | -     |
| $p_1$       | $2.3563 \times 10^{-5}$ | -     |

Table 10. Results of a study where the thermal impedance between the compensating thermistor and aluminum substrate was varied.

| Epoxy thickness<br>μm | Responsivity<br>V/W | Time Constant<br>ms |
|-----------------------|---------------------|---------------------|
| 0.25                  | 63.97               | 9.27                |
| 0.75                  | 62.34               | 8.97                |
| 1                     | 61.54               | 8.82                |
| 1.25                  | 60.76               | 8.68                |
| 1.5                   | 59.99               | 8.54                |
| 1.75                  | 55.70               | 8.40                |

Table 11. Overall number of footprints sorted by cloud categories for two weightings of the point spread function. Row and Column values correspond to the point spread function weightings displayed in Figures 5.33(a) and (b), respectively.

|               |                      | 2-by-2 bins |               |               |          |       |
|---------------|----------------------|-------------|---------------|---------------|----------|-------|
|               |                      | clear       | partly cloudy | mostly cloudy | overcast | total |
| 16-by-16 bins | <b>clear</b>         | 5480        | 121           | 0             | 1        | 5602  |
|               | <b>partly cloudy</b> | 4862        | 3066          | 907           | 419      | 9254  |
|               | <b>mostly cloudy</b> | 326         | 1444          | 1809          | 4982     | 8561  |
|               | <b>overcast</b>      | 275         | 9             | 74            | 8269     | 8627  |
|               | <b>total</b>         | 10943       | 4640          | 2790          | 13671    | 32044 |

Table 12. Overall number of footprints sorted by surface type for two weightings of the point spread function. Row and Column values correspond to the point spread function weightings displayed in Figures 5.33(a) and (b), respectively.

|               |               | 2-by-2 bins  |       |      |        |       |       |       |
|---------------|---------------|--------------|-------|------|--------|-------|-------|-------|
|               |               | ocean        | land  | snow | desert | coast | total |       |
| 16-by-16 bins | <b>ocean</b>  | 23250        | 12    | 0    | 0      | 19    | 23281 |       |
|               | <b>land</b>   | 4            | 7229  | 14   | 0      | 13    | 7260  |       |
|               | <b>snow</b>   | 2            | 20    | 734  | 0      | 4     | 760   |       |
|               | <b>desert</b> | 0            | 0     | 0    | 22     | 0     | 22    |       |
|               | <b>coast</b>  | 301          | 260   | 9    | 0      | 151   | 721   |       |
|               |               | <b>total</b> | 23559 | 7521 | 757    | 22    | 187   | 32044 |

Table 13. Comparison of the recovered **shortwave** TOA flux ( $\text{Wm}^{-2}$ ) for the two point spread function weightings displayed in Figure 5.33. The statistical mean difference in  $\text{Wm}^{-2}$  (2-by-2 minus 16-by-16), standard deviation of the differences (std), and number of footprints (count) used in the comparison are presented.

|               |                      | 2-by-2 bins |                  |                  |          |       |
|---------------|----------------------|-------------|------------------|------------------|----------|-------|
|               |                      | clear       | partly<br>cloudy | mostly<br>cloudy | overcast |       |
| 16-by-16 bins | <b>clear</b>         | -0.05       | 6.49             | 0.00             | 0.00     | mean  |
|               |                      | 3.20        | 15.84            | 0.00             | 0.00     | std   |
|               |                      | 4447        | 92               | 0                | 0        | count |
|               | <b>partly cloudy</b> | -11.13      | -0.22            | 12.08            | 20.05    | mean  |
|               |                      | 18.11       | 3.47             | 16.29            | 26.96    | std   |
|               |                      | 3124        | 2010             | 565              | 254      | count |
|               | <b>mostly cloudy</b> | -34.11      | -12.51           | -0.04            | 9.63     | mean  |
|               |                      | 49.95       | 27.51            | 1.21             | 17.15    | std   |
|               |                      | 211         | 992              | 1280             | 3410     | count |
|               | <b>overcast</b>      | -6.20       | -68.48           | -20.26           | 0.00     | mean  |
|               |                      | 20.88       | 64.3             | 22.25            | 0.08     | std   |
|               |                      | 4           | 6                | 54               | 5912     | count |

Table 14. Comparison of the recovered **longwave** TOA flux ( $\text{Wm}^{-2}$ ) for the two point spread function weightings displayed in Figure 5.33. The statistical mean difference in  $\text{Wm}^{-2}$  (2-by-2 minus 16-by-16), standard deviation of the differences (std), and number of footprints (count) used in the comparison are presented.

|               |                      | 2-by-2 bins |       |                  |                  |          |  |
|---------------|----------------------|-------------|-------|------------------|------------------|----------|--|
|               |                      | cloudiness  | clear | partly<br>cloudy | mostly<br>cloudy | overcast |  |
| 16-by-16 bins | <b>clear</b>         | 0.00        | 0.23  | 0.00             | -3.09            | mean     |  |
|               |                      | .31         | 0.63  | 0.00             | 0.00             | Std      |  |
|               |                      | 5480        | 121   | 0                | 1                | count    |  |
|               | <b>partly cloudy</b> | -0.28       | -0.01 | 0.15             | -0.27            | mean     |  |
|               |                      | 0.78        | 0.16  | 1.00             | 1.25             | std      |  |
|               |                      | 4862        | 3066  | 907              | 419              | count    |  |
|               | <b>mostly cloudy</b> | -0.25       | 0.26  | 0.00             | -0.43            | mean     |  |
|               |                      | 1.55        | 1.13  | 0.04             | 0.50             | std      |  |
|               |                      | 326         | 1444  | 1809             | 4982             | count    |  |
|               | <b>overcast</b>      | -0.70       | 0.83  | 0.51             | 0.00             | mean     |  |
|               |                      | 4.60        | 1.02  | 0.56             | 0.01             | std      |  |
|               |                      | 275         | 9     | 74               | 8269             | count    |  |

Table 15. Autoregression coefficients determined for four combinations of n, N, and frequency content,  $\omega$ . All units are in  $\text{Wm}^{-2}\text{sr}^{-1}/\text{count}$ .

| Coefficient    | n=4<br>N=5<br>$\omega=20 \text{ Hz}$ | n=4<br>N=12<br>$\omega=10 \text{ Hz}$ | n=4<br>N=12<br>$\omega=20 \text{ Hz}$ | n=4<br>N=12<br>$\omega=30 \text{ Hz}$ |
|----------------|--------------------------------------|---------------------------------------|---------------------------------------|---------------------------------------|
| A <sub>1</sub> | -2.6855 x 10 <sup>-6</sup>           | -5.5767 x 10 <sup>-6</sup>            | -4.2493 x 10 <sup>-6</sup>            | 1.8792 x 10 <sup>-6</sup>             |
| A <sub>2</sub> | -5.7803 x 10 <sup>-6</sup>           | -5.5923 x 10 <sup>-6</sup>            | -4.8840 x 10 <sup>-6</sup>            | 4.5437 x 10 <sup>-7</sup>             |
| A <sub>3</sub> | -7.0164 x 10 <sup>-6</sup>           | -9.3568 x 10 <sup>-7</sup>            | -4.2011 x 10 <sup>-6</sup>            | -1.3222 x 10 <sup>-5</sup>            |
| A <sub>4</sub> | -1.9232 x 10 <sup>-6</sup>           | 1.1504 x 10 <sup>-6</sup>             | -4.1307 x 10 <sup>-6</sup>            | -2.2797 x 10 <sup>-5</sup>            |